

Contrasting Design Approaches for Slab-on-Ground and Raised Floor Foundations on Expansive Soils

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Outline

- Elements of design
- Site conditions
- Slabs-on-ground
- Raised floor foundations
- Costs

Elements of Design

- Structural requirements
 - Moments
 - Shear
 - Deflection

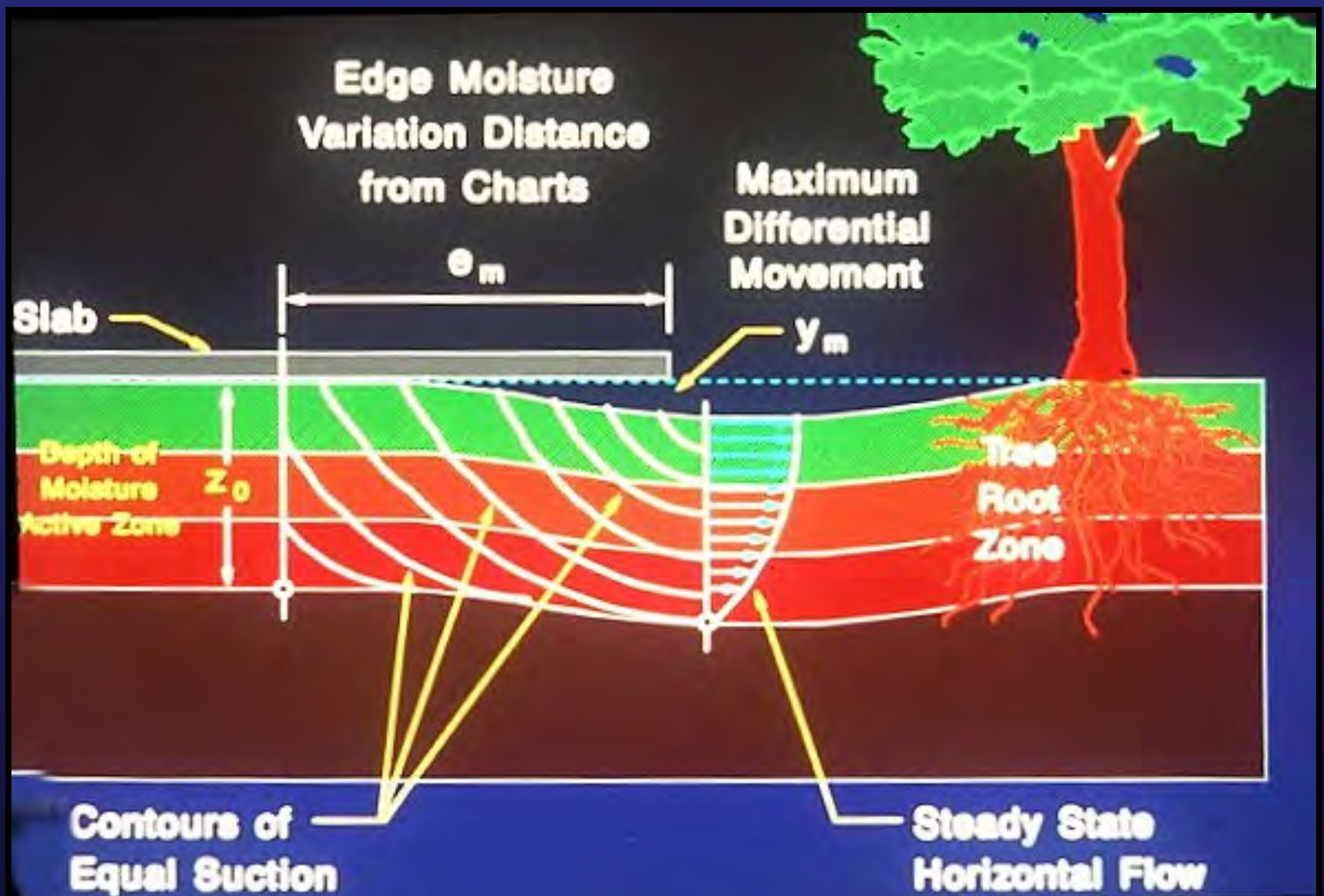
As determined by site conditions
- Costs

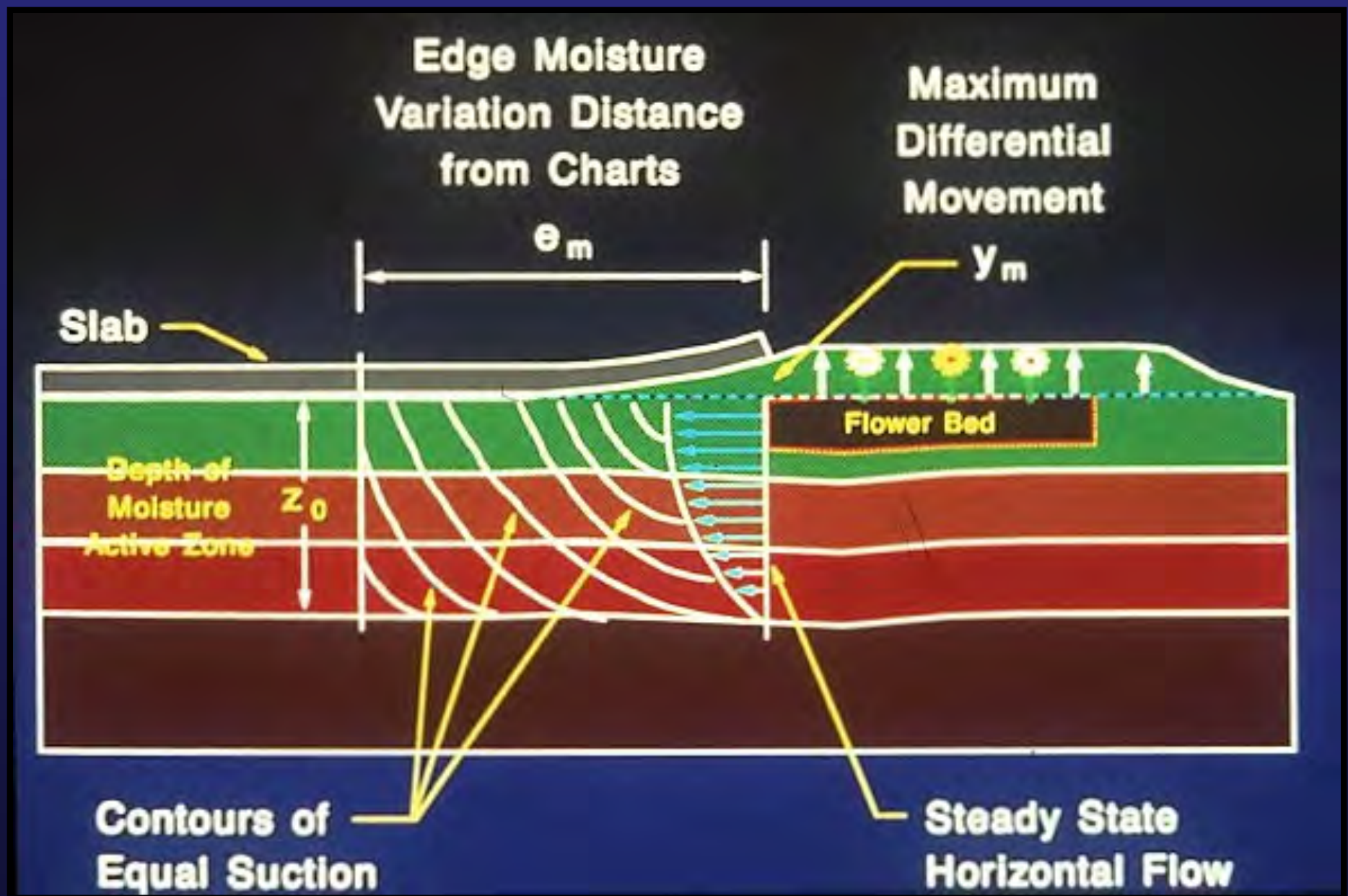
Site Conditions

- Soils
- Site hazards
 - Trees
 - Slopes
 - Drainage
- Building geometry

Slabs-on-Ground: Soils

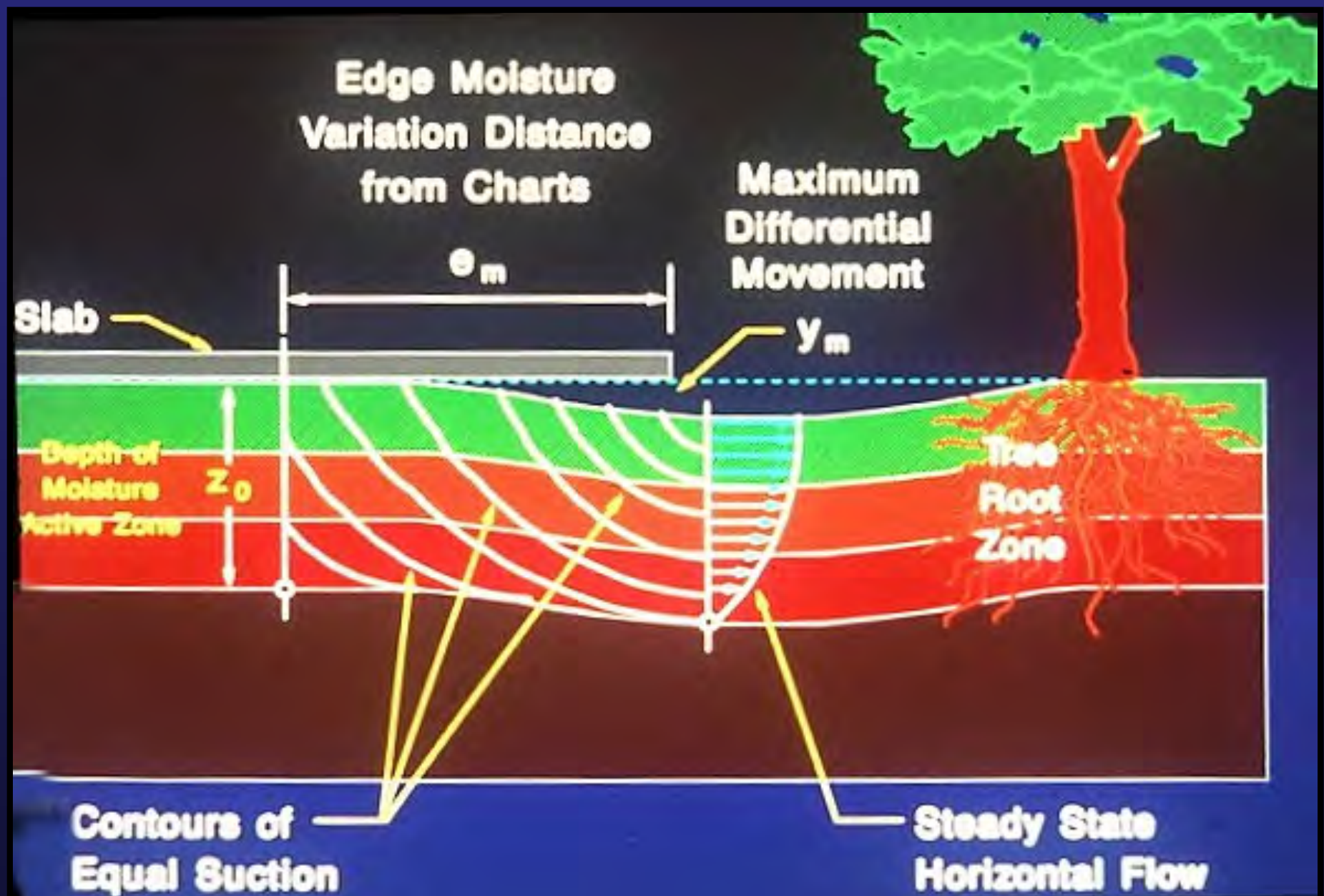
- y_m : differential movement of soil
 - Perimeter swelling
 - Perimeter shrinking
 - Center swelling
 - Center shrinking

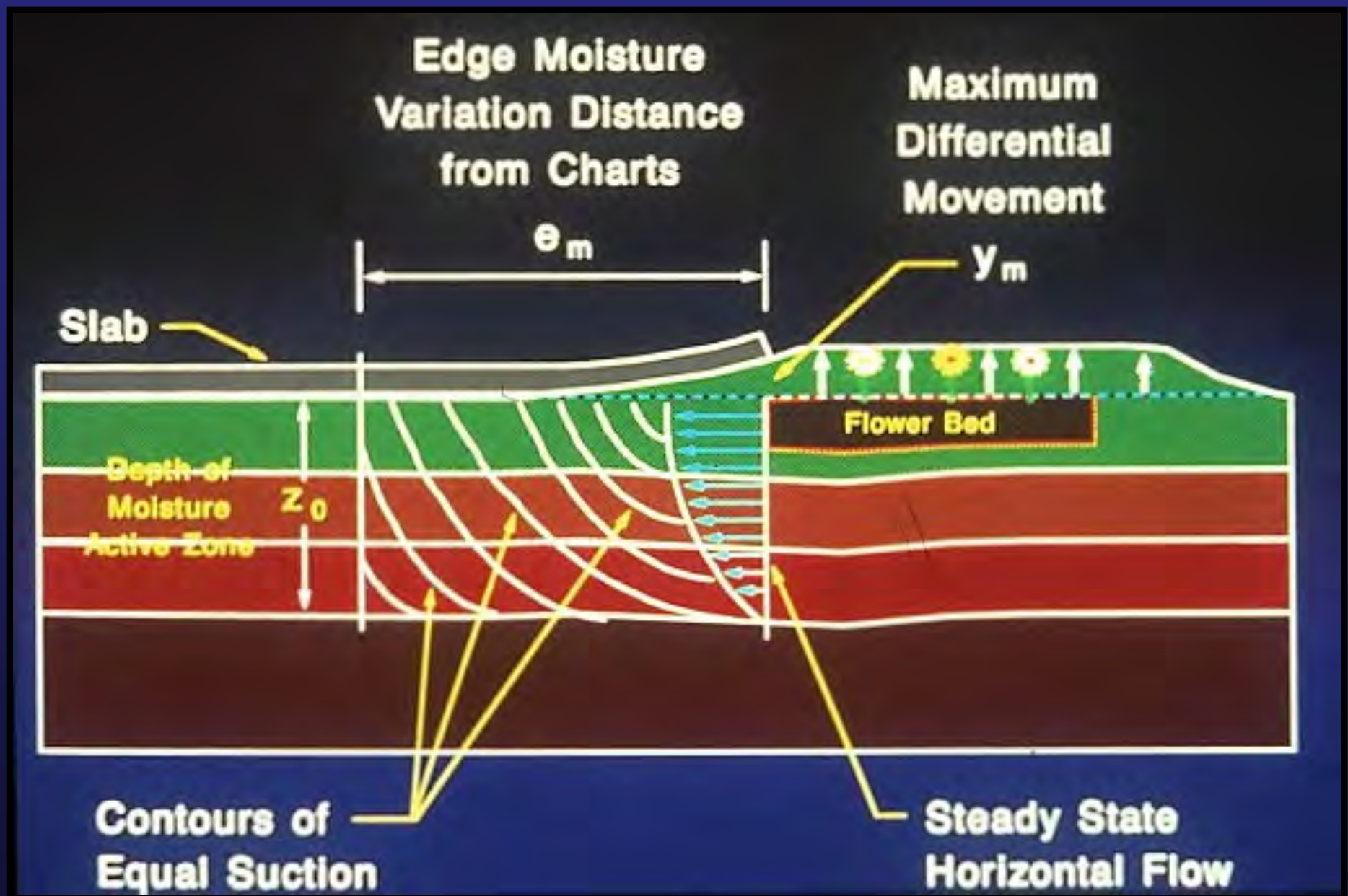




Slabs-on-Ground: Soils

- e_m : edge moisture variation distance
 - Not a cantilever distance
 - A property of the soil mass
 - Depends on soil activity and cracking



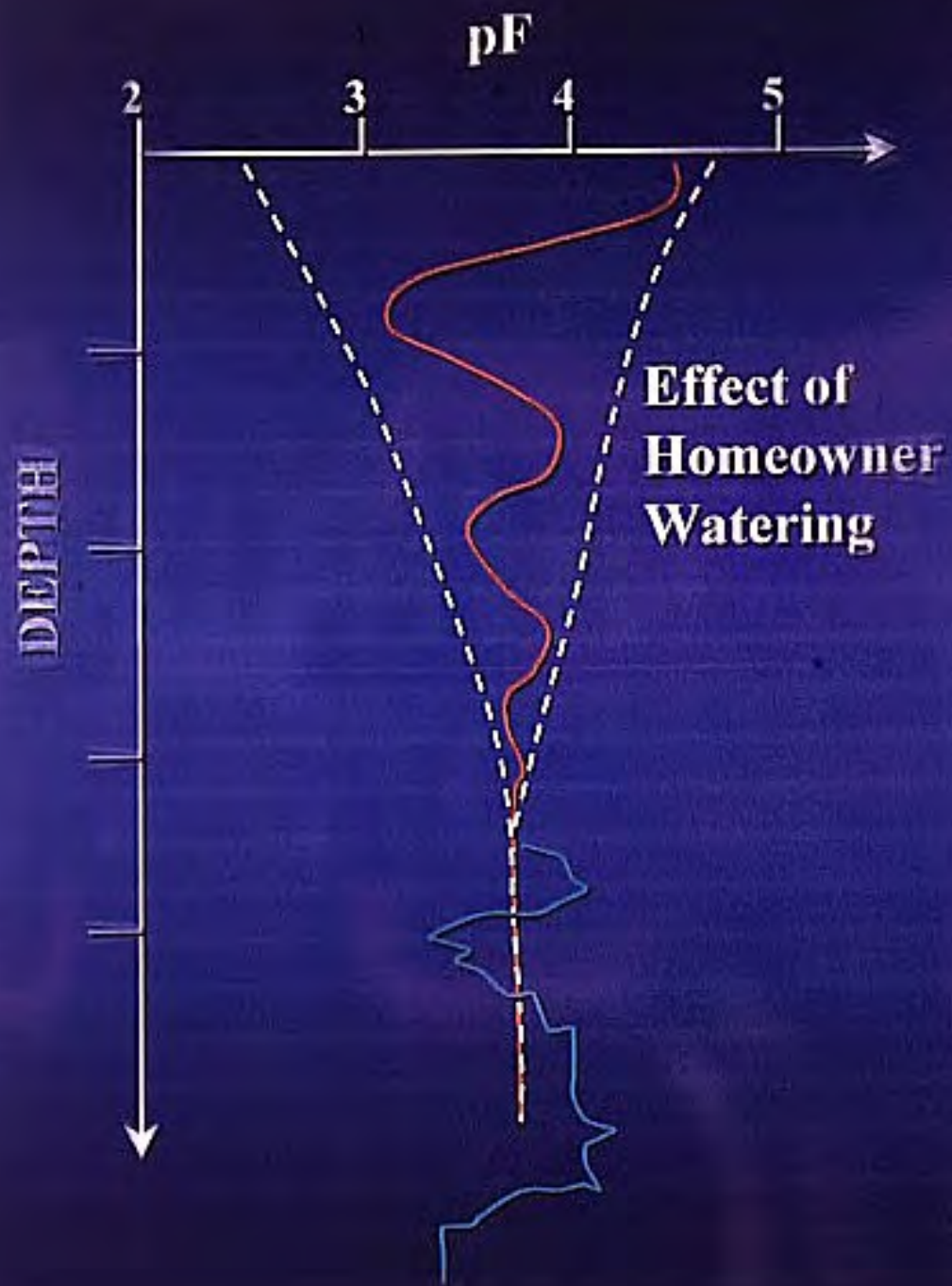


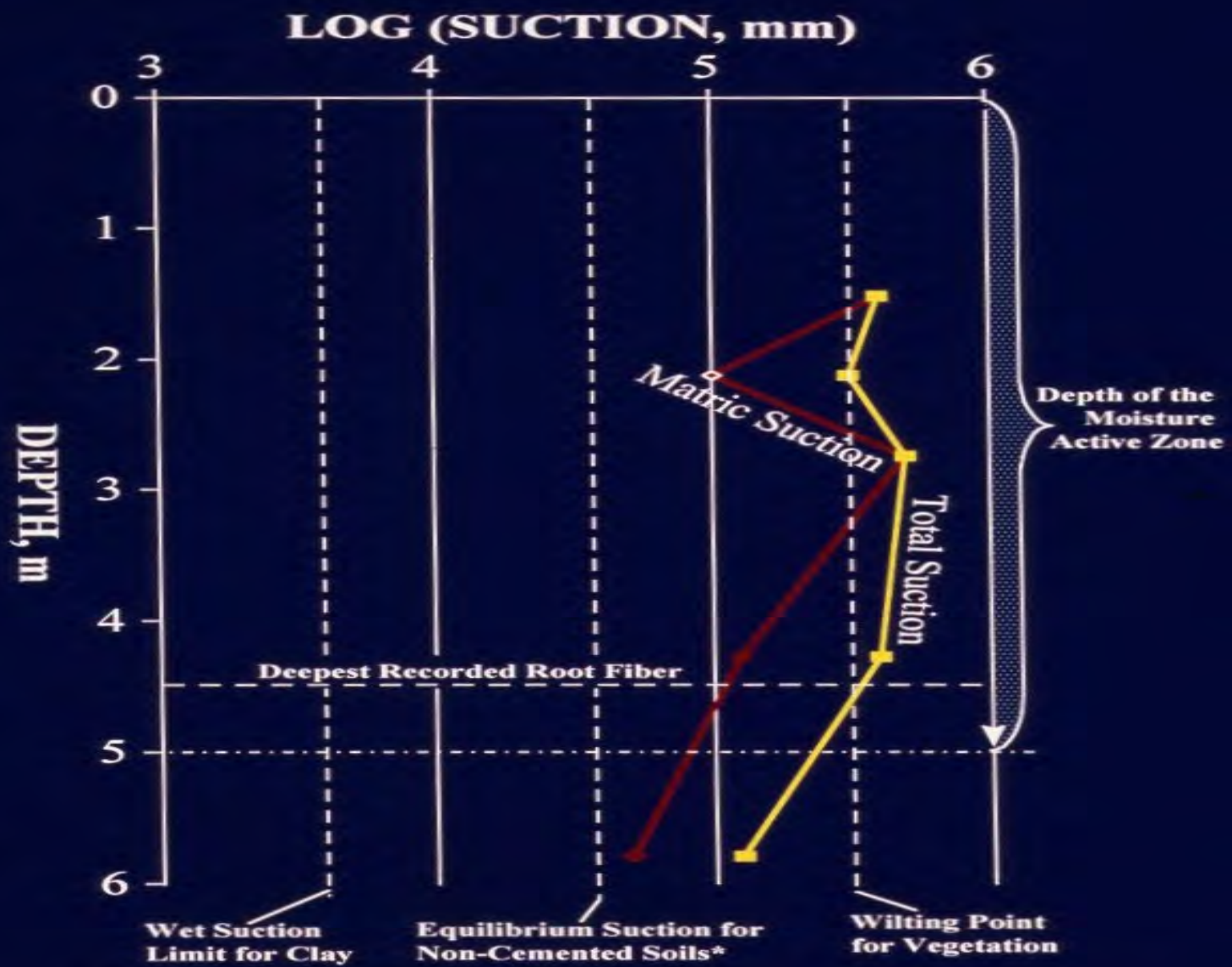


Slabs-on-Ground: Soils

- z_m : depth of the moisture active zone
 - Depth of shrinkage cracks created by roots (log for root fibers)
 - No deeper than soil at the wilting point of plants







* From Empirical Relation of Thornthwaite Moisture Index with equilibrium suction (Russam and Coleman, 1961)

Slabs-on-Ground: Soils

- z_A : depth of the movement active zone
 - Always shallower than z_m
 - Large factor in y_m

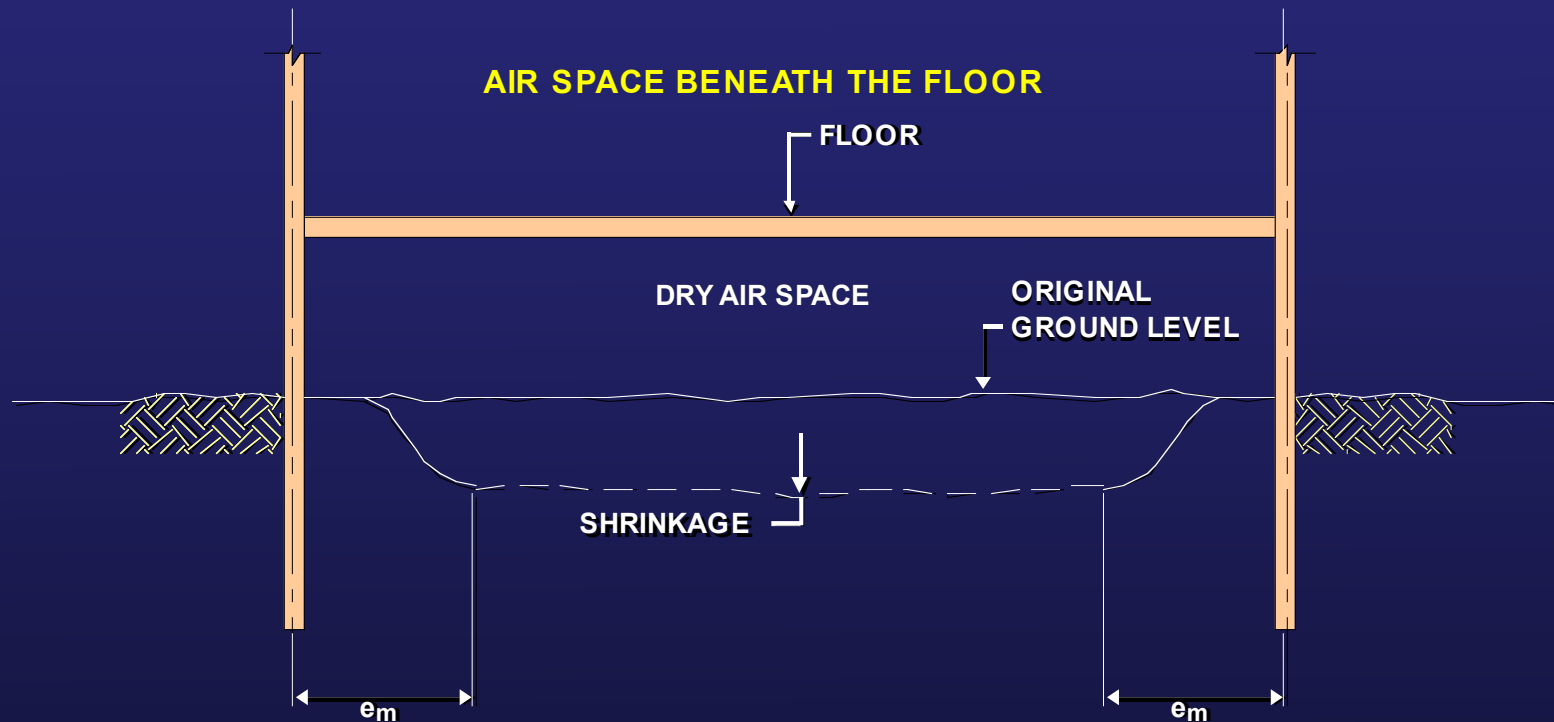




Raised Floor Foundations: Soils

- y_m : differential movement
 - Center drying, total shrinkage
 - Perimeter total swelling
 - Drainage
 - Flower beds
 - Perimeter total shrinking: trees
 - Downhill creep

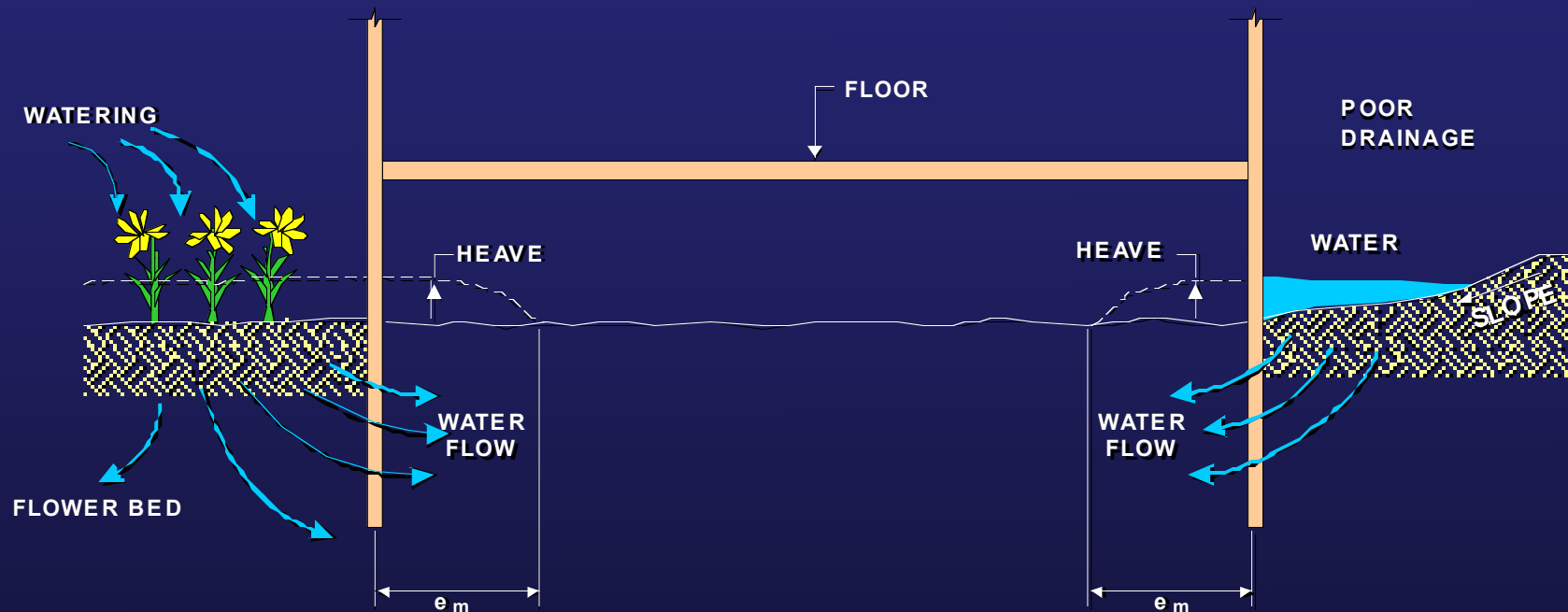
TOTAL MOVEMENT PATTERNS WITH RAISED WOOD FLOOR FOUNDATIONS



NOTE

AMOUNT OF SHRINKAGE DEPENDS ON THE LEVEL OF RELATIVE HUMIDITY IN THE AIR BENEATH THE FLOOR. THE LOWER THE RELATIVE HUMIDITY, THE GREATER WILL BE THE AMOUNT OF SHRINKAGE. INITIALLY, THE SOIL WILL BE AT OR ABOVE 98% RELATIVE HUMIDITY. e_m IS THE EDGE MOISTURE VARIATION DISTANCE WHICH VARIES TYPICALLY BETWEEN 3 AND 9 FEET DEPENDING ON THE TYPE OF SOIL.

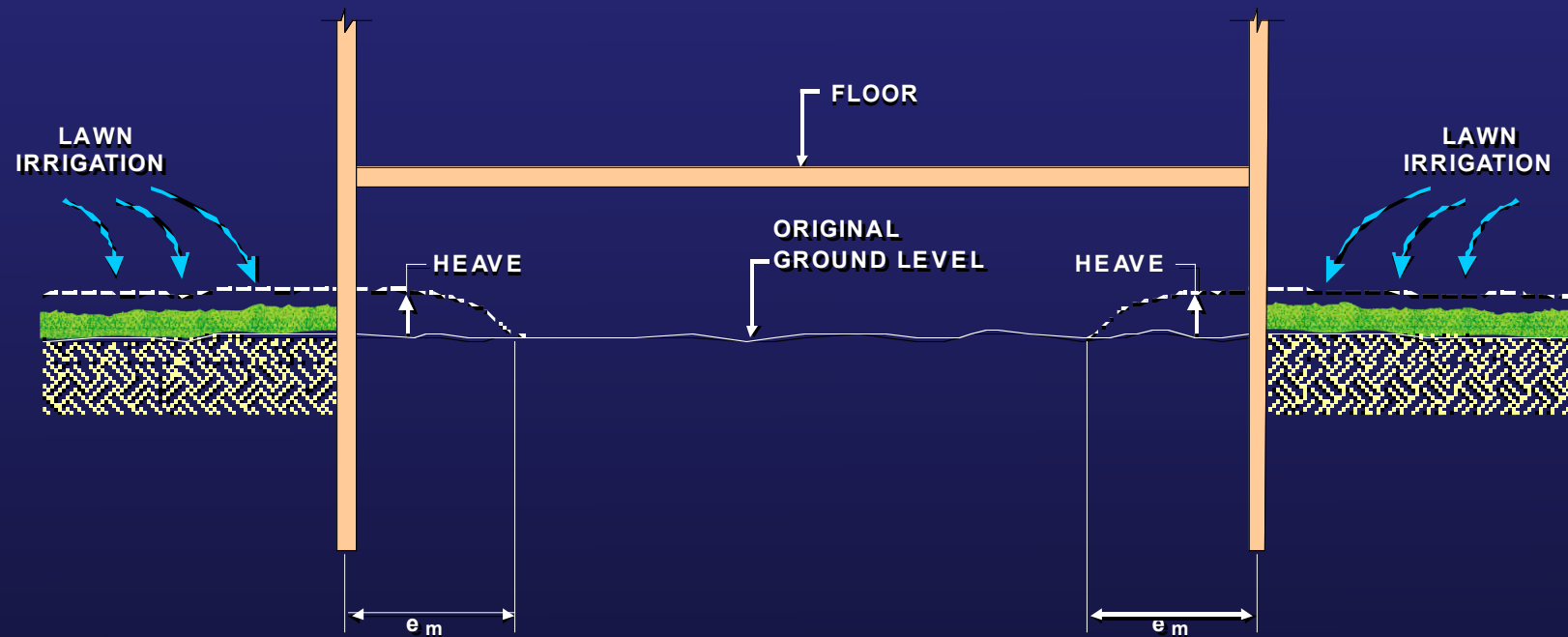
VERTICAL AND HORIZONTAL MOISTURE BARRIERS



NOTE

AMOUNT OF HEAVE DEPENDS ON THE AMOUNT OF WATER THAT IS MADE AVAILABLE TO THE SOIL AT THE EDGE OF THE BUILDING AND THE TYPE OF SOIL. e_m IS THE EDGE MOISTURE VARIATION DISTANCE WHICH VARIES TYPICALLY BETWEEN 3 AND 9 FEET DEPENDING ON THE TYPE OF SOIL.

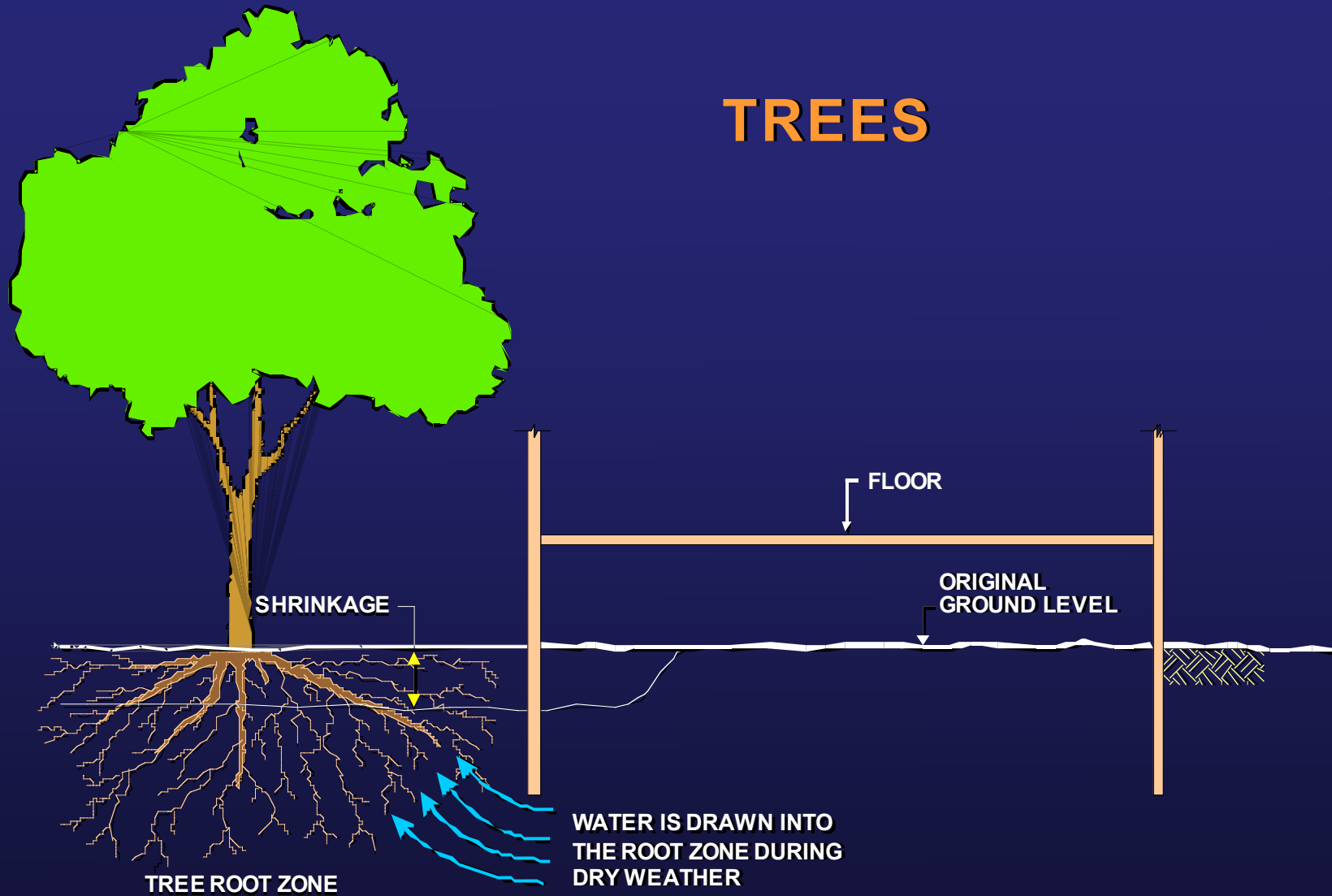
LAWN IRRIGATION



NOTE

AMOUNT OF HEAVE DEPENDS ON FREQUENCY OF LAWN IRRIGATION AND TYPE OF SOIL. e_m IS THE EDGE MOISTURE VARIATION DISTANCE WHICH VARIES TYPICALLY BETWEEN 3 AND 9 FEET DEPENDING ON THE TYPE OF SOIL.

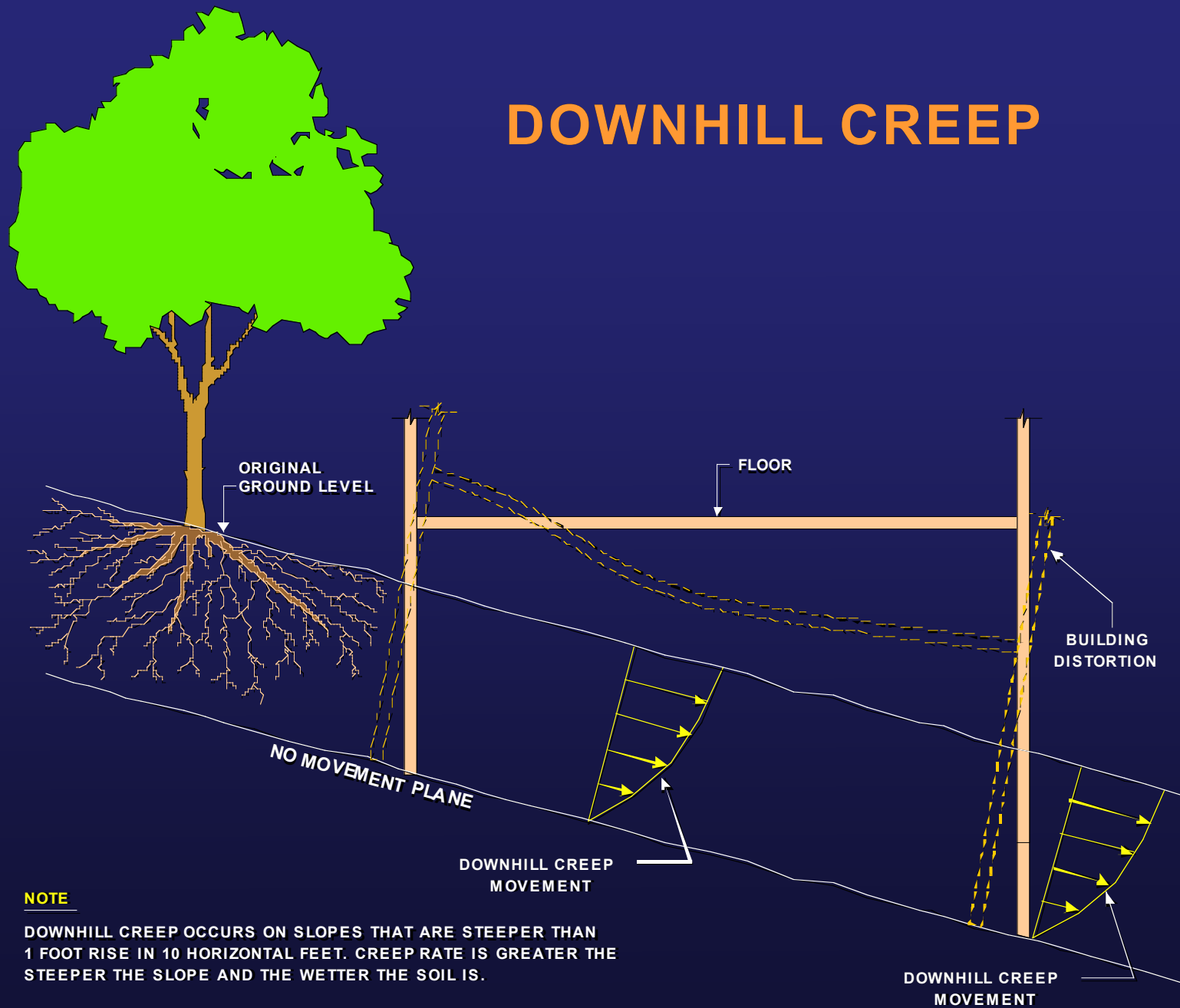
TREES



NOTE

AMOUNT OF SHRINKAGE DEPENDS ON THE DEPTH OF THE TREE ROOT ZONE, HOW FAR THE ROOTS PENETRATE BENEATH THE BUILDING, AND THE TYPE OF SOIL.

DOWNHILL CREEP



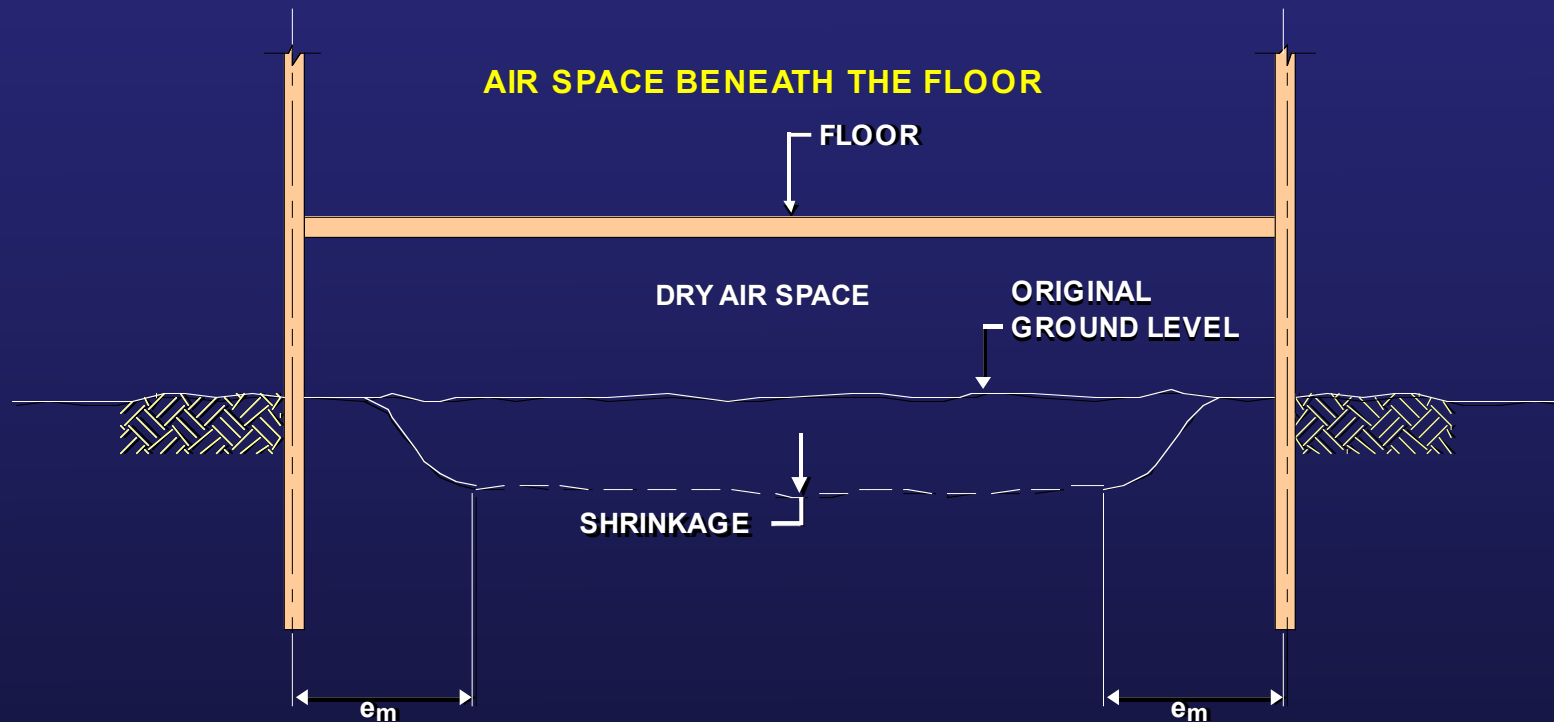
NOTE

DOWNHILL CREEP OCCURS ON SLOPES THAT ARE STEEPER THAN 1 FOOT RISE IN 10 HORIZONTAL FEET. CREEP RATE IS GREATER THE STEEPER THE SLOPE AND THE WETTER THE SOIL IS.

Raised Floor Foundations: Soils

- e_m : edge moisture variation distance
 - Not as important as with slabs on ground except around the perimeter

TOTAL MOVEMENT PATTERNS WITH RAISED WOOD FLOOR FOUNDATIONS

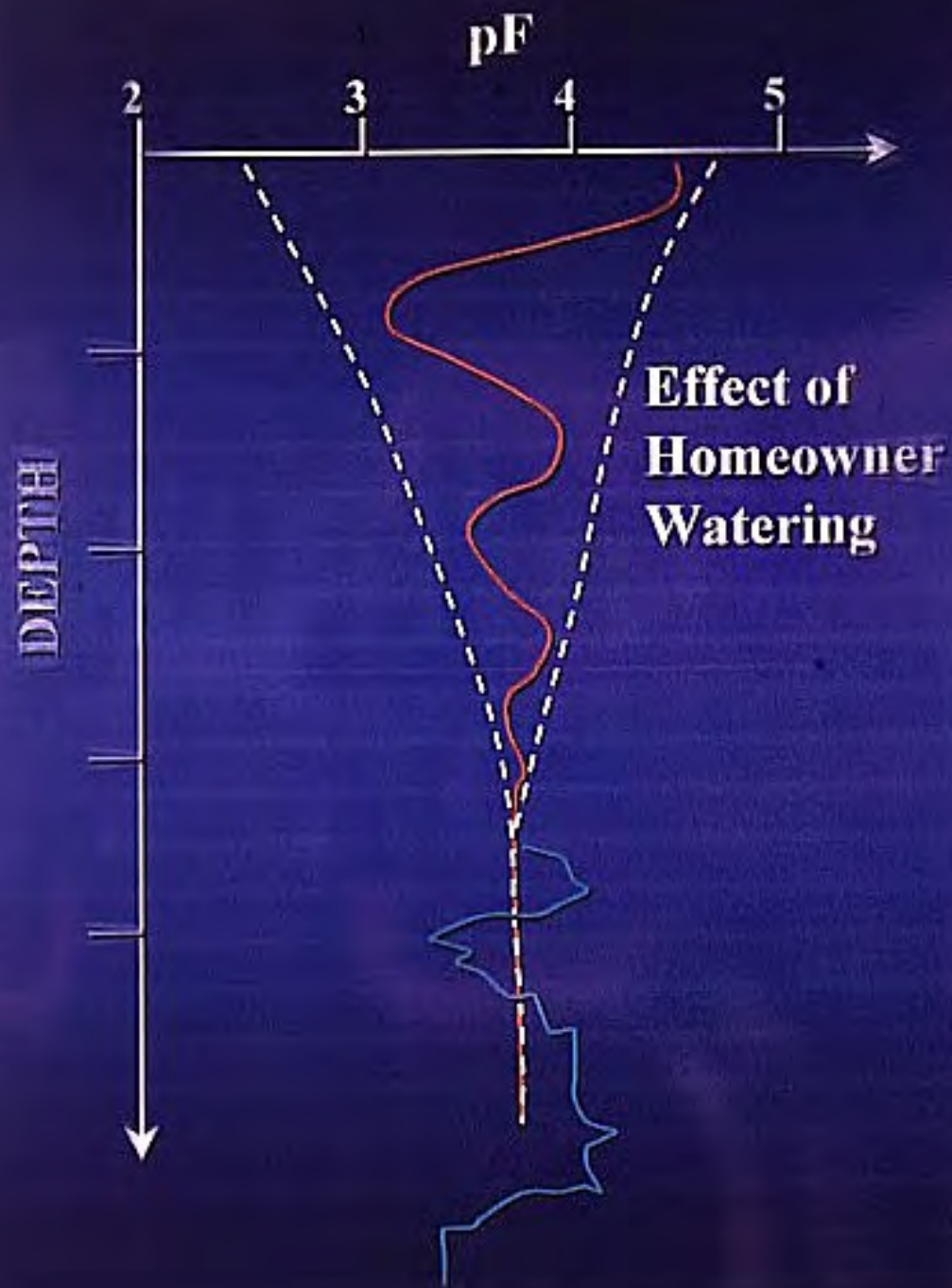


NOTE

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Raised Floor Foundations: Soils

- z_m : depth of the moisture active zone
 - Same factors as with slab on ground
 - Interest is in the total movement



Raised Floor Foundations: Soils

- z_A : depth of movement active zone
 - Important to determine movement of supports
 - Pads
 - Spread footings
 - Posts
 - Piers
- Objective: design for expected movement
- Objective: small support movement
- Which to use? Determined by costs

Slab-on-Ground: Site Hazards

- Trees
 - Shrinkage
 - Affects z_m , z_A , e_m , y_m
- Slopes
 - Like differential shrinkage
 - Rate depends on moisture
 - Affects z_m , y_m
- Drainage
 - Swelling
 - Affects e_m , y_m

Raised Floor Foundations: Site Hazards

- Trees: shrinkage reduces total differential movement
- Slopes
 - Like differential shrinkage
 - Rate depends on moisture
 - Affects z_m , y_m
- Drainage
 - Swelling
 - Increases total differential movement
 - Affects y_m

Slab-on-Ground: Building Geometry

- Shape factor affects structural design quantities
 - Moment
 - Shear
 - Differential deflection

- Shape factor

$$\frac{(\text{Perimeter})^2}{\text{Area}} \leq 24$$

- Circle = 12.56
- Square = 16
- Rectangle = $3.7 \sim 1 \implies \text{SF} = 24$

Raised Floor Foundations: Building Geometry

With adjustable floor elevation, does not matter





Slab-on-Ground: Structural Requirements

This is a soil-structure interaction problem.

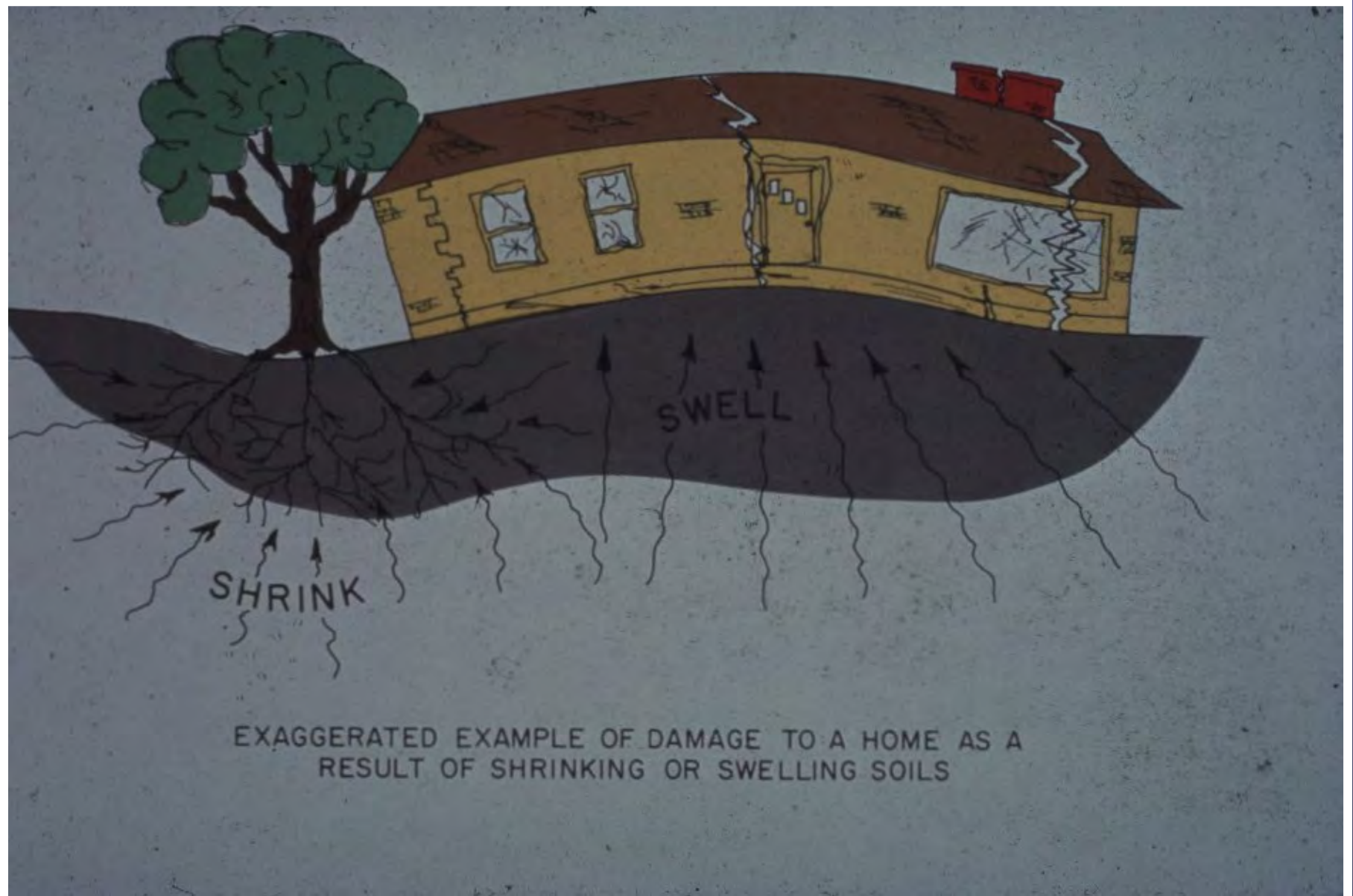
- Soil is not a uniform pressure
- e_m is not a cantilever distance
- Structural properties of slab and soil are creep (long-term) properties

Slab-on-Ground: Structural Requirements

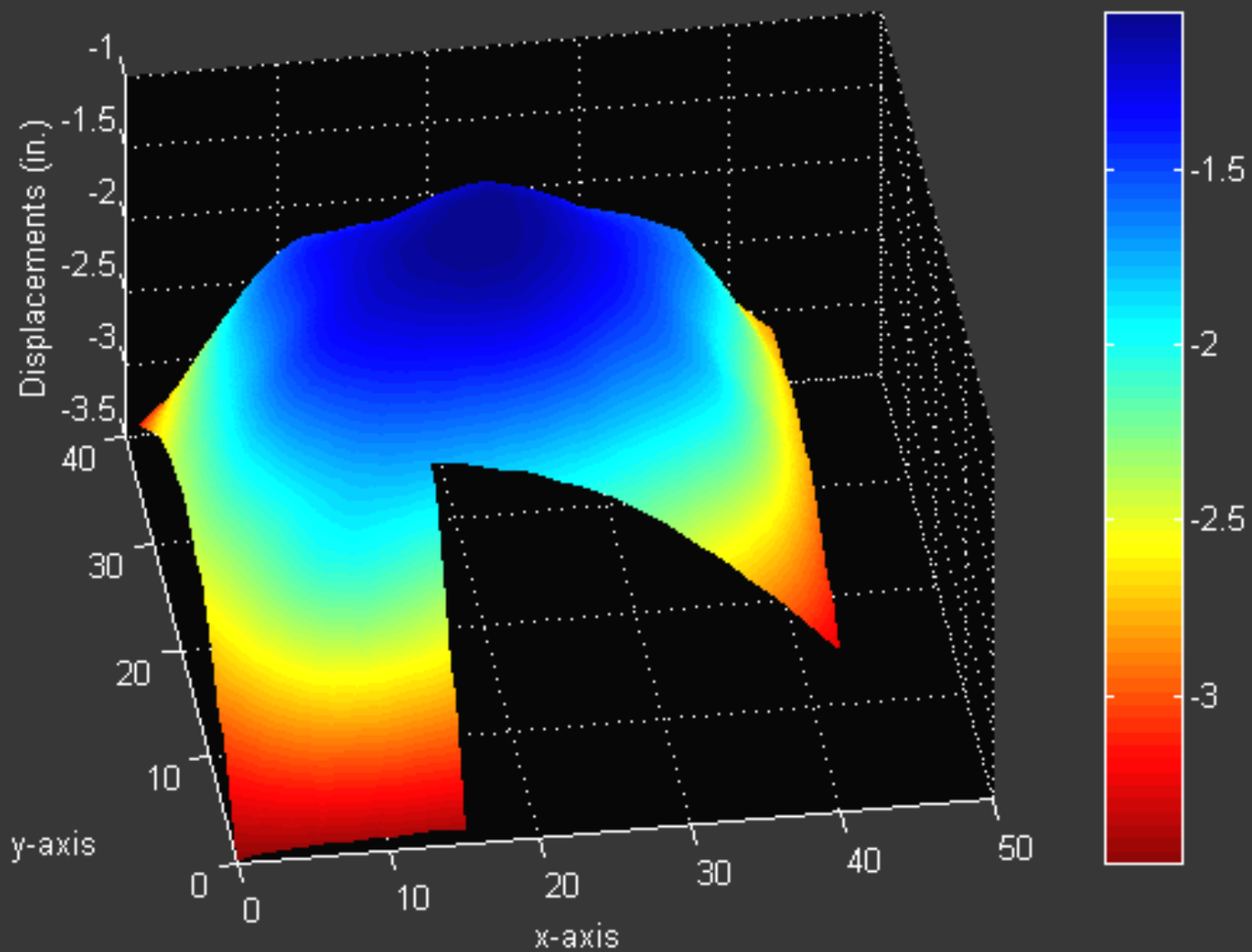
- Ground pressures never come close to bearing capacity
- z_m is dictated by site conditions and not by regional conditions
- y_m for both edge shrinking and edge swelling (> 1 inch) must be estimated accurately

Slab-on-Ground: Structural Requirements

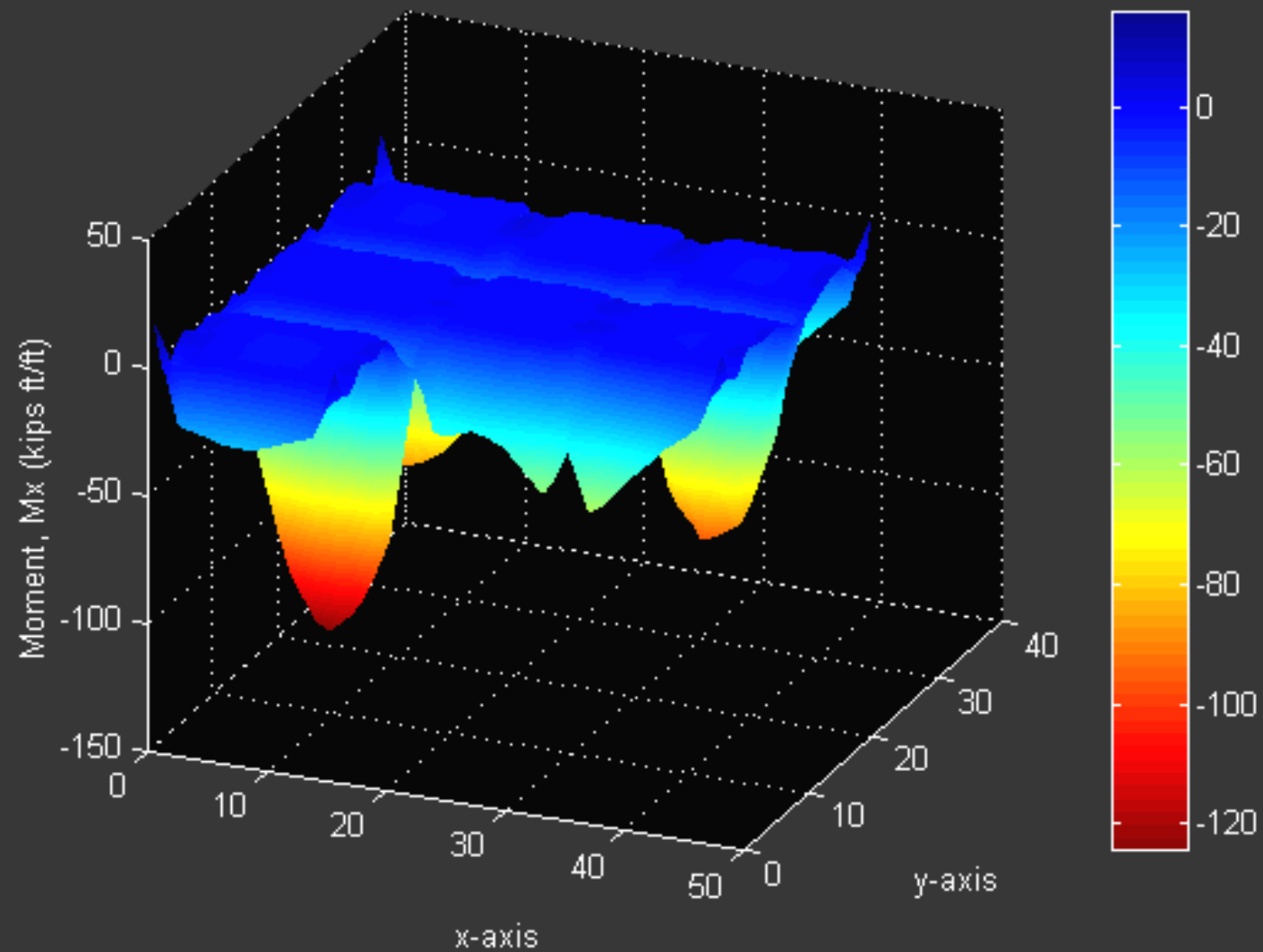
- e_m : for both edge shrinking and edge swelling is the most sensitive predictor of design moments, shears, and required stiffness, EI.
- z_A : is smaller than z_m and is dictated by site conditions and not by regional conditions



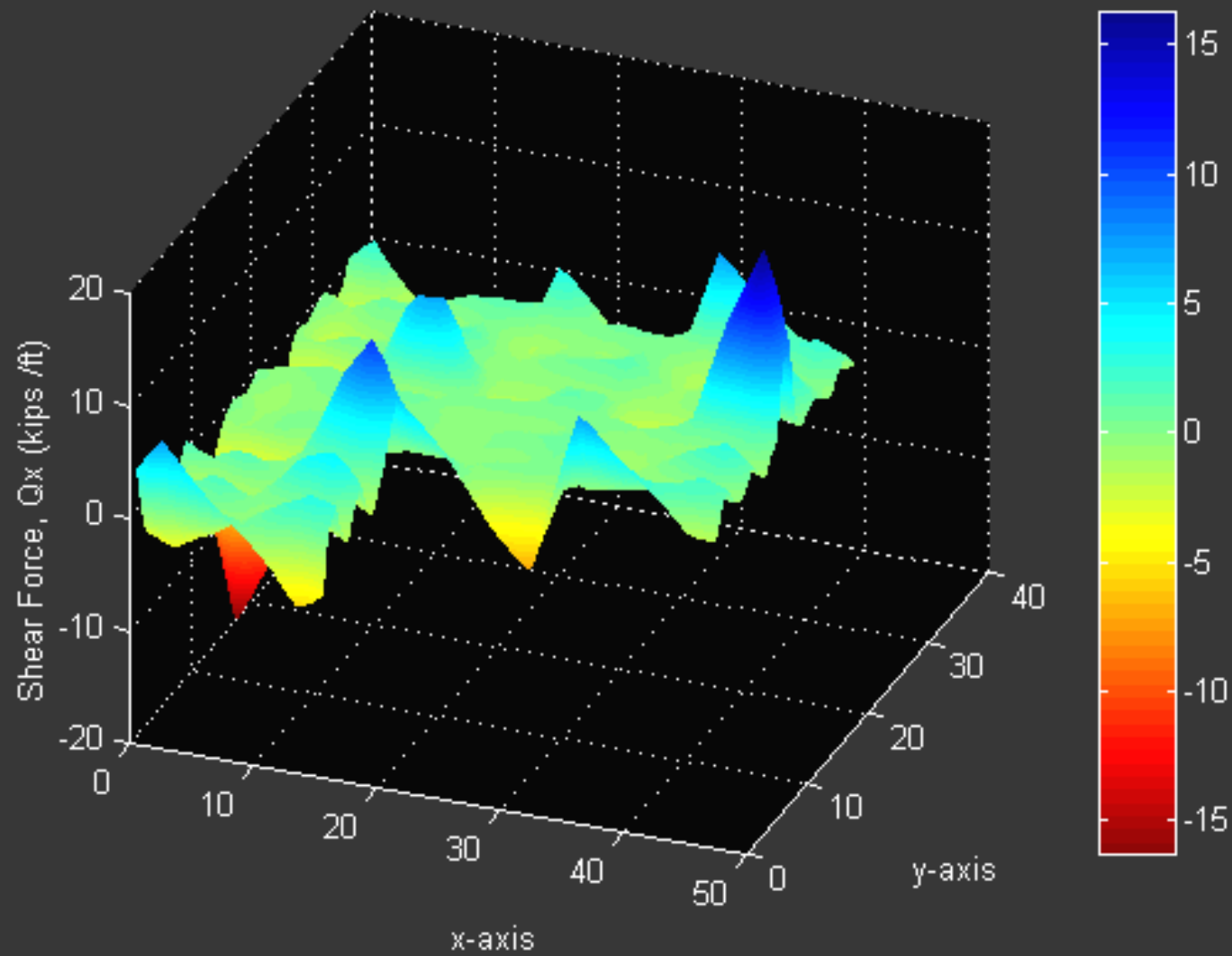
Example 1: Center Lift ($e_m=5.5\text{ft}$, $y_m=3.608\text{in.}$), Displacements (in.)



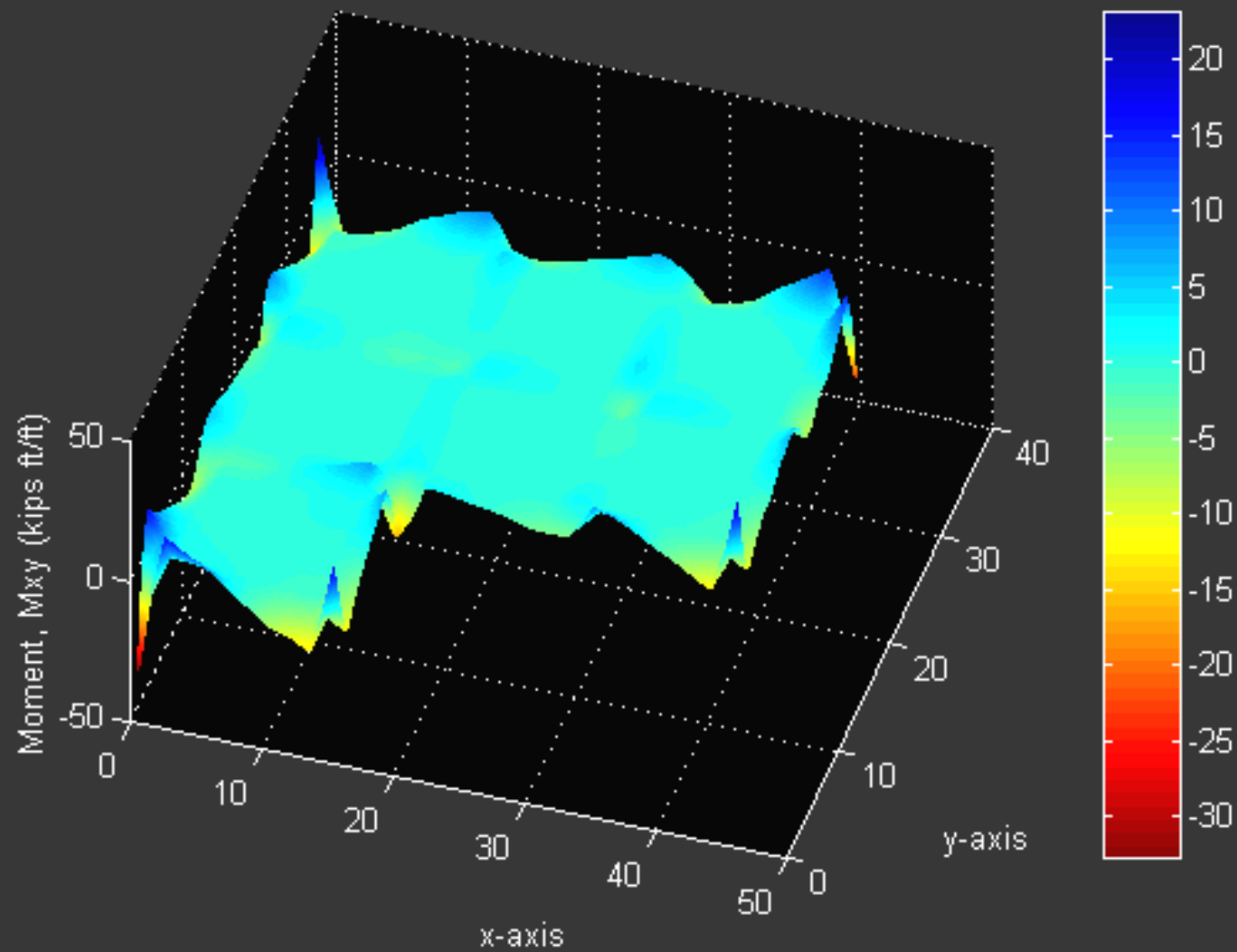
Example 1: Center Lift ($e_m=5.5\text{ft}$, $y_m=3.608\text{in.}$), Moment, M_x (kips ft/ft)



Example 1: Center Lift ($x_m=5.5\text{ft}$, $y_m=3.608\text{in.}$), Shear Force, Q_x (kips /ft)

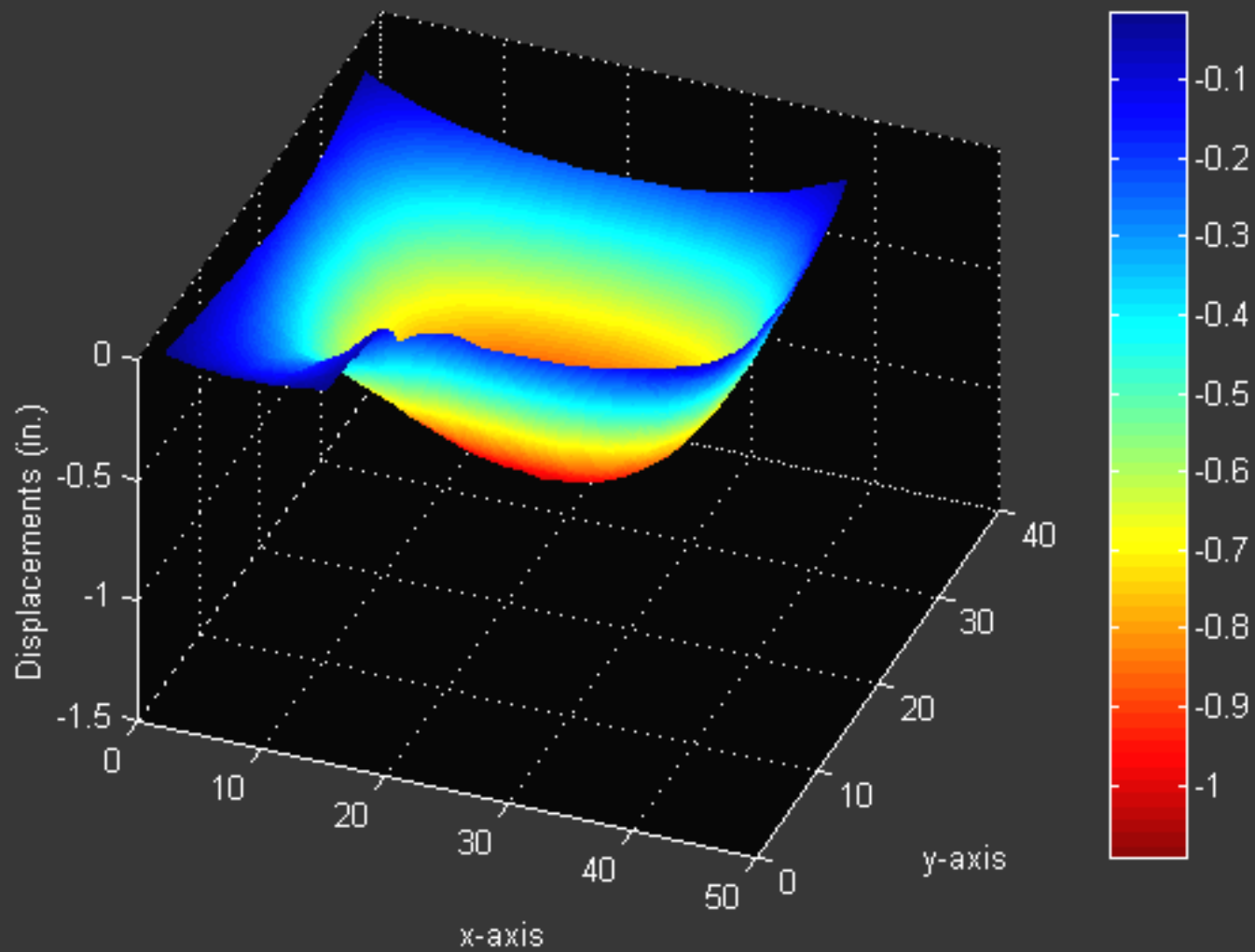


Example 1: Center Lift ($x_m=5.5\text{ft}$, $y_m=3.608\text{in.}$), Moment, M_{xy} (kips ft/ft)

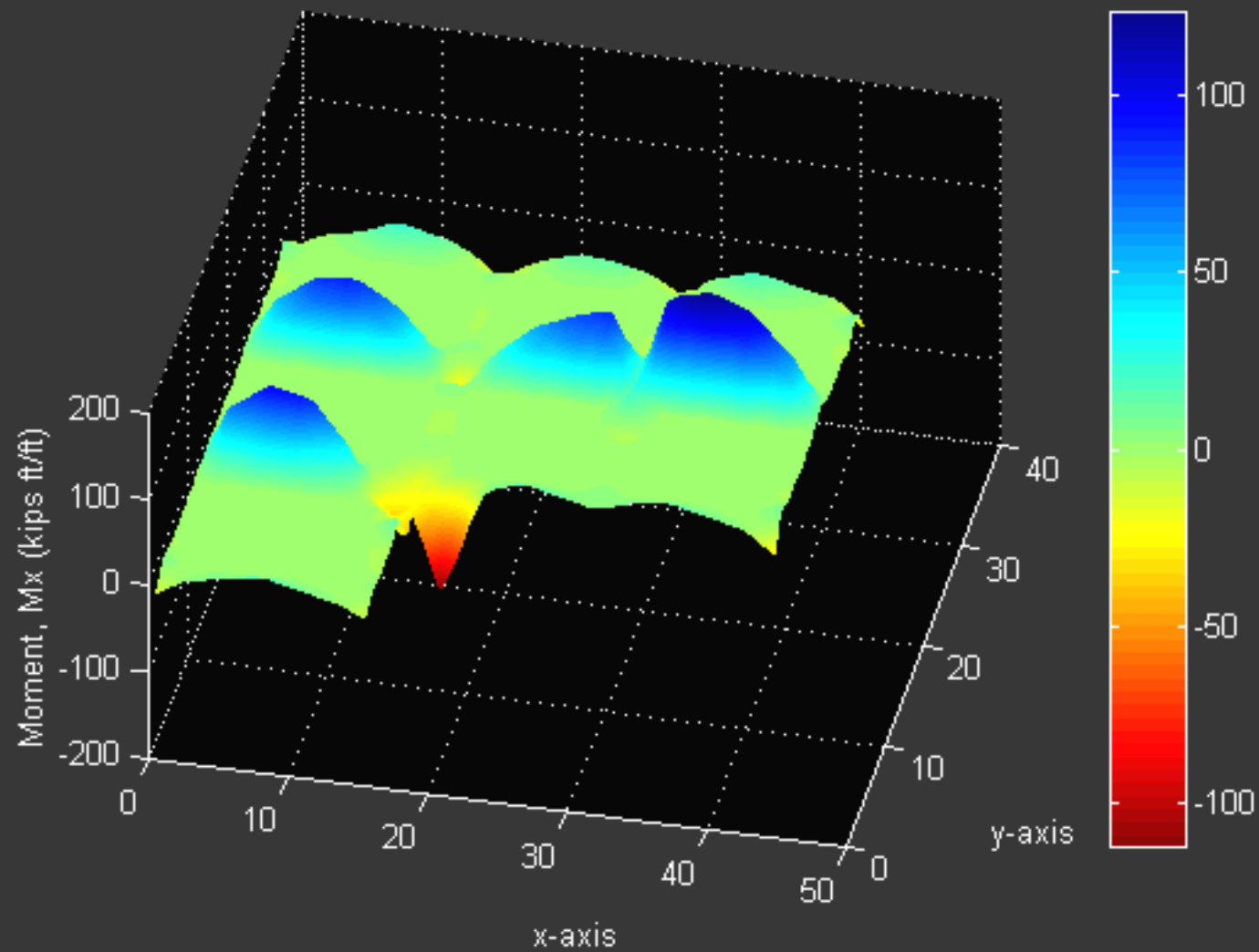




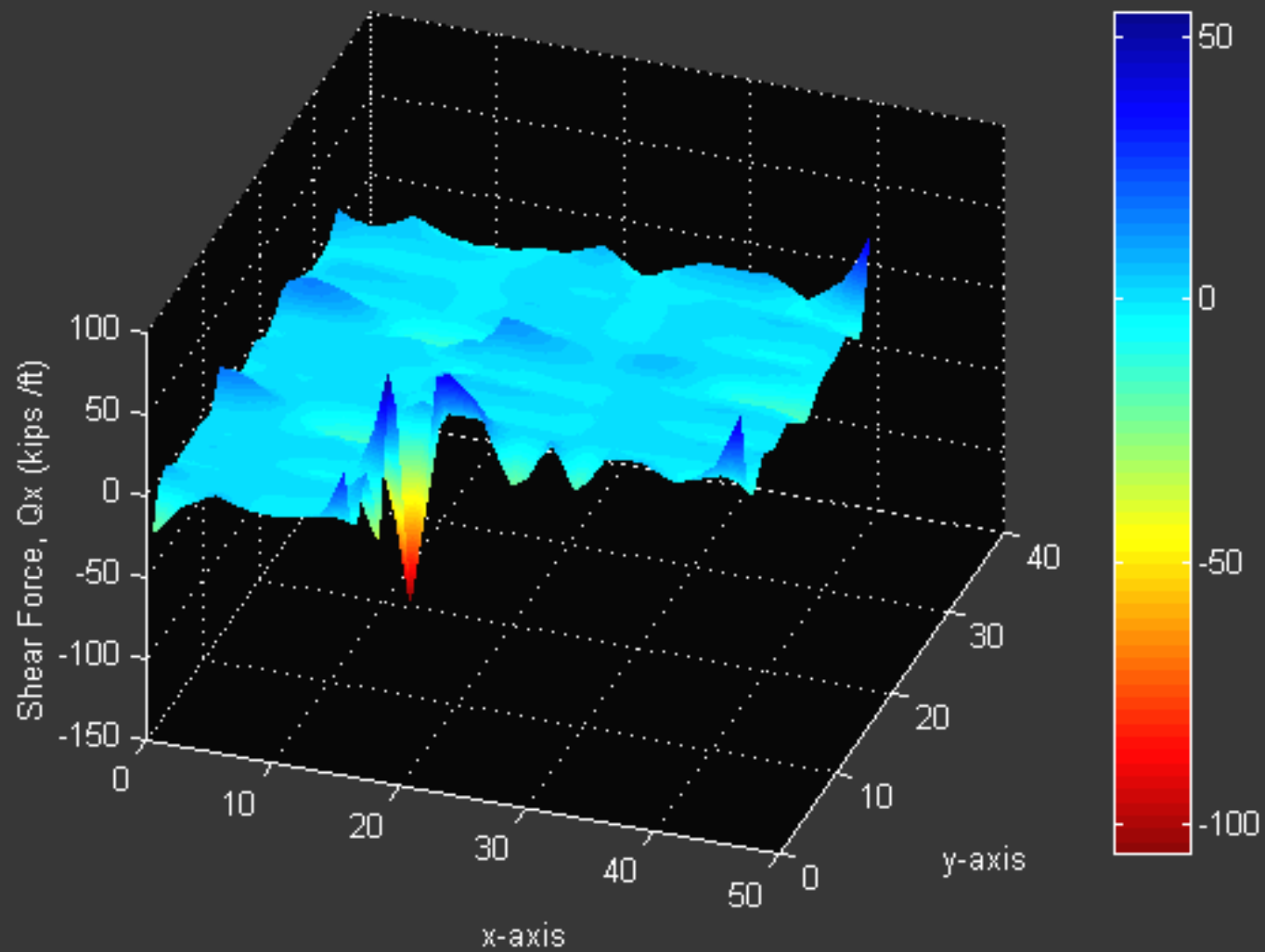
Example 1: Edge Lift, ($e_m=2.5\text{ft}$, $y_m=0.752\text{in.}$), Displacements (in.), (CT)



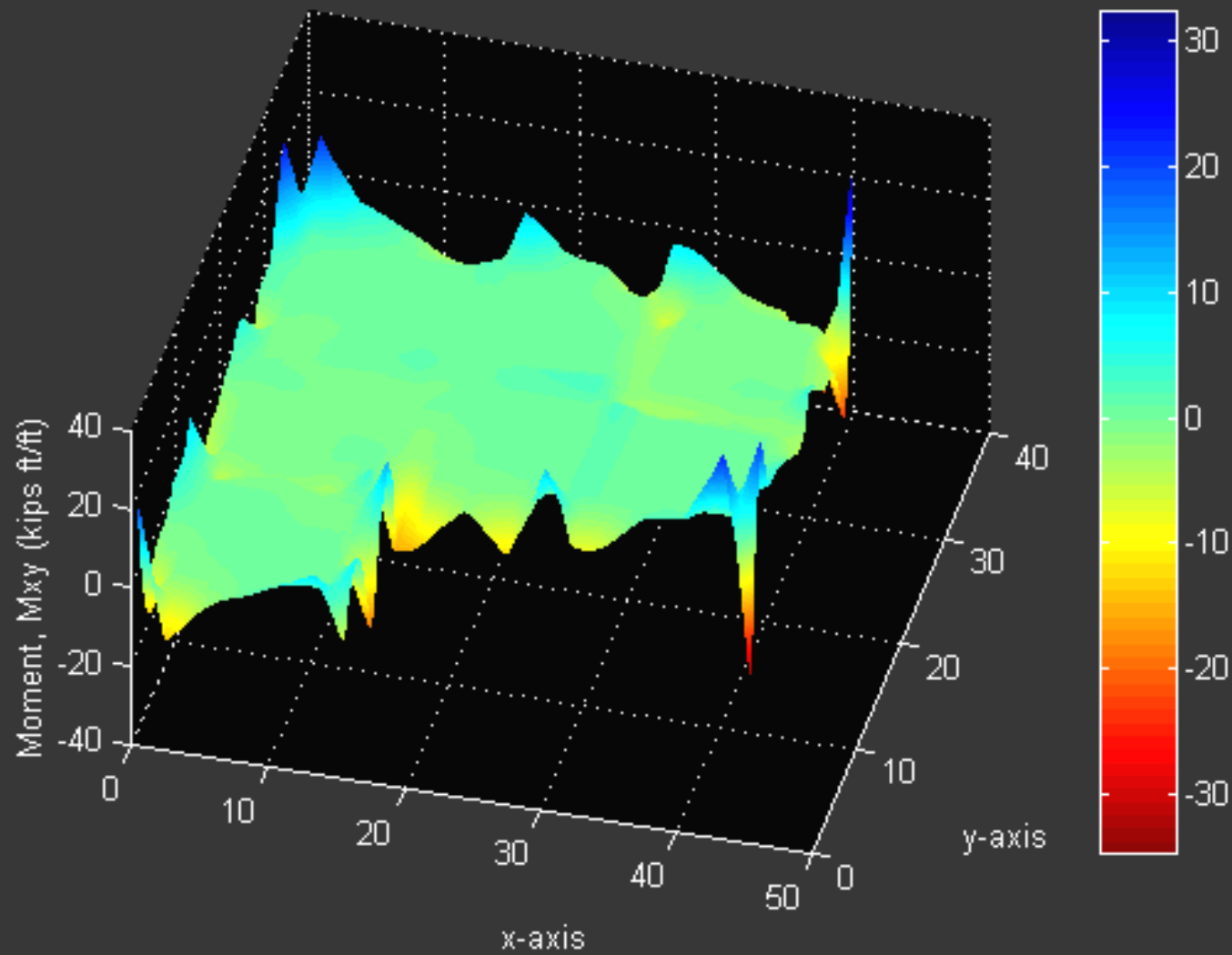
Example 1: Edge Lift ($e_m=2.5\text{ft}$, $y_m=0.752\text{in.}$), Moment, M_x (kips ft/ft)



Example 1: Edge Lift ($e_m=2.5\text{ft}$, $y_m=0.752\text{in.}$), Shear Force, Q_x (kips /ft)



Example 1: Edge Lift ($e_m=2.5\text{ft}$, $y_m=0.752\text{in.}$), Moment, M_{xy} (kips ft/ft)



Slab-on-Ground: Structural Requirements

- β – length = relative stiffness length

$$= \frac{1}{12} \sqrt[4]{\frac{E_c I}{E_s}} \quad \begin{array}{l} E_c = \text{creep stiffness of concrete} \\ E_s = \text{creep stiffness of soil} \end{array}$$

- Dictates what is a long- and short-slab ($> 6\beta$ is long)
- Controls design quantities for long slabs

Design Criteria: Deflections / Tolerance

- Sensitivity of foundation and super structure (Δ/L)
- Differential ($\Delta_c + \Delta_s$)
 - As built (Δ_c)
 - Soil movement (Δ_s)
- Total
- Twisting

Design Criteria: Stiffness

- Substitute for deflection tolerance
- Enough concrete section to handle soil movement

Raised Floor Foundations: Structural Requirements

This is NOT a soil-structure interaction problem.

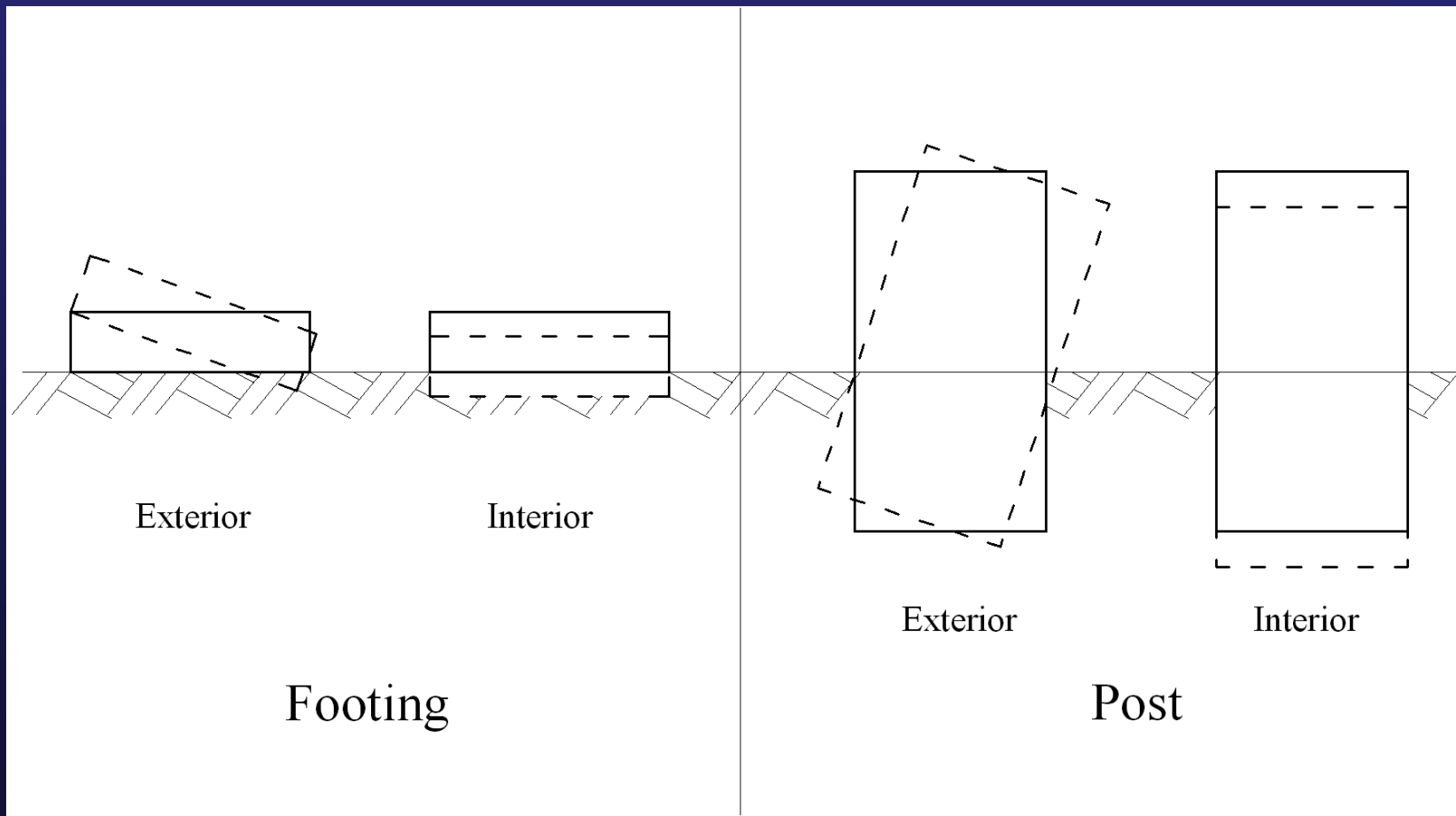
- Moment
 - Shear
 - Deflection
- 
- criteria

are the same as for column-supported structures.

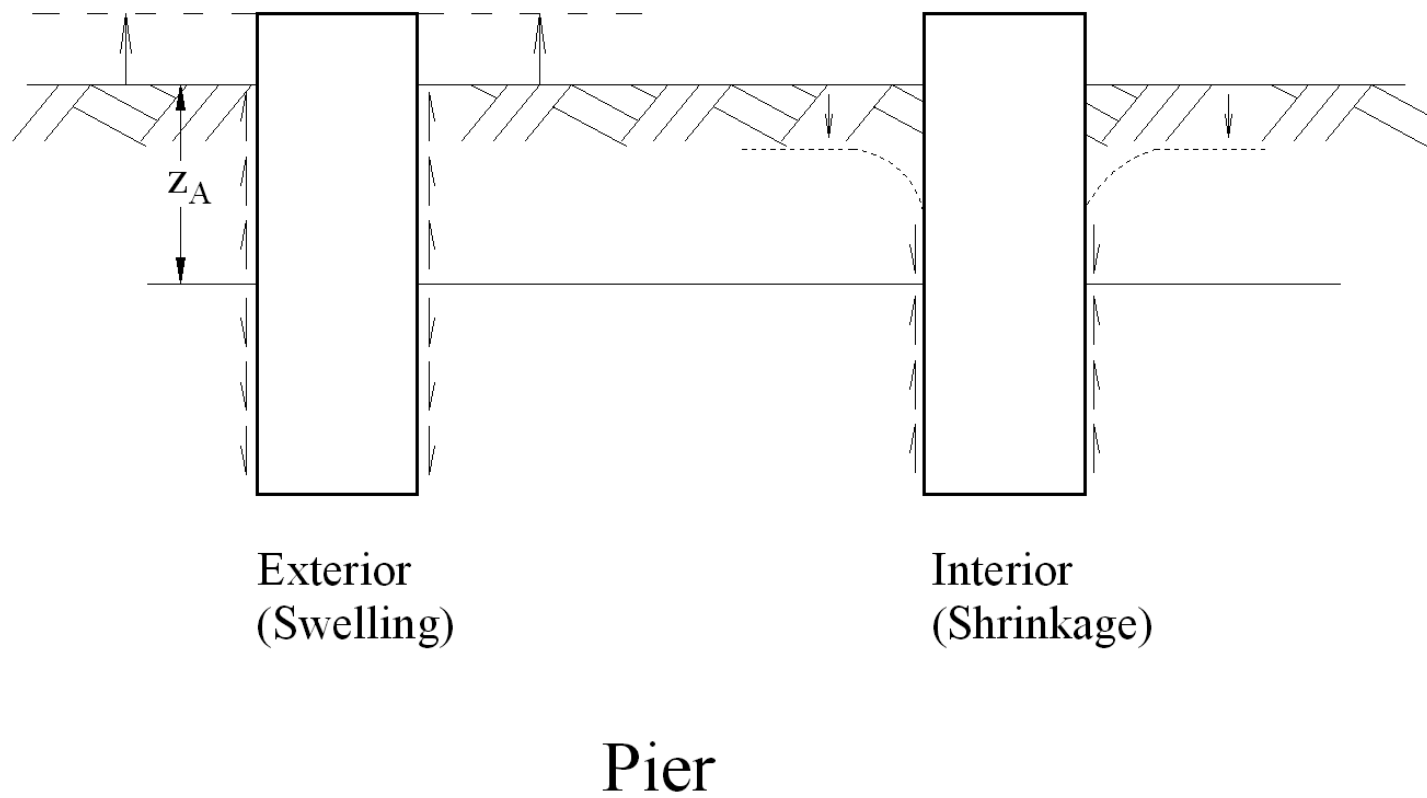
Raised Floor Foundations: Structural Requirements

- Allowable deflections before adjusting support elevations dictate the design quantities of the floor supports
- Design of supporting footings, posts or piers is to make rough estimate of total movement
 - Vertical
 - Rotation

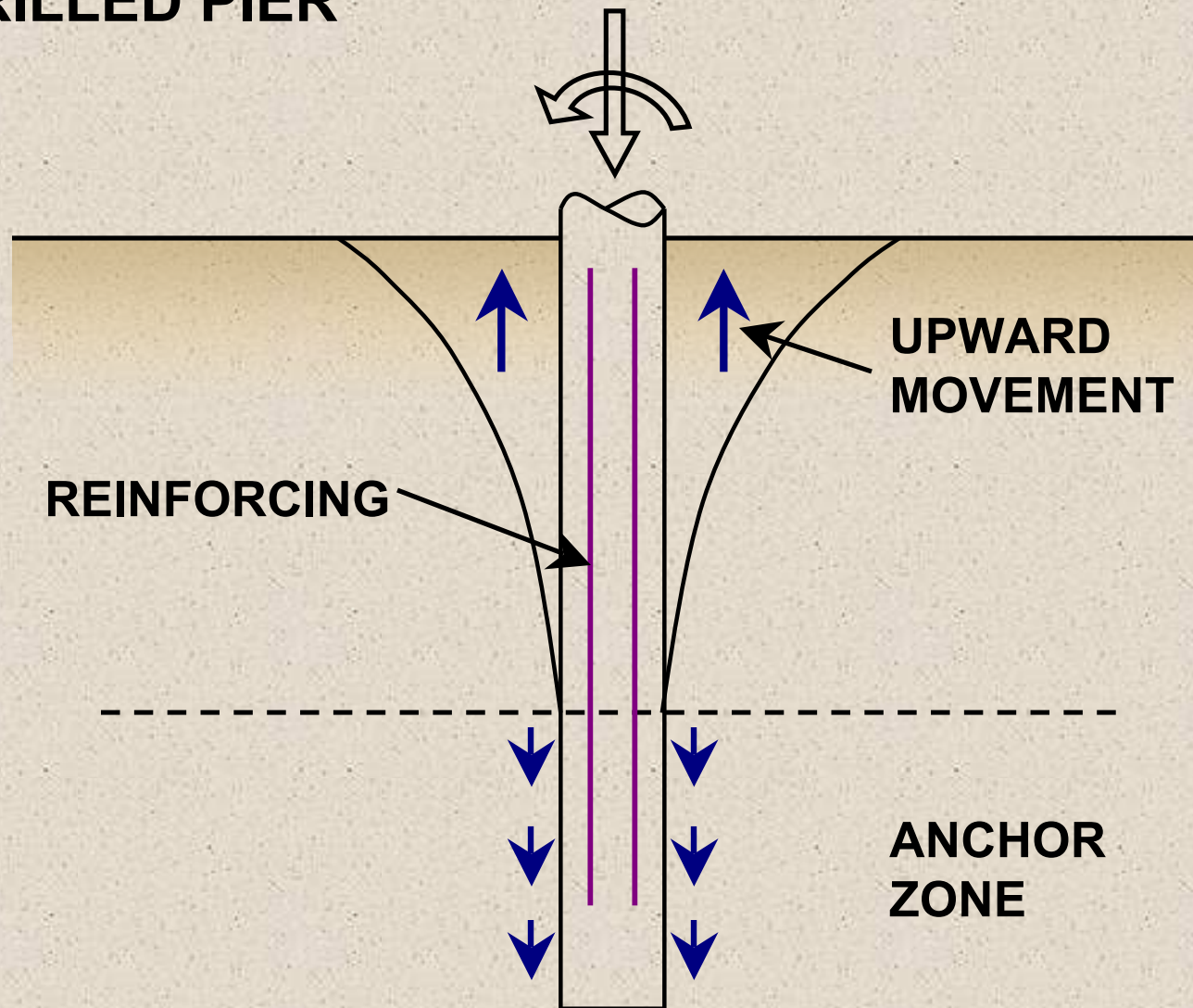
Movement Patterns



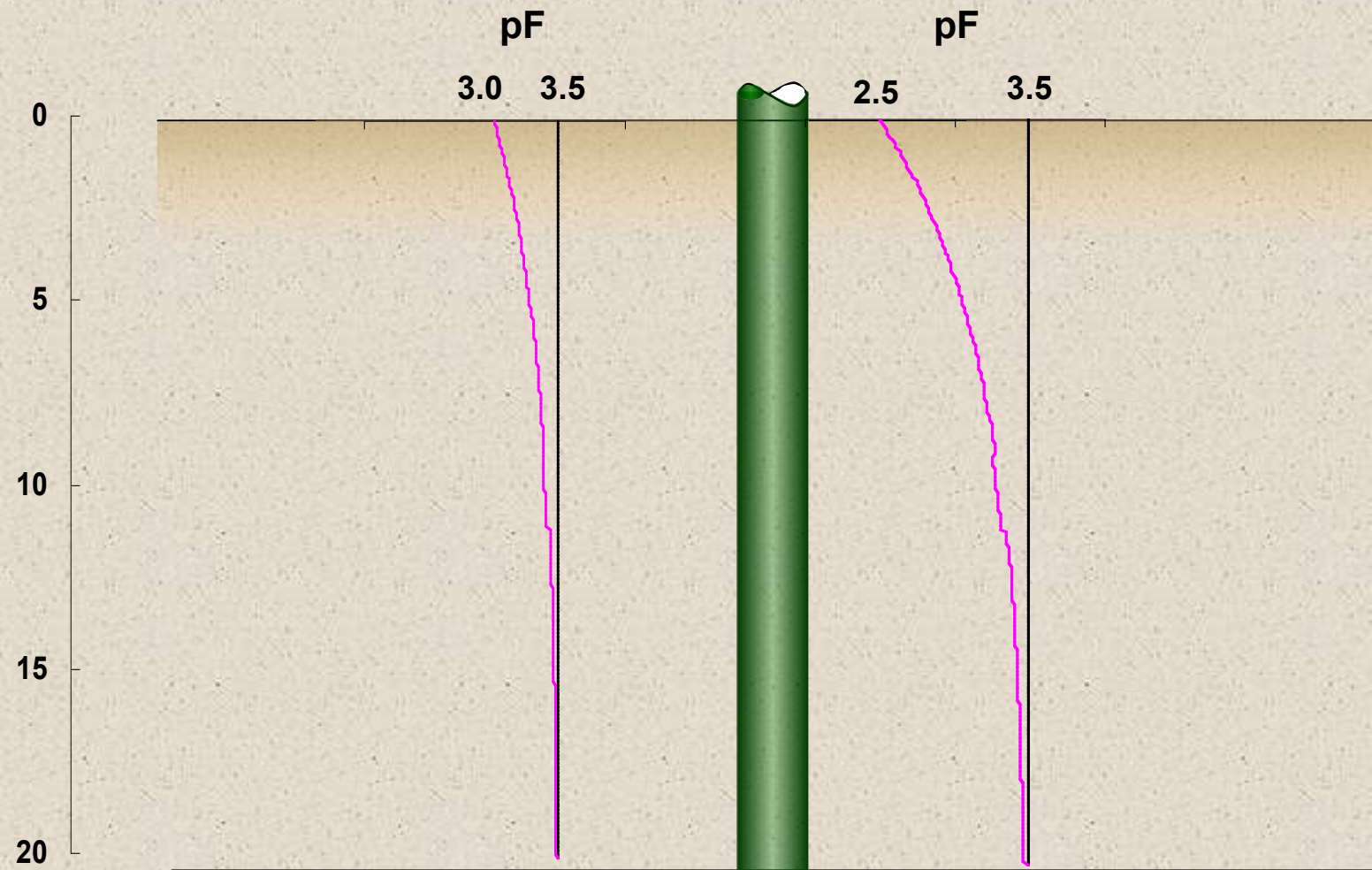
Movement Patterns



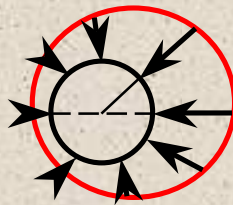
DRILLED PIER



DRILLED PIER

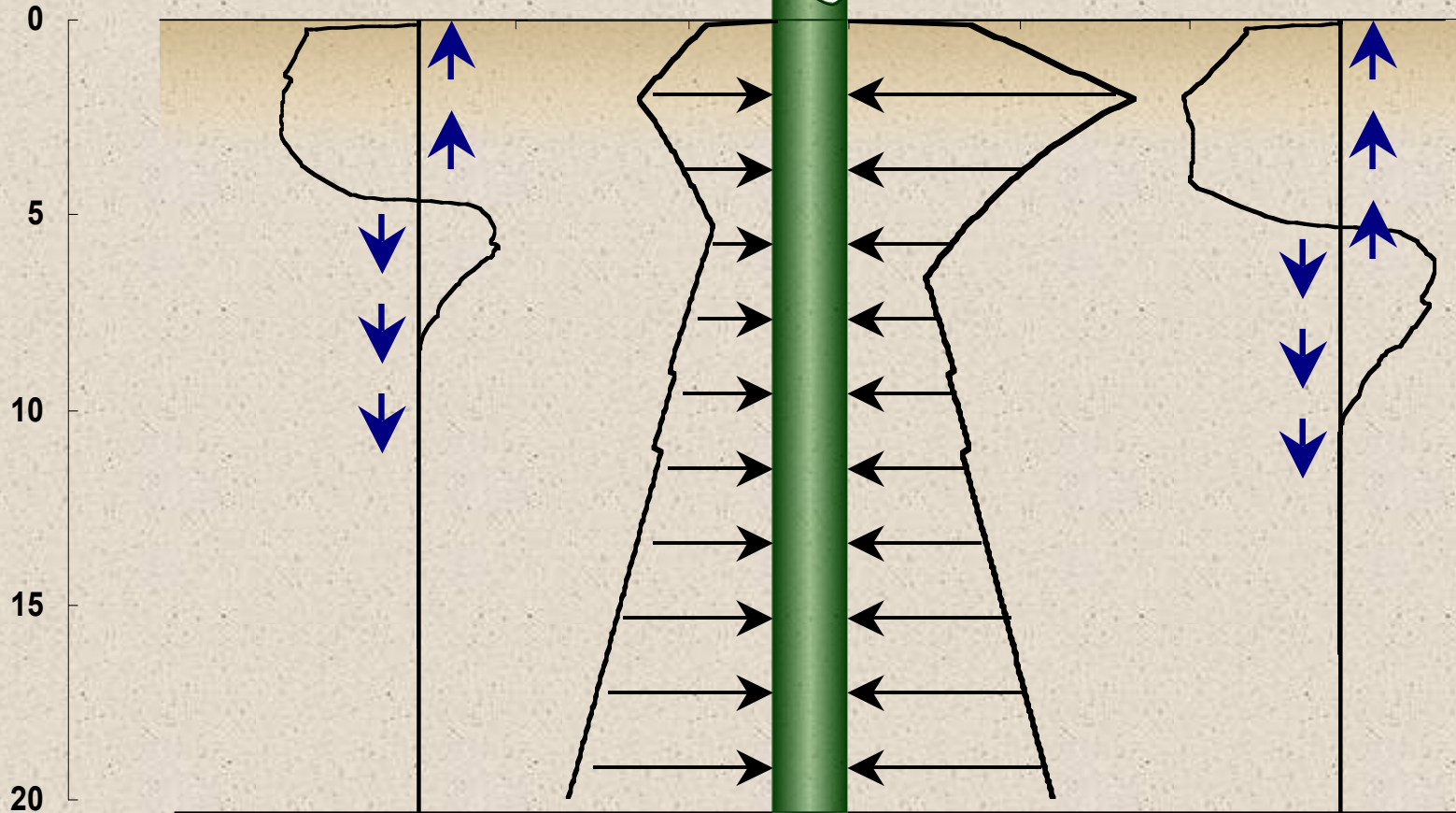


DRILLED PIER



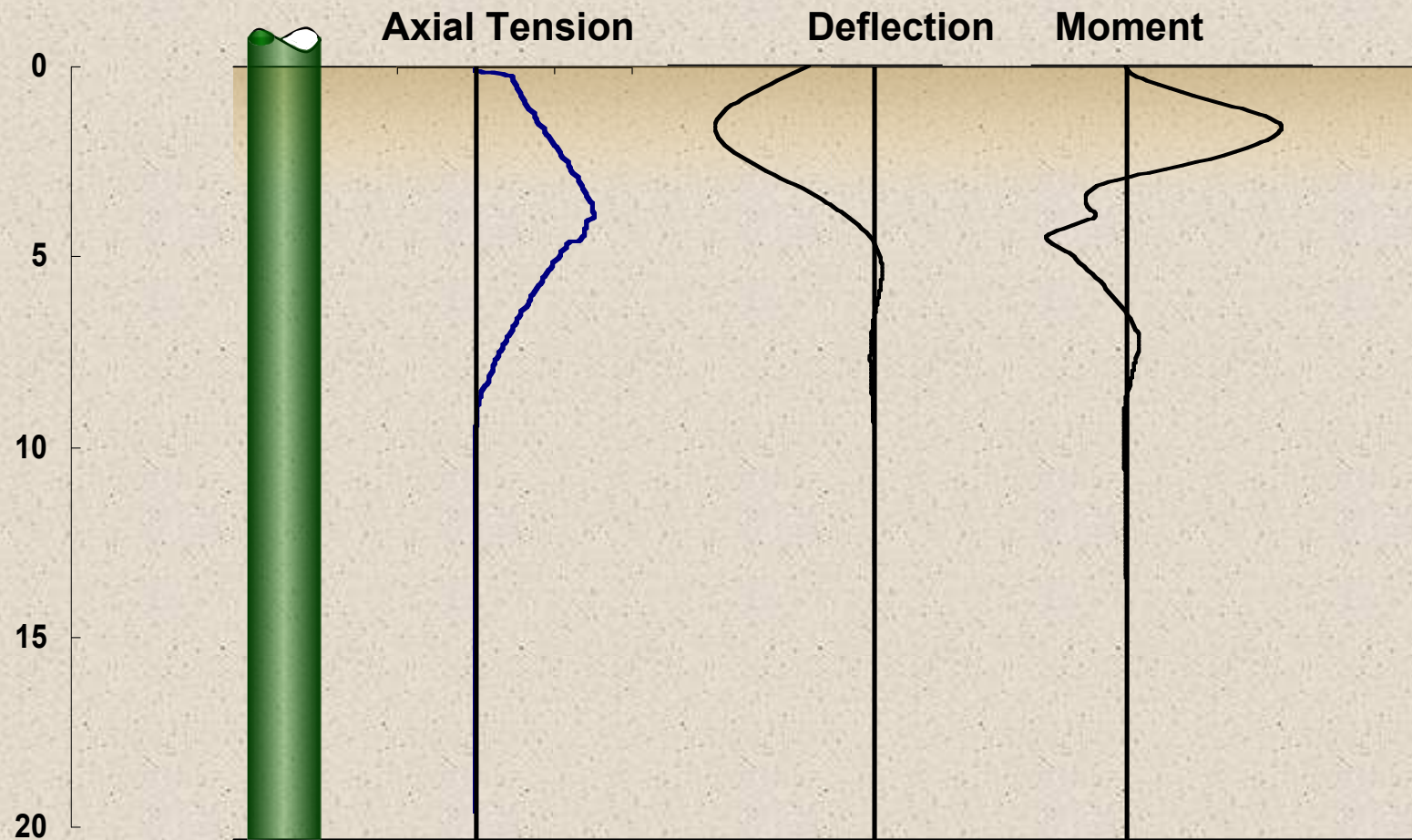
Shear Stress

Shear Stress

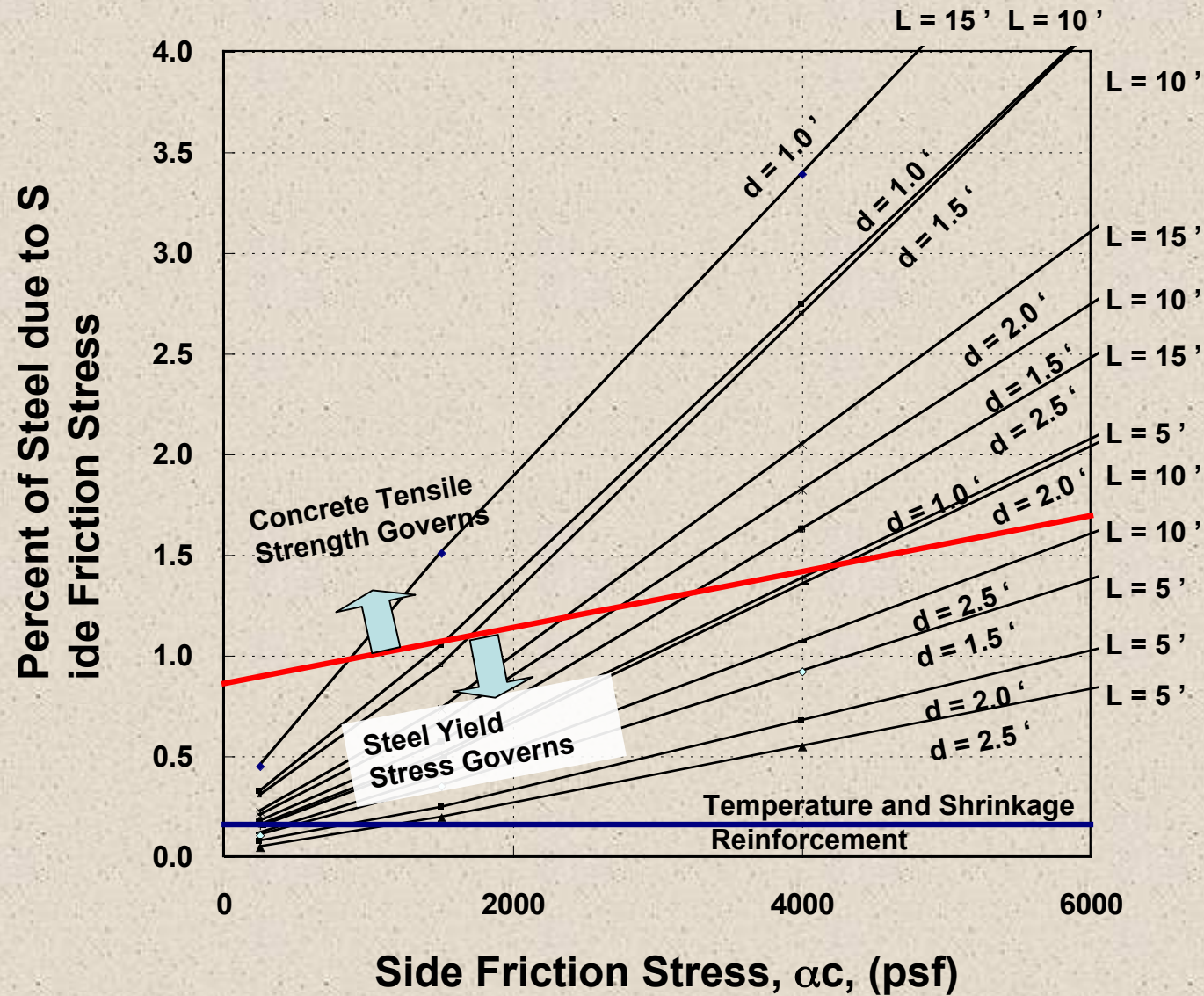


Horizontal Stress
Distribution

DRILLED PIER

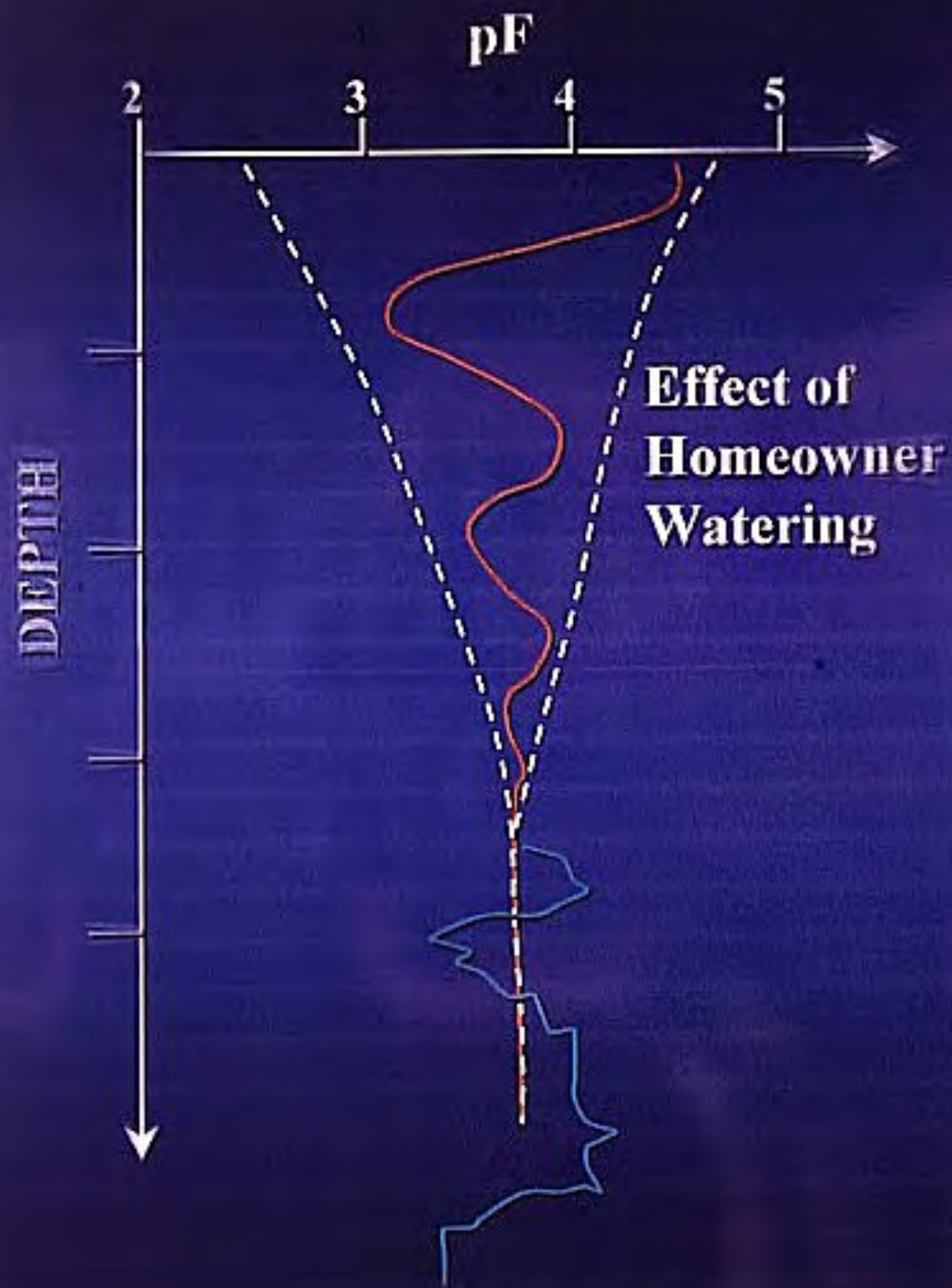


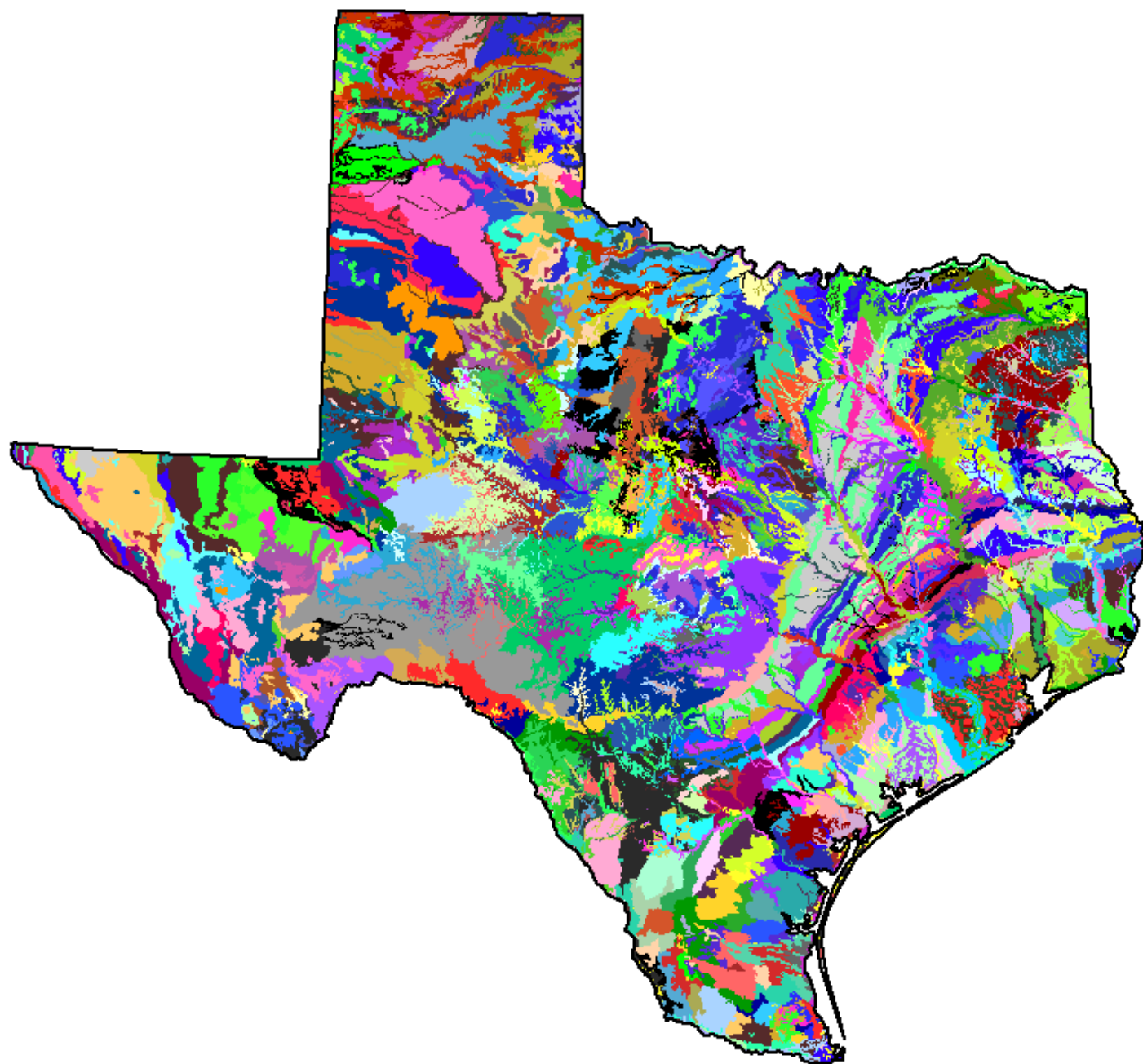
DRILLED PIER REINFORCEMENT

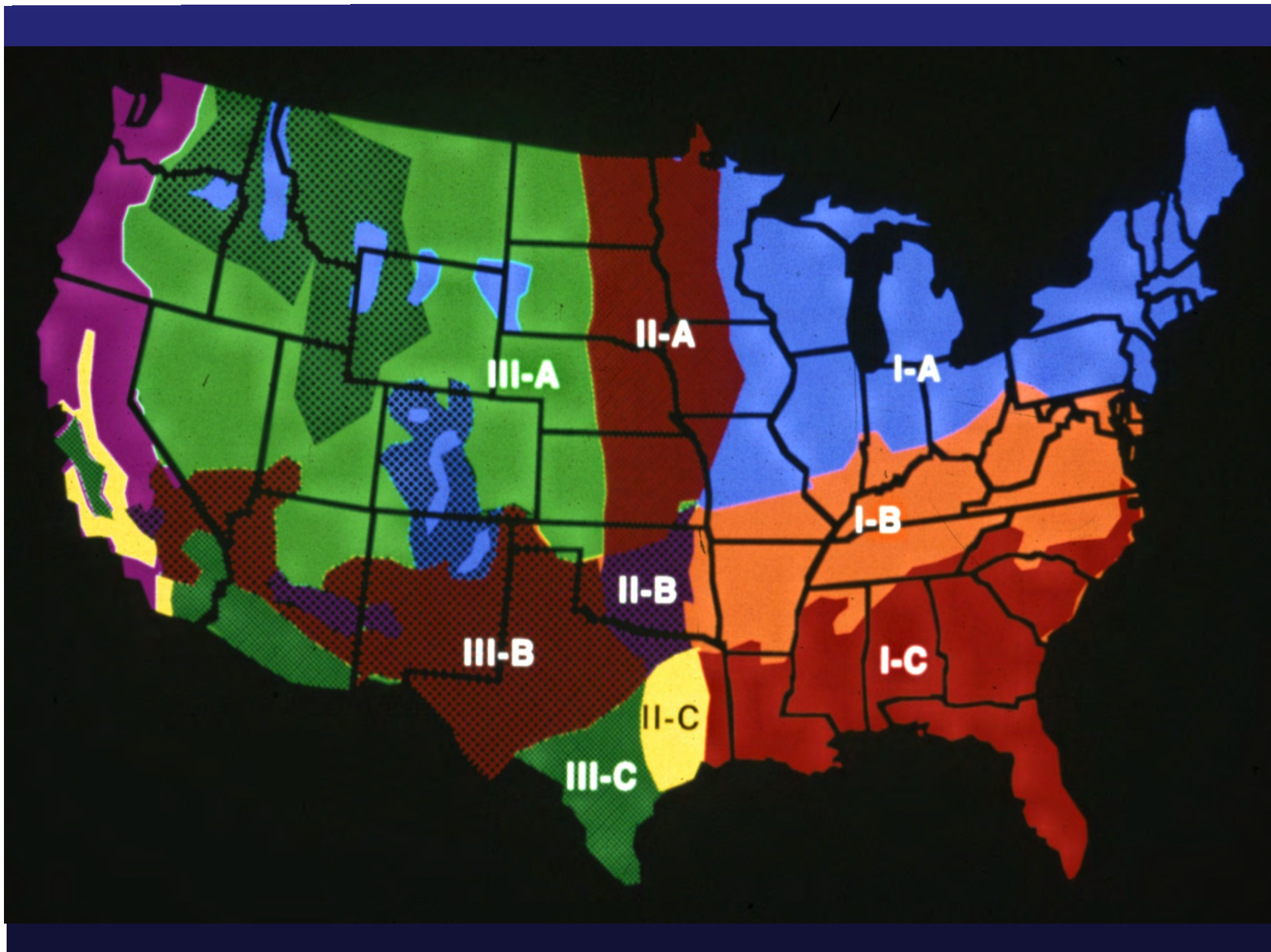


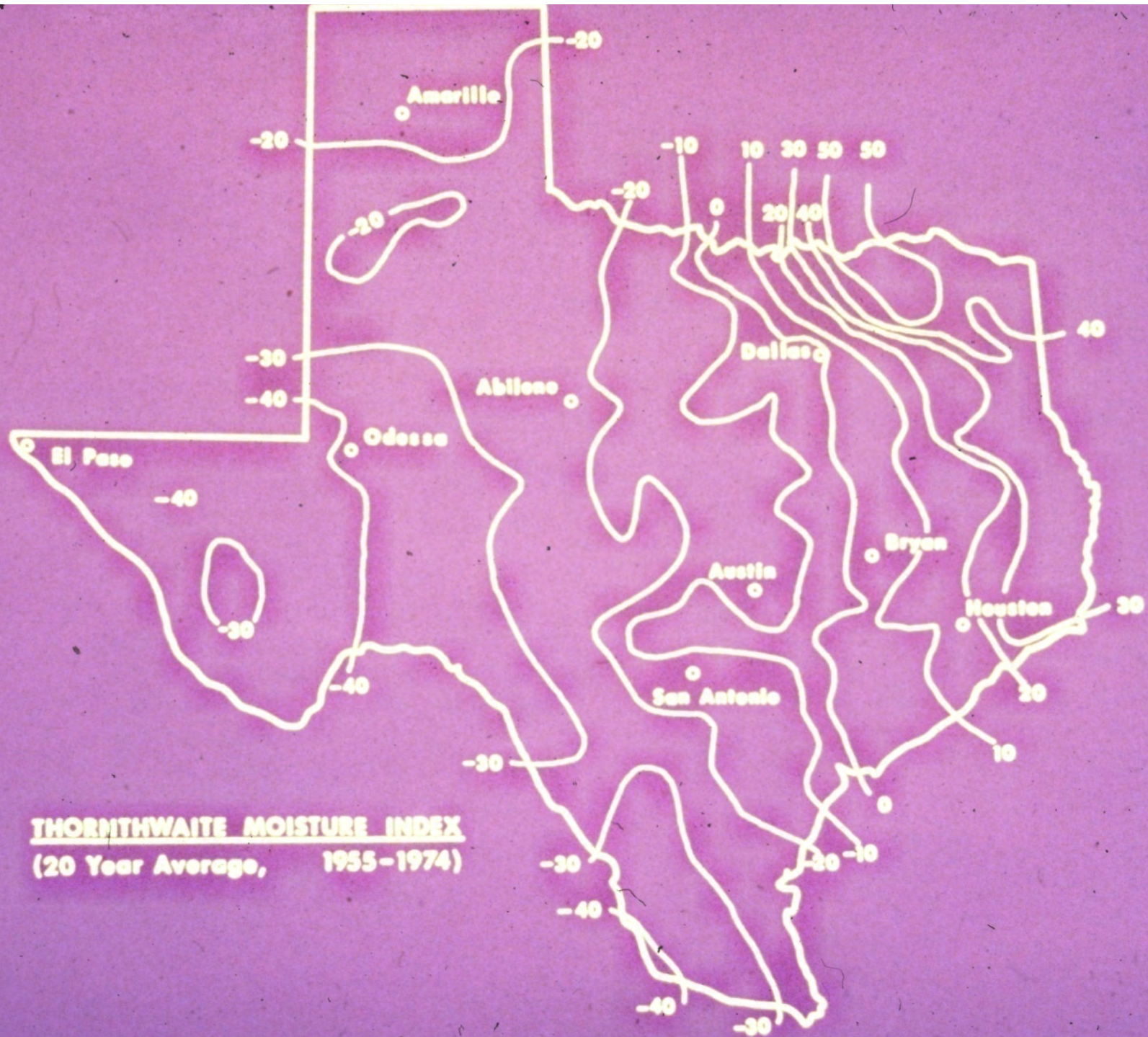




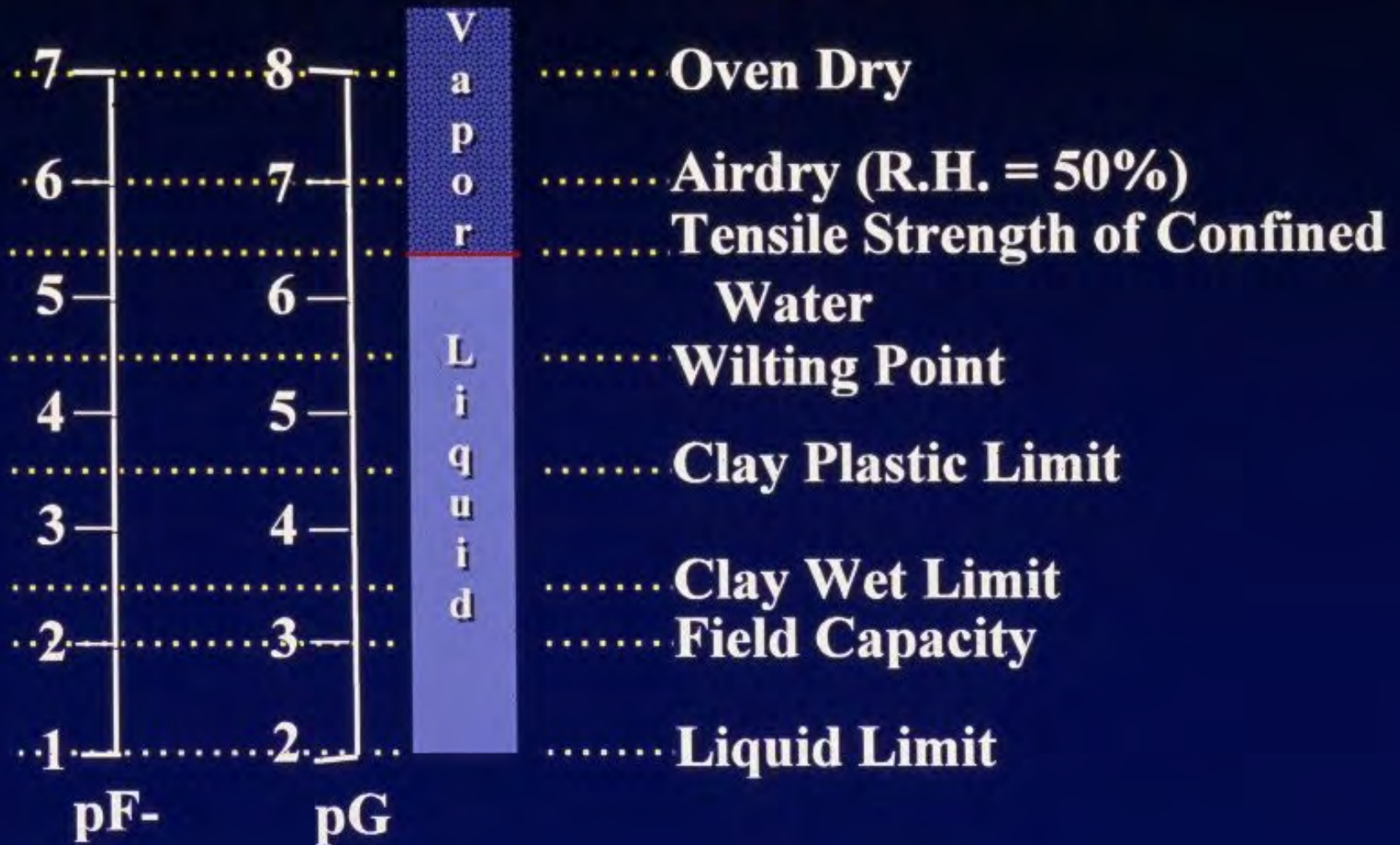






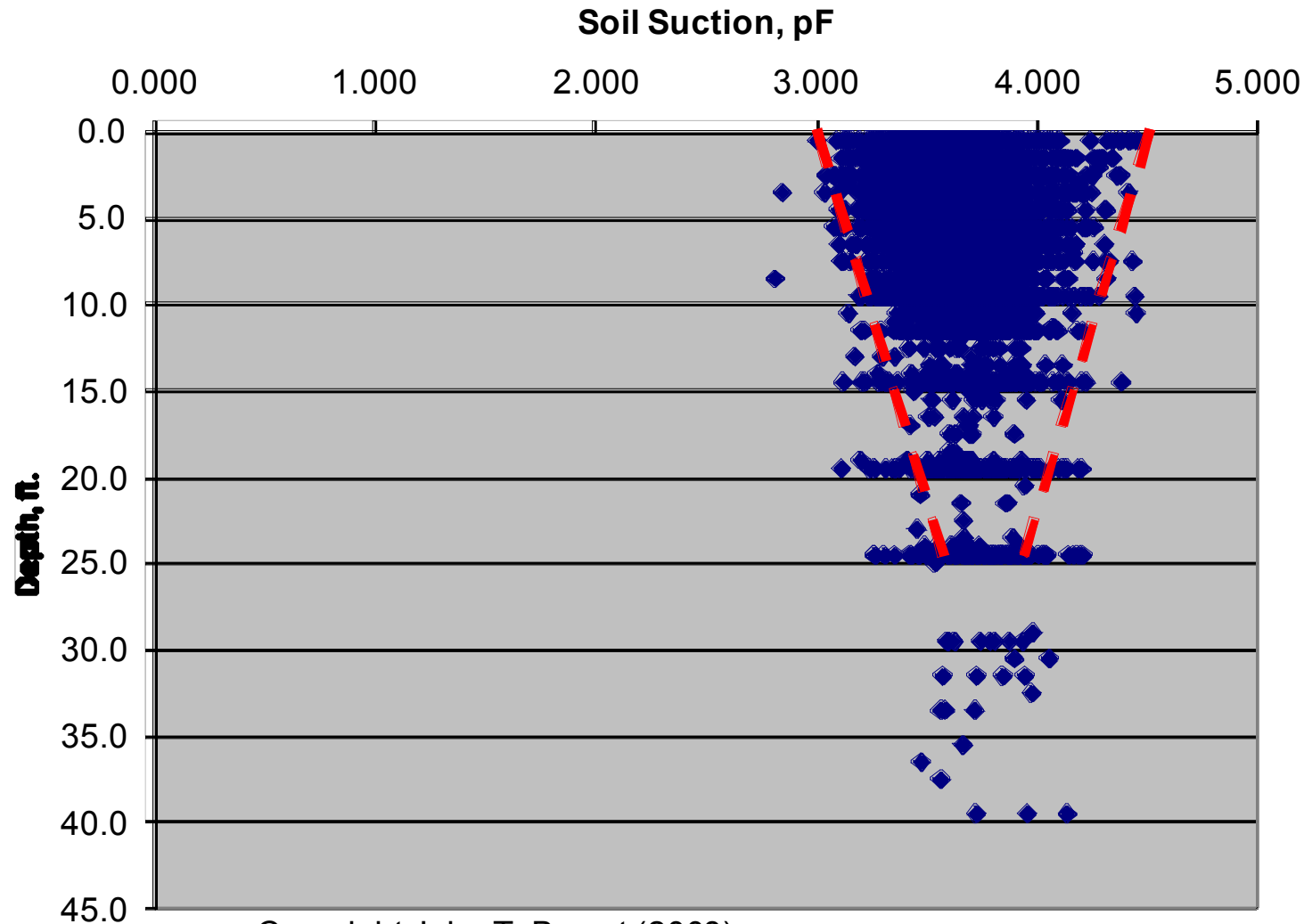


Physical Meaning of Scales



Empirically Measured Suctions

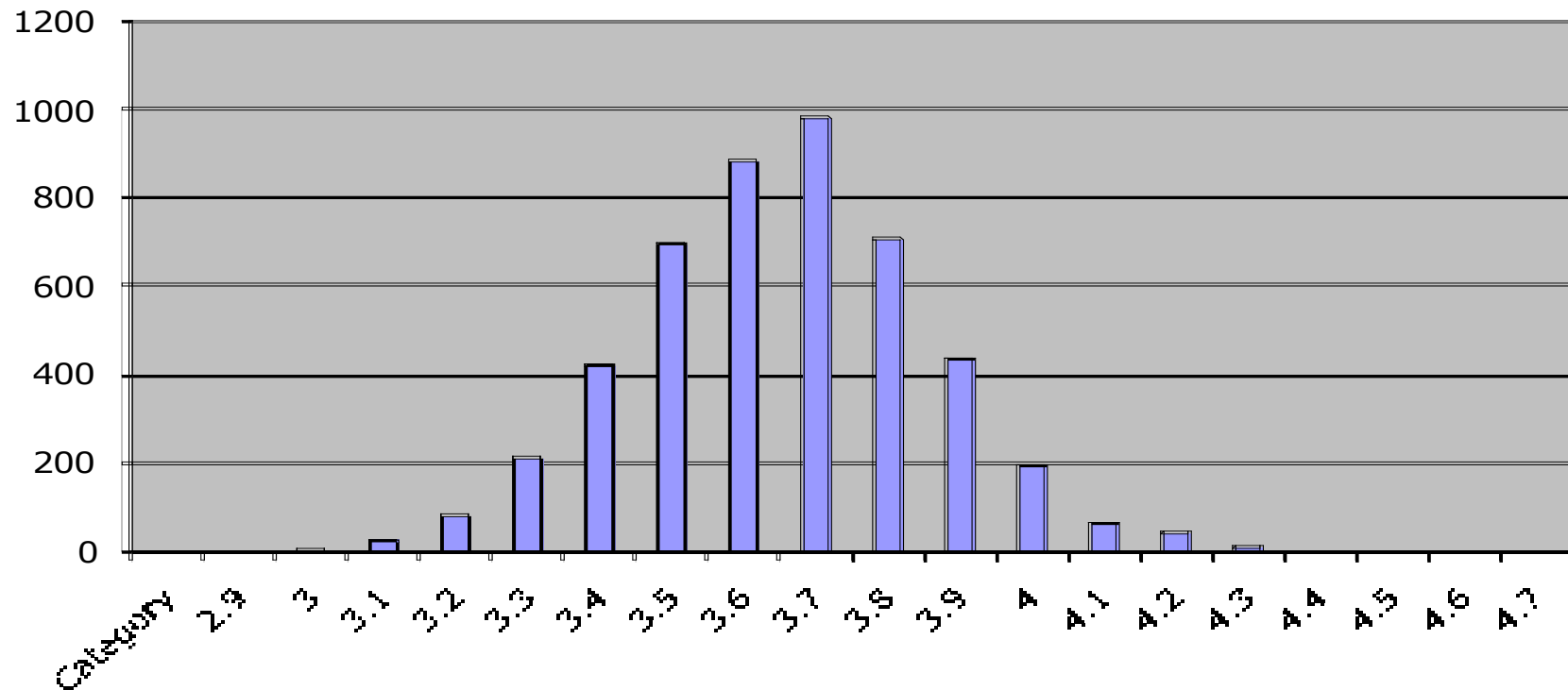
BCI 2002 to 2008 = 26,000+ Data Points



Copyright John T. Bryant (2008)

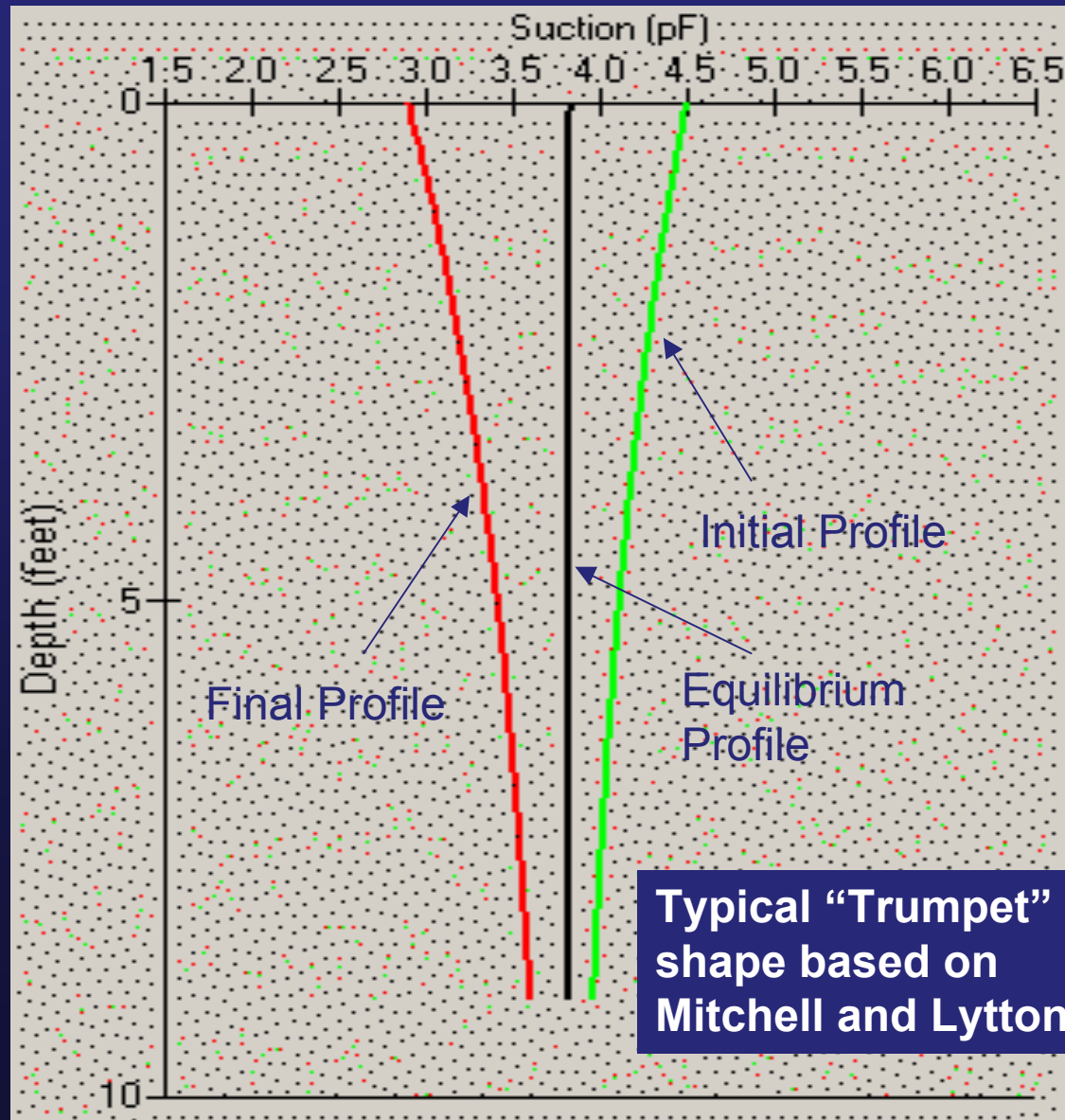
Reasonable Suction Change Range

2003 Total Soil Suction Data (4776 Observations)



Unsaturated Soil Mechanics

Typical Suction Envelope



Exponential Suction Profile for Extreme Wetting and Drying Condition

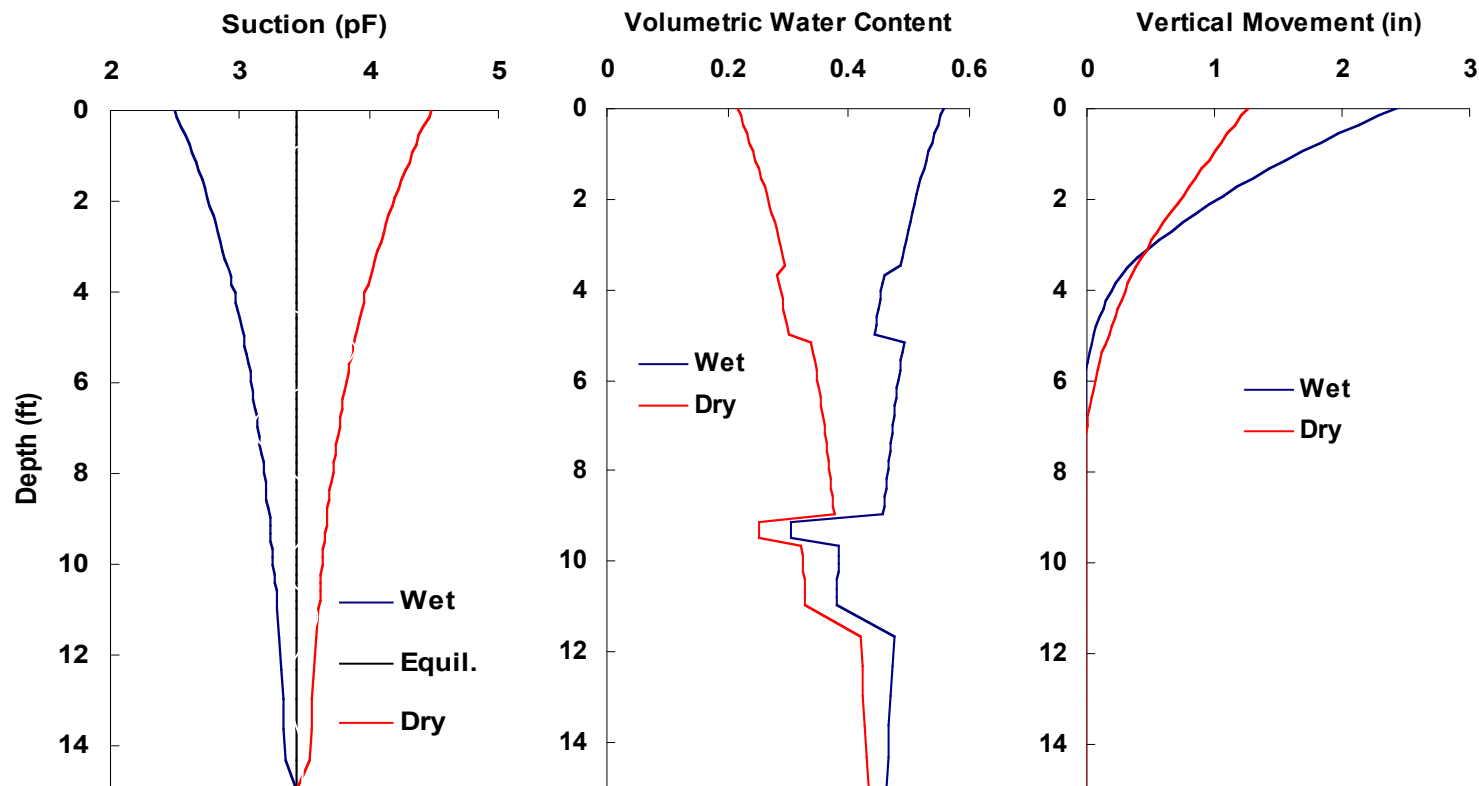
$$U(Z,t) = U_e + U_o \exp\left(-\sqrt{\frac{n\pi}{\alpha}}Z\right) \cos\left(2\pi nt - \sqrt{\frac{n\pi}{\alpha}}Z\right)$$

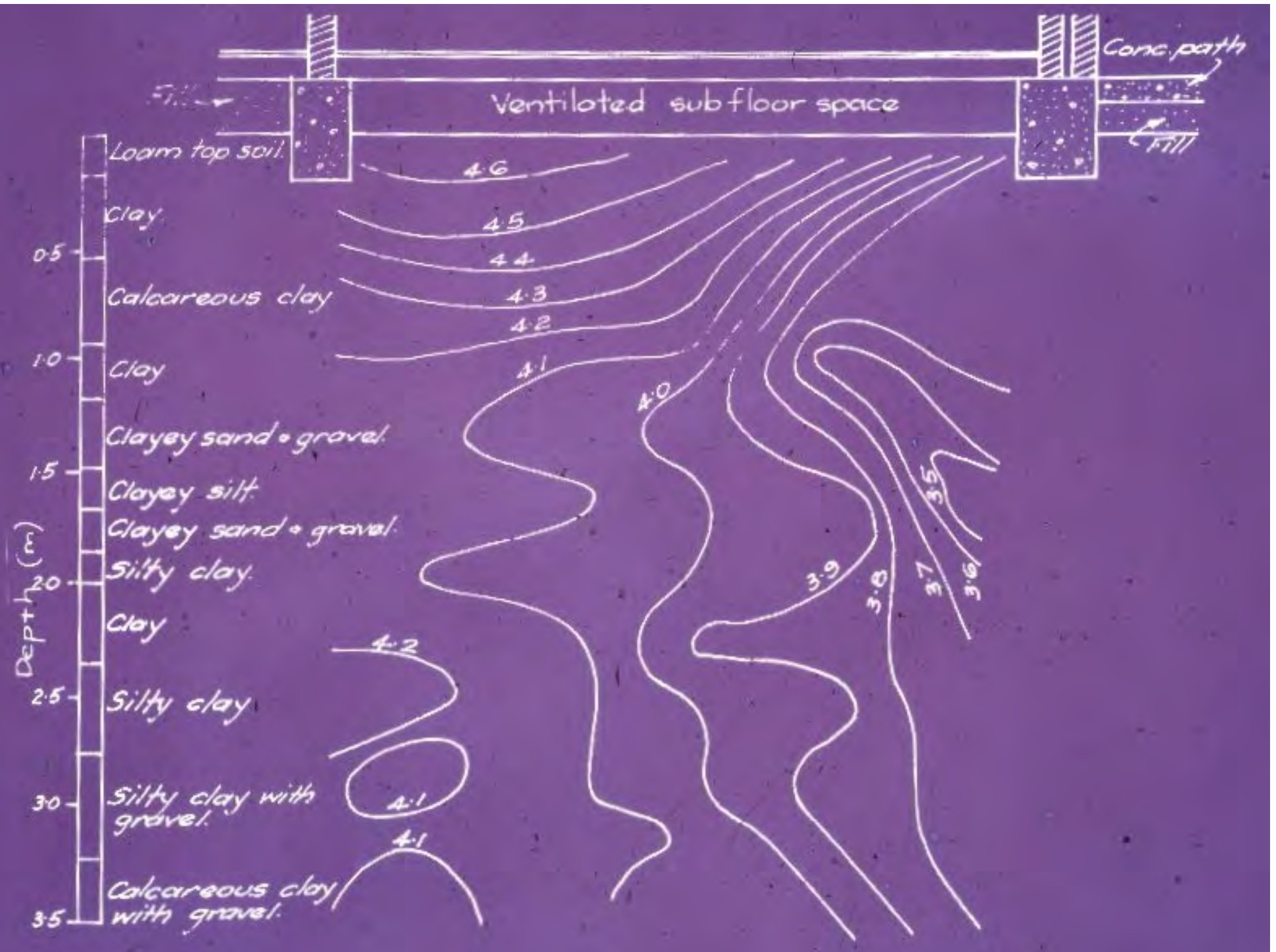
Mitchell (1979)

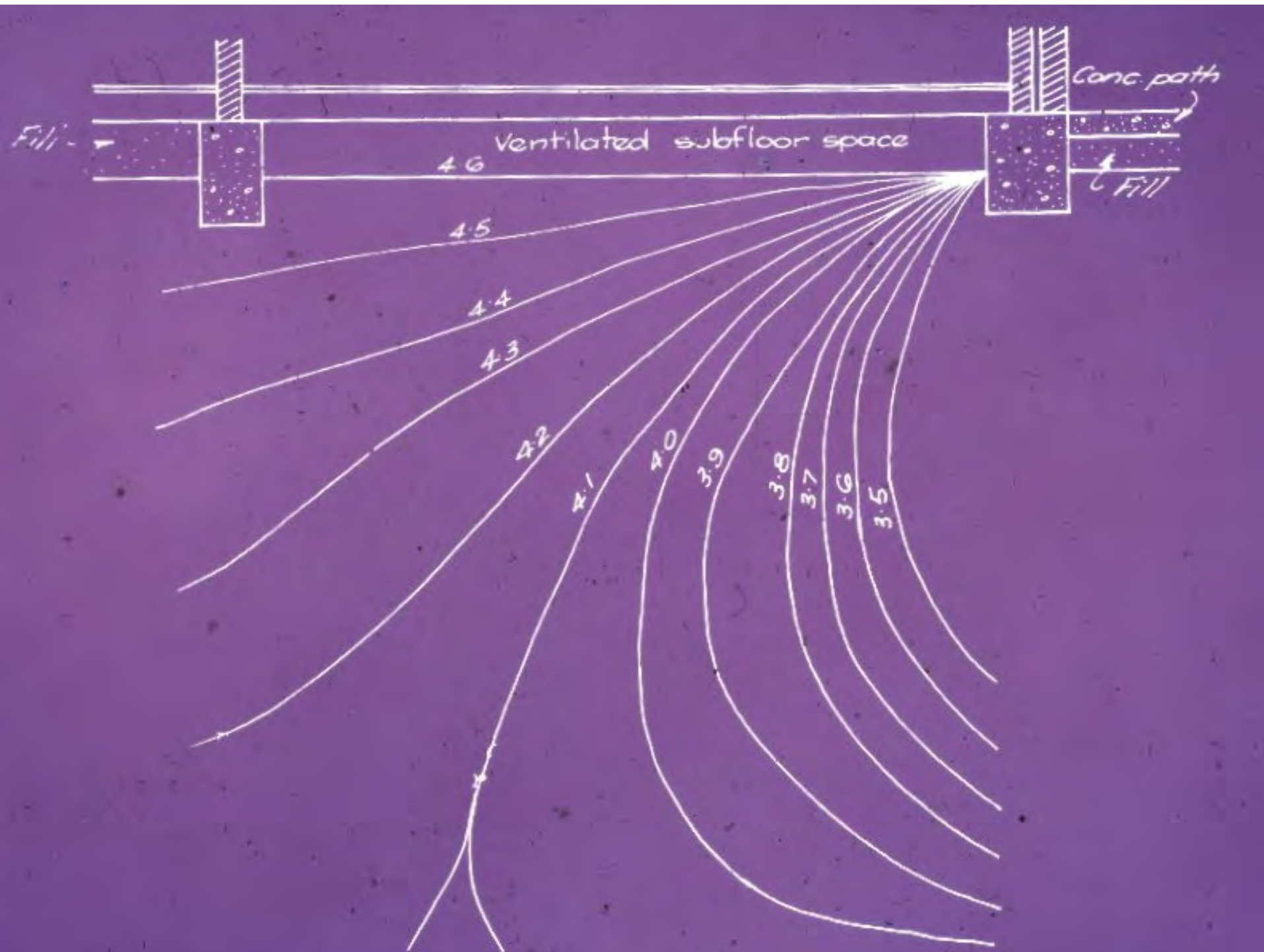
$$U(Z) = U_e + U_o \exp\left(-\sqrt{\frac{n\pi}{\alpha}}Z\right)$$

Fort Worth Interstate 820

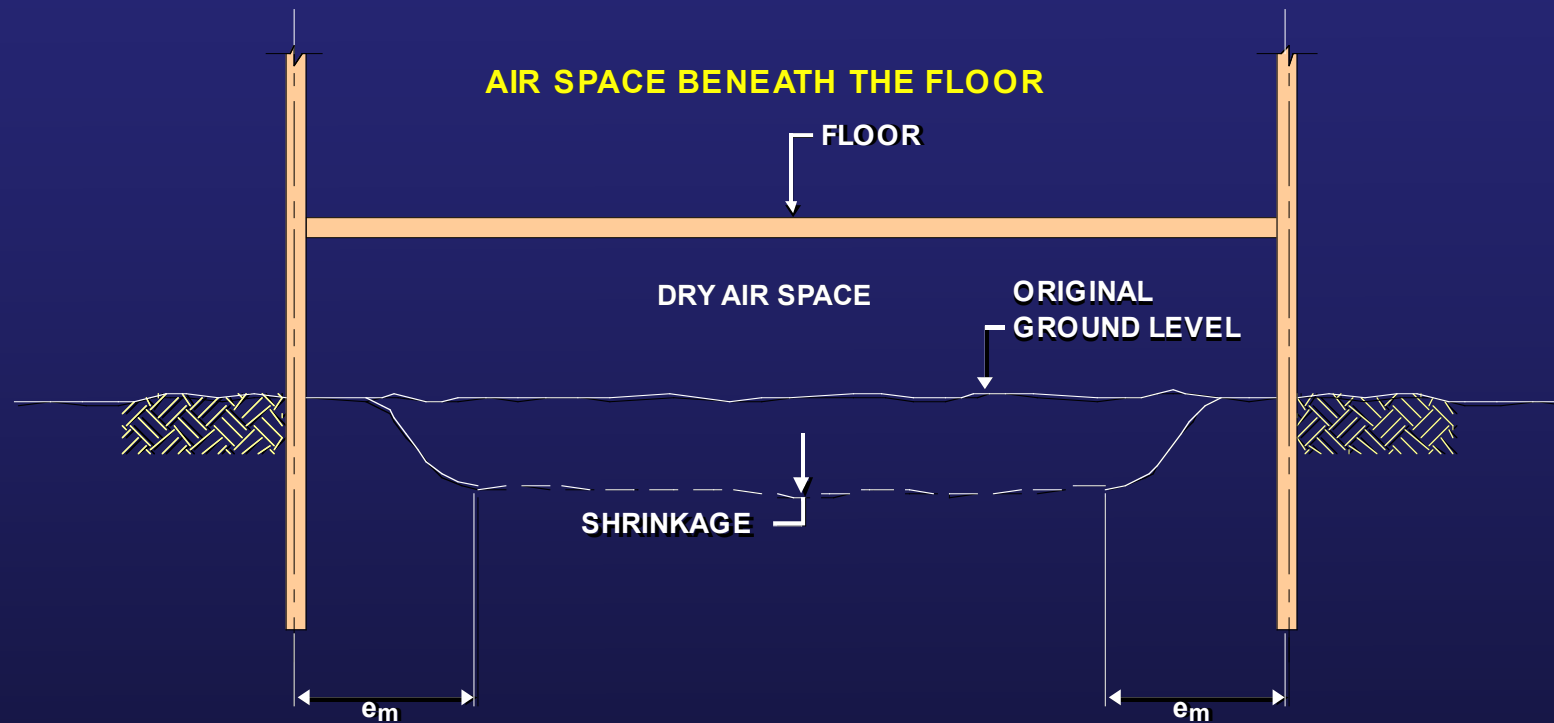
Moisture
Active
zone







TOTAL MOVEMENT PATTERNS WITH RAISED WOOD FLOOR FOUNDATIONS



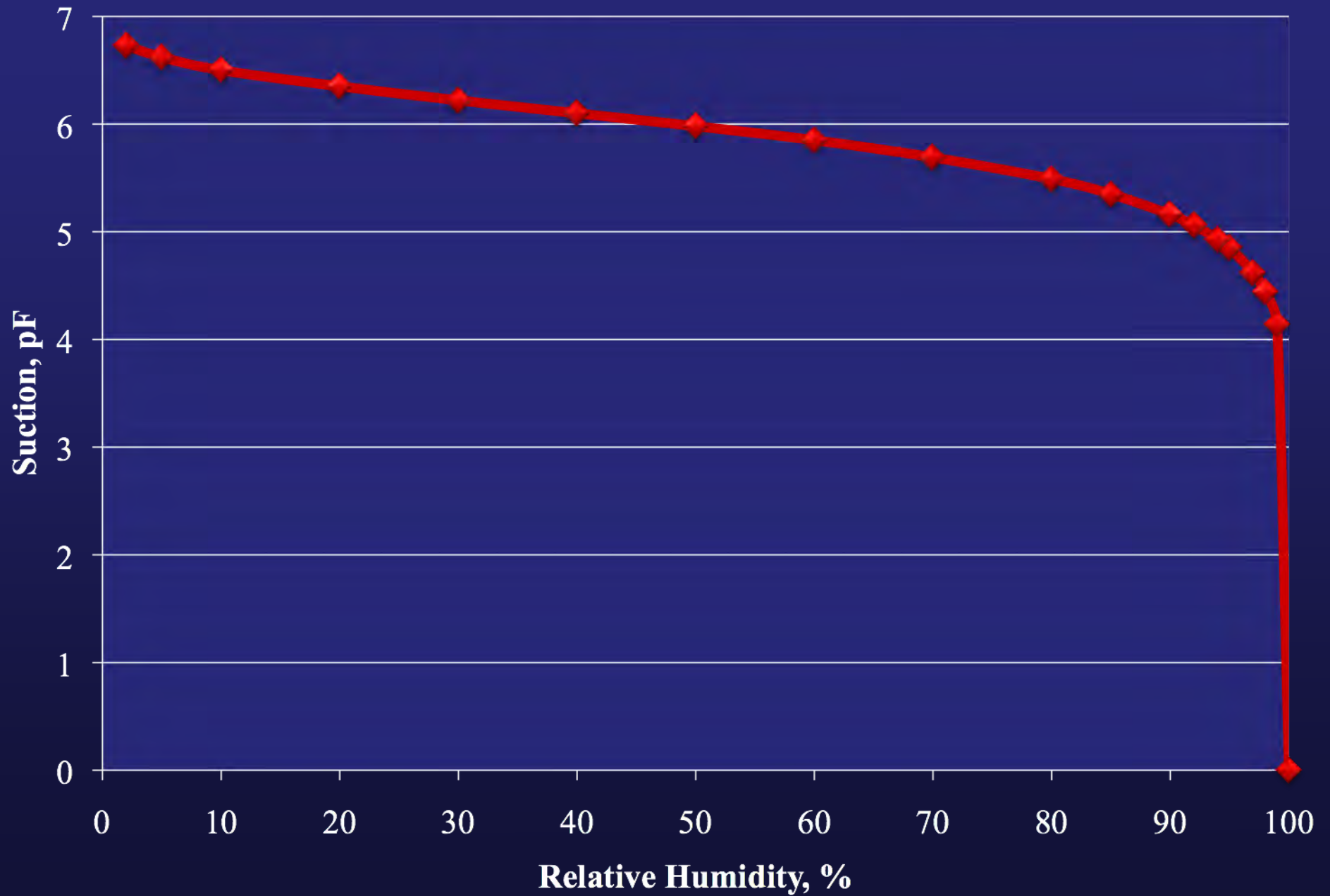
NOTE

AMOUNT OF SHRINKAGE DEPENDS ON THE LEVEL OF RELATIVE HUMIDITY IN THE AIR BENEATH THE FLOOR. THE LOWER THE RELATIVE HUMIDITY, THE GREATER WILL BE THE AMOUNT OF SHRINKAGE. INITIALLY, THE SOIL WILL BE AT OR ABOVE 98% RELATIVE HUMIDITY. e_m IS THE EDGE MOISTURE VARIATION DISTANCE WHICH VARIES TYPICALLY BETWEEN 3 AND 9 FEET DEPENDING ON THE TYPE OF SOIL.

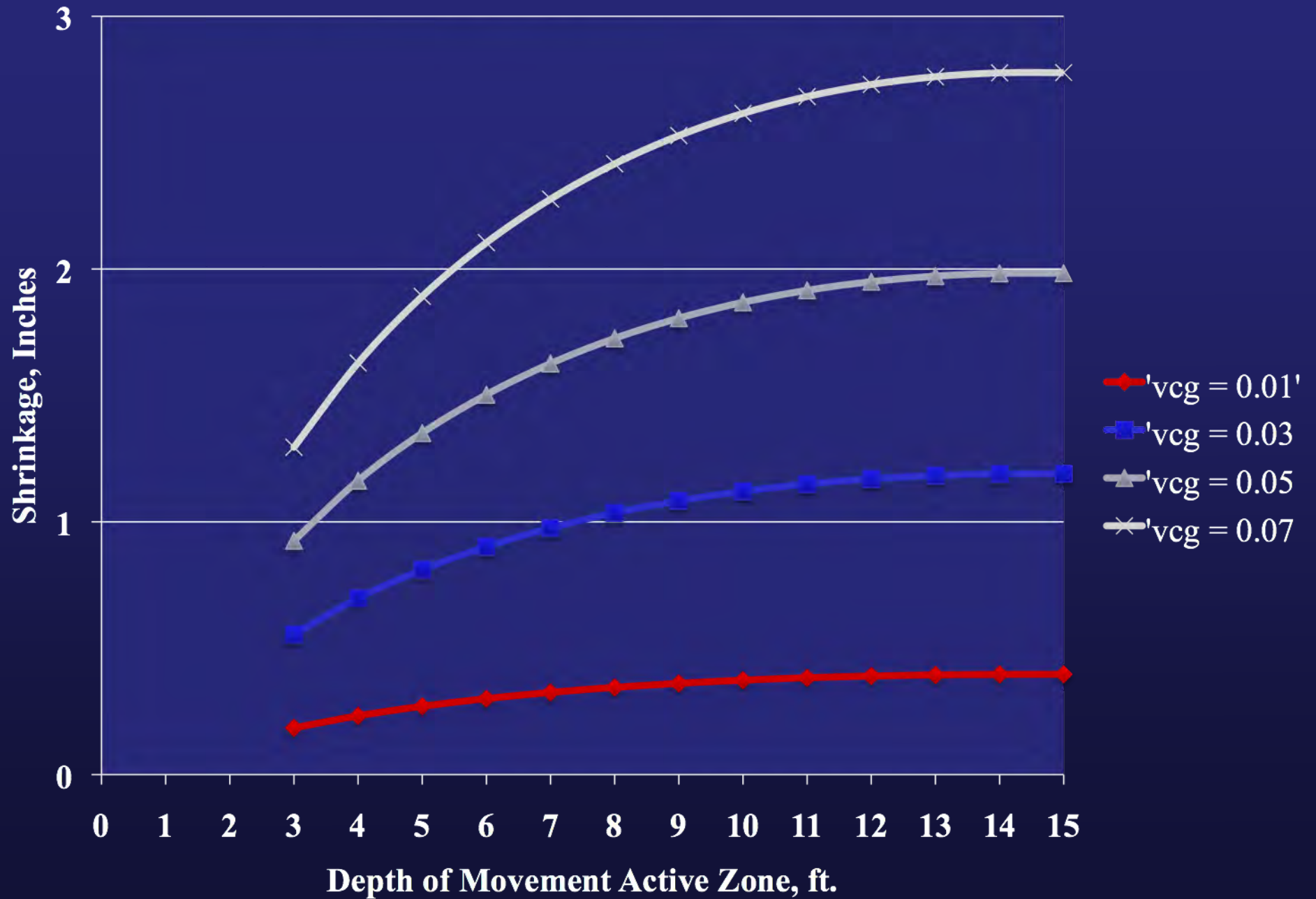
Raised Floor Foundation Boundary Conditions

<u>OUTSIDE</u>	<u>pF</u>	<u>pF DRY</u>	<u>R.H.</u>
<u>WET</u>		<u>BENEATH, %</u>	
FLOWER BED	2.9	6.50	10
LAWN WATER	3.0	6.35	20
TREE	4.5	6.22	30
		6.10	40
		5.98	50

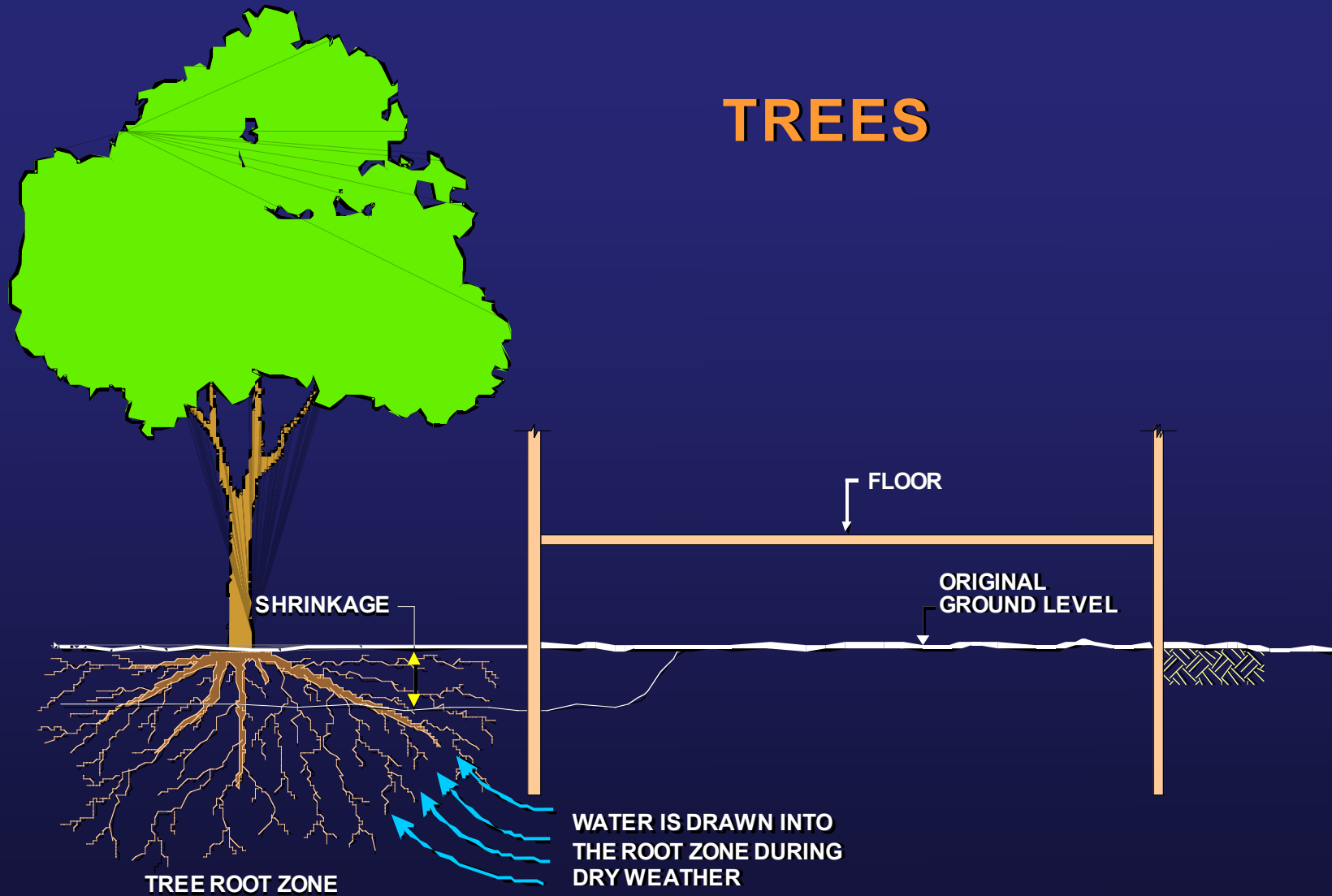
Suction, pF vs Relative Humidity, %



Shrinkage, in. vs Depth of Active Zone, ft.



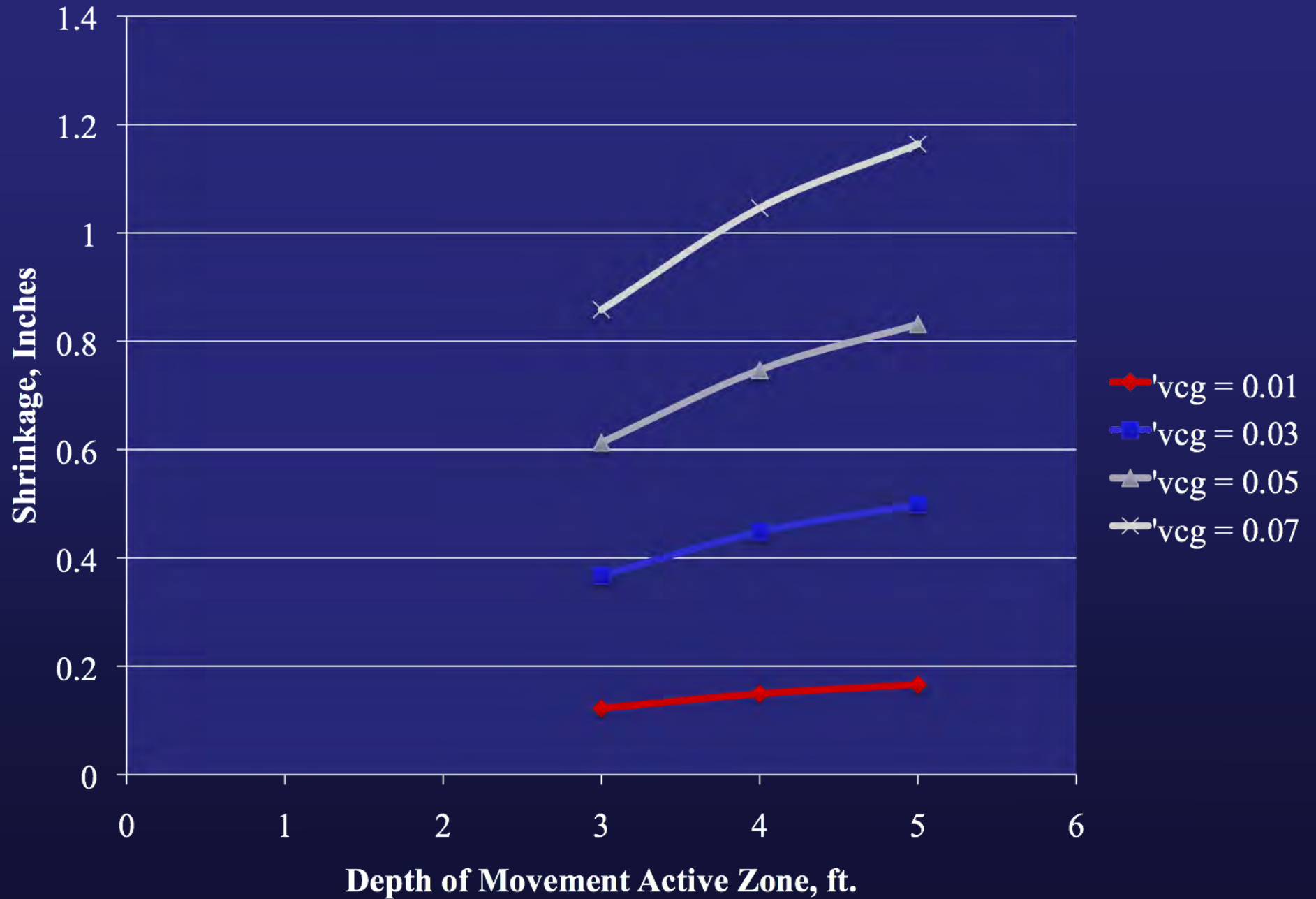
TREES



NOTE

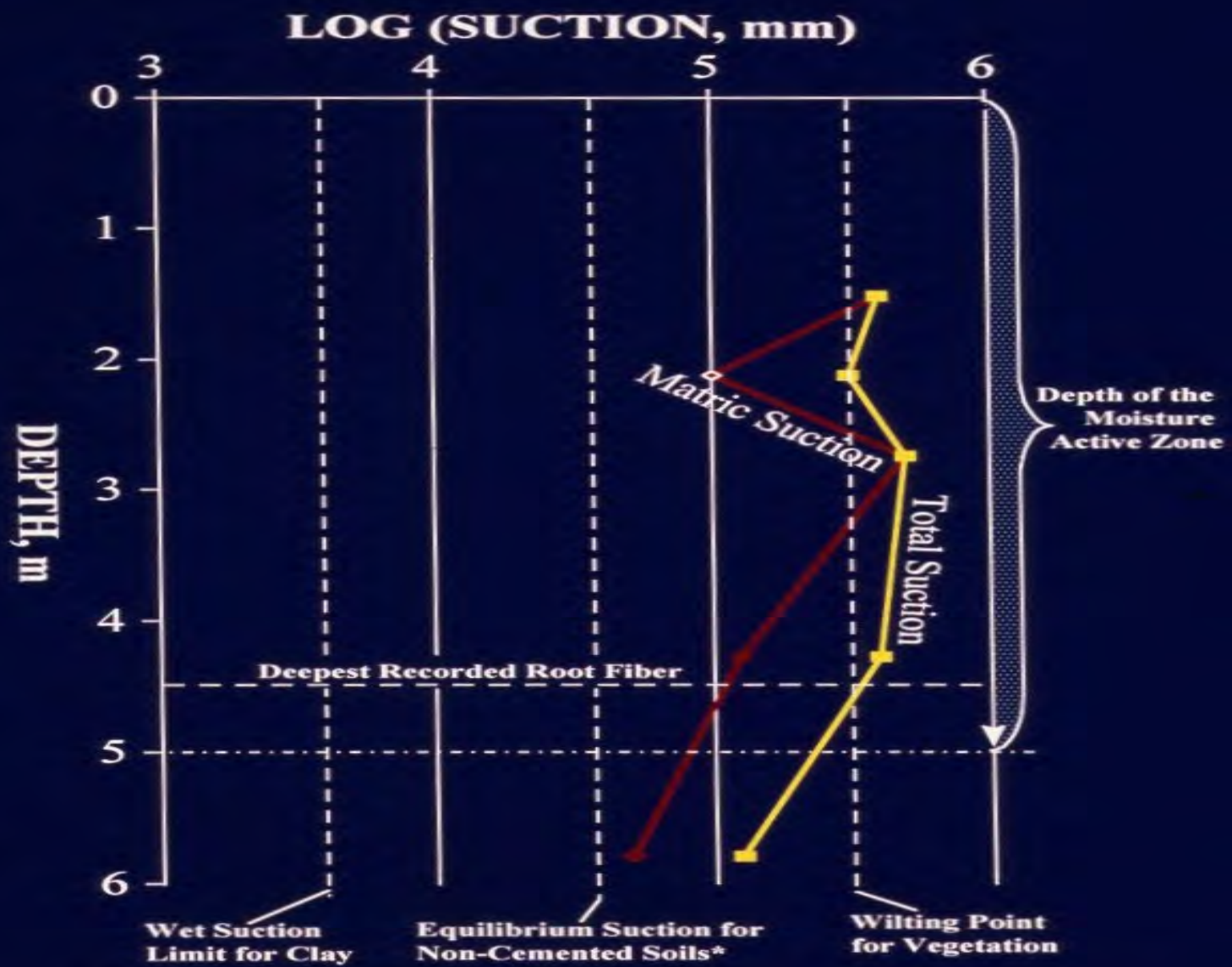
AMOUNT OF SHRINKAGE DEPENDS ON THE DEPTH OF THE TREE ROOT ZONE, HOW FAR THE ROOTS PENETRATE BENEATH THE BUILDING, AND THE TYPE OF SOIL.

Shrinkage with $DpF = 1.5$



Laboratory Tests

- Atterberg limits
- Hydrometer
- Water content
- Dry density
- Sieve analysis



* From Empirical Relation of Thornthwaite Moisture Index with equilibrium suction (Russam and Coleman, 1961)

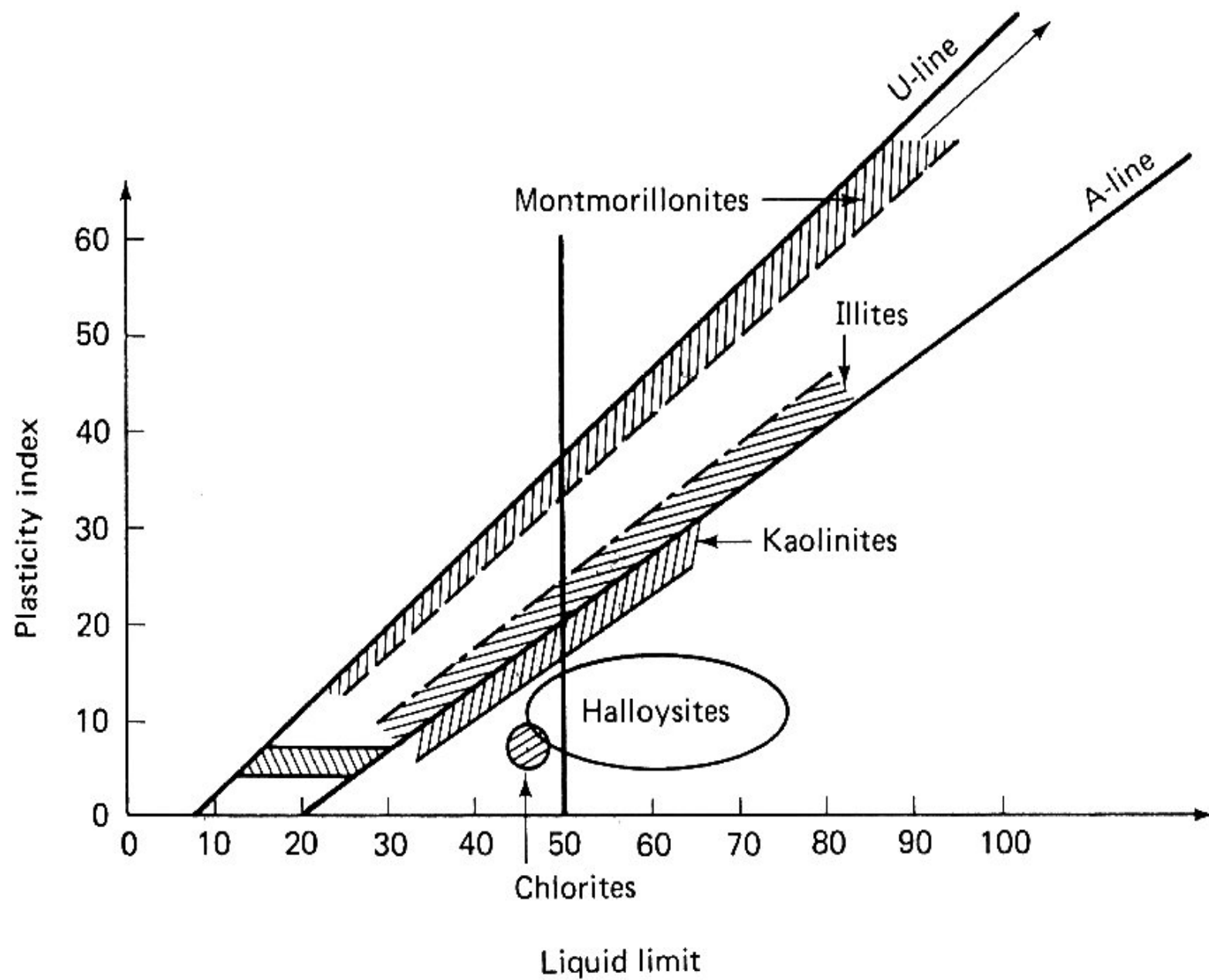
YaA	Yahola fine sandy loam, 0 to 1 percent slopes, rarely flooded	858.7	0.2%
ZaB	Zack fine sandy loam, 1 to 5 percent slopes	11,763.7	3.1%
ZaC2	Zack fine sandy loam, 2 to 5 percent slopes, eroded	1,729.5	0.5%
ZaD	Zack fine sandy loam, 5 to 8 percent slopes	3,194.0	0.8%
ZaE3	Zack fine sandy loam, 8 to 25 percent slopes, severely eroded	269.9	0.1%
ZcB	Zack-Urban land complex, 1 to 5 percent slopes	7,841.9	2.1%
ZcD	Zack-Urban land complex, 5 to 8 percent slopes	547.6	0.1%
ZuB	Zulch fine sandy loam, 1 to 3 percent slopes	11,440.6	3.0%
Totals for Area of Interest		377,977.9	100.0%

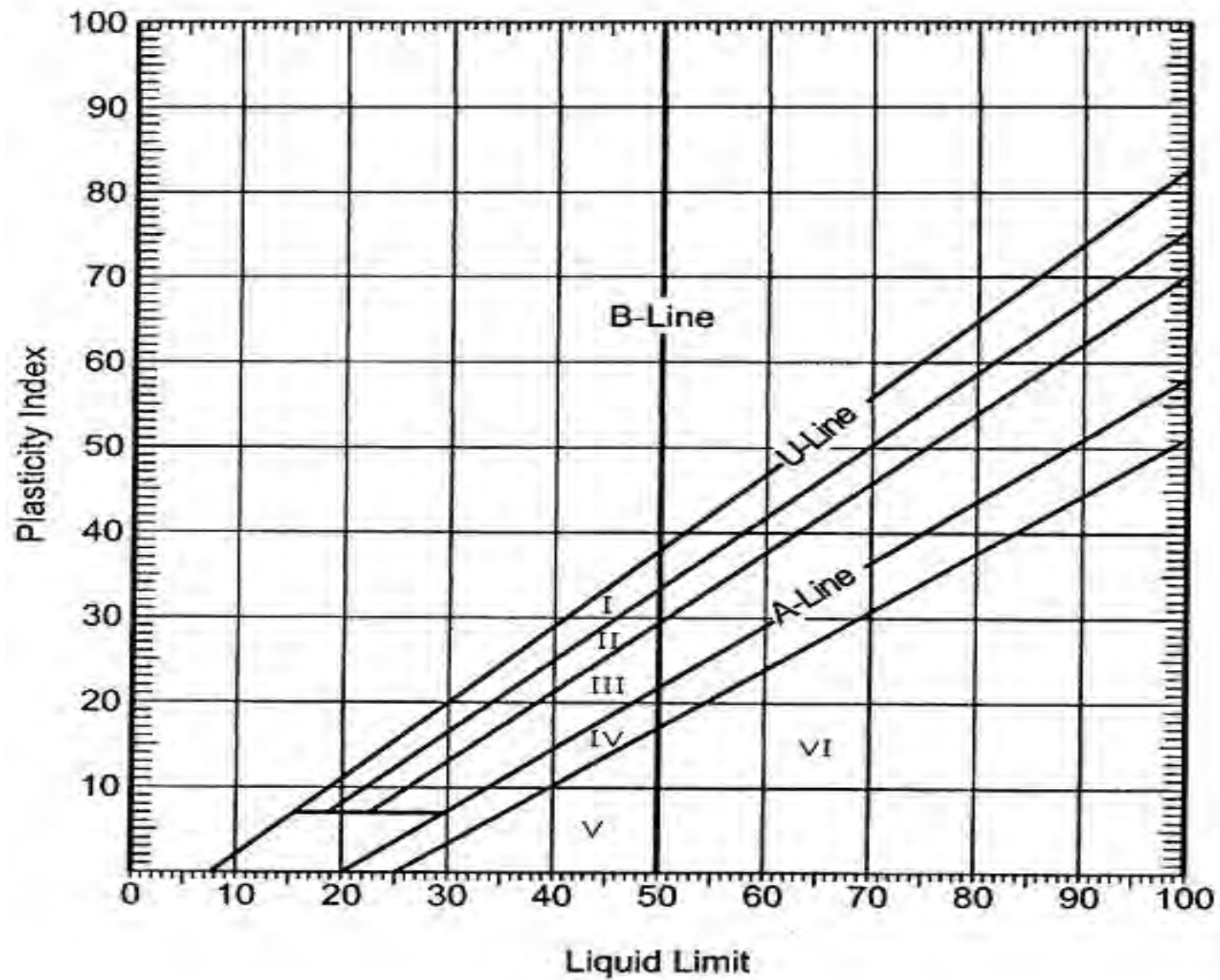


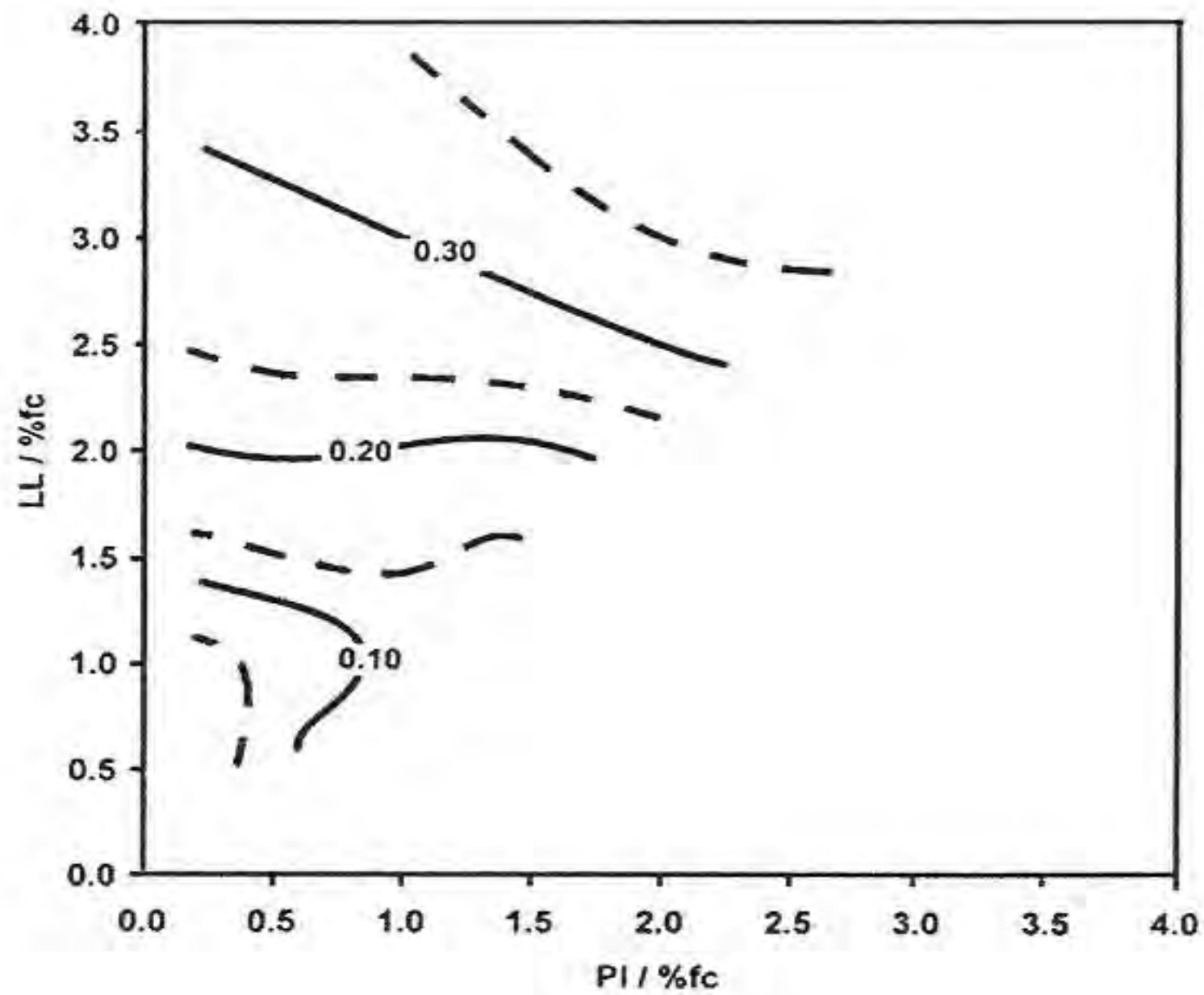
 **Warning:** Soil Map may not be valid at this scale.

You have zoomed in beyond the scale at which the soil map for this area is intended to be used. Mapping of soils is done at a particular scale. The soil surveys that comprise your AOI were mapped at 1:20,000. The design of map units and the level of detail shown in the resulting soil map are dependent on that map scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

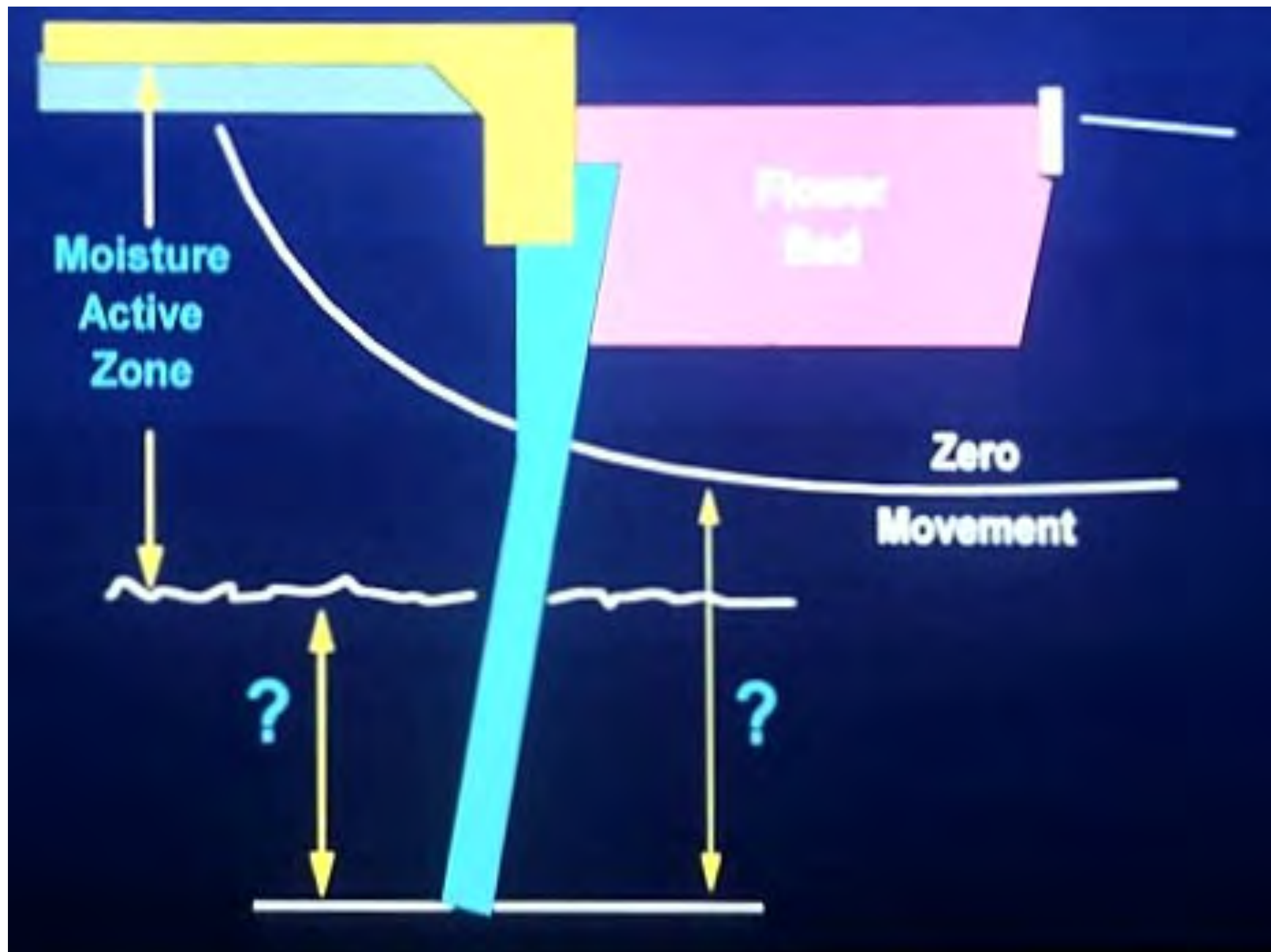


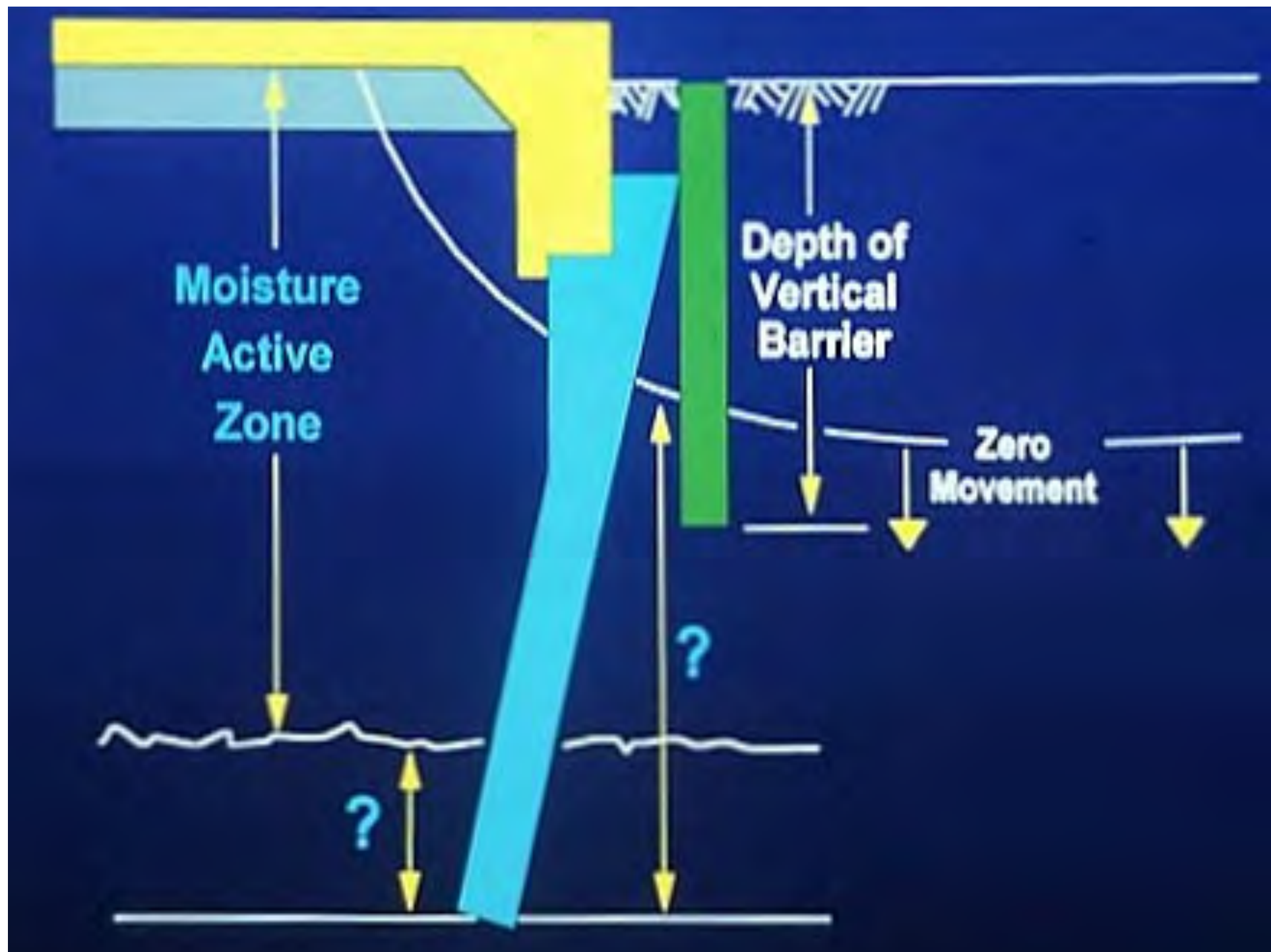




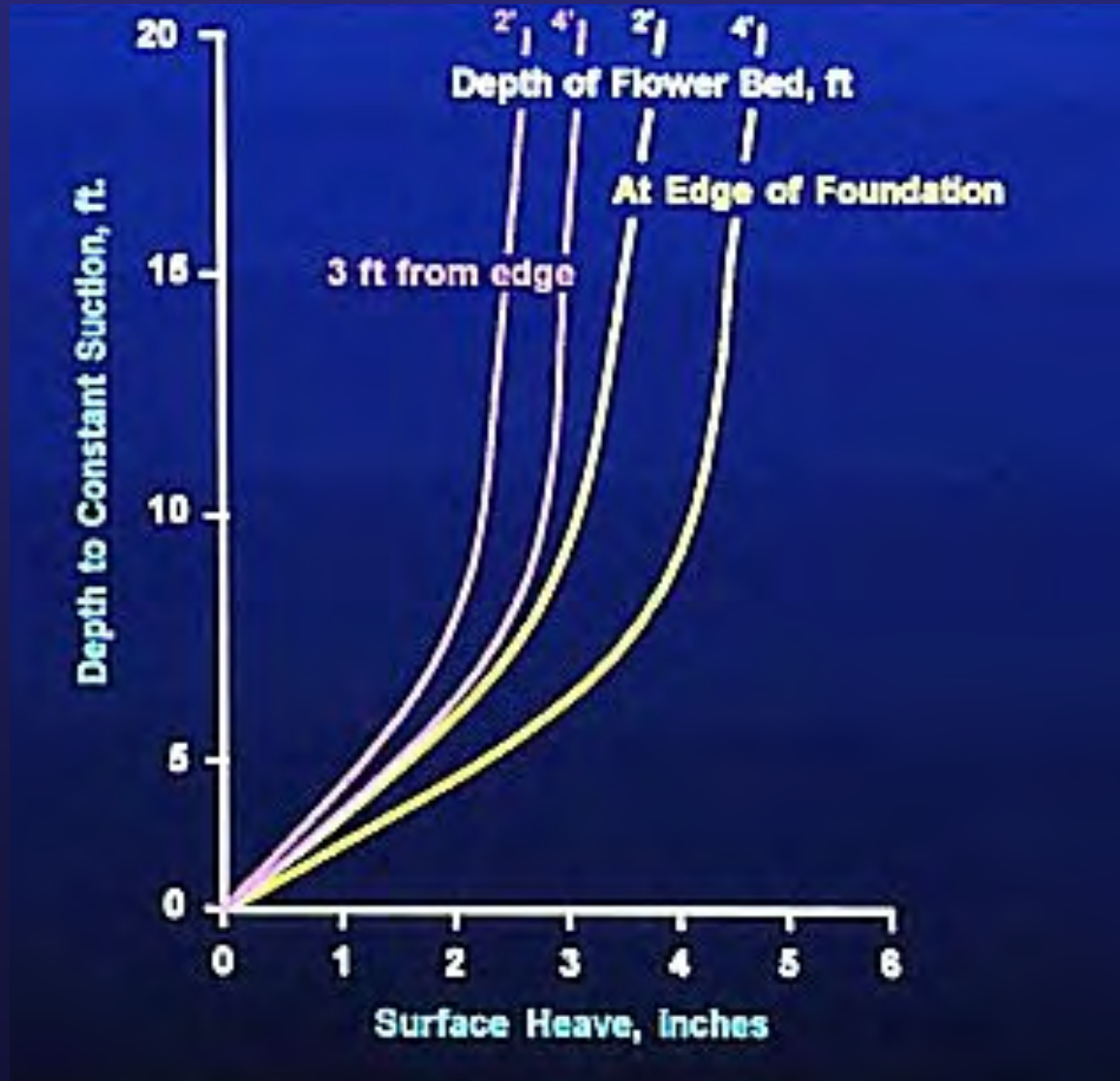
Typical Clay Properties

<u>Property</u>	<u>Range</u>	<u>Example</u>
Liquid Limit	55-90	86
Plasticity	30-60	59
Plastic Limit	25-30	27
Percent Passing #200	80-99	97
Percent Passing 0.002mm	-	65

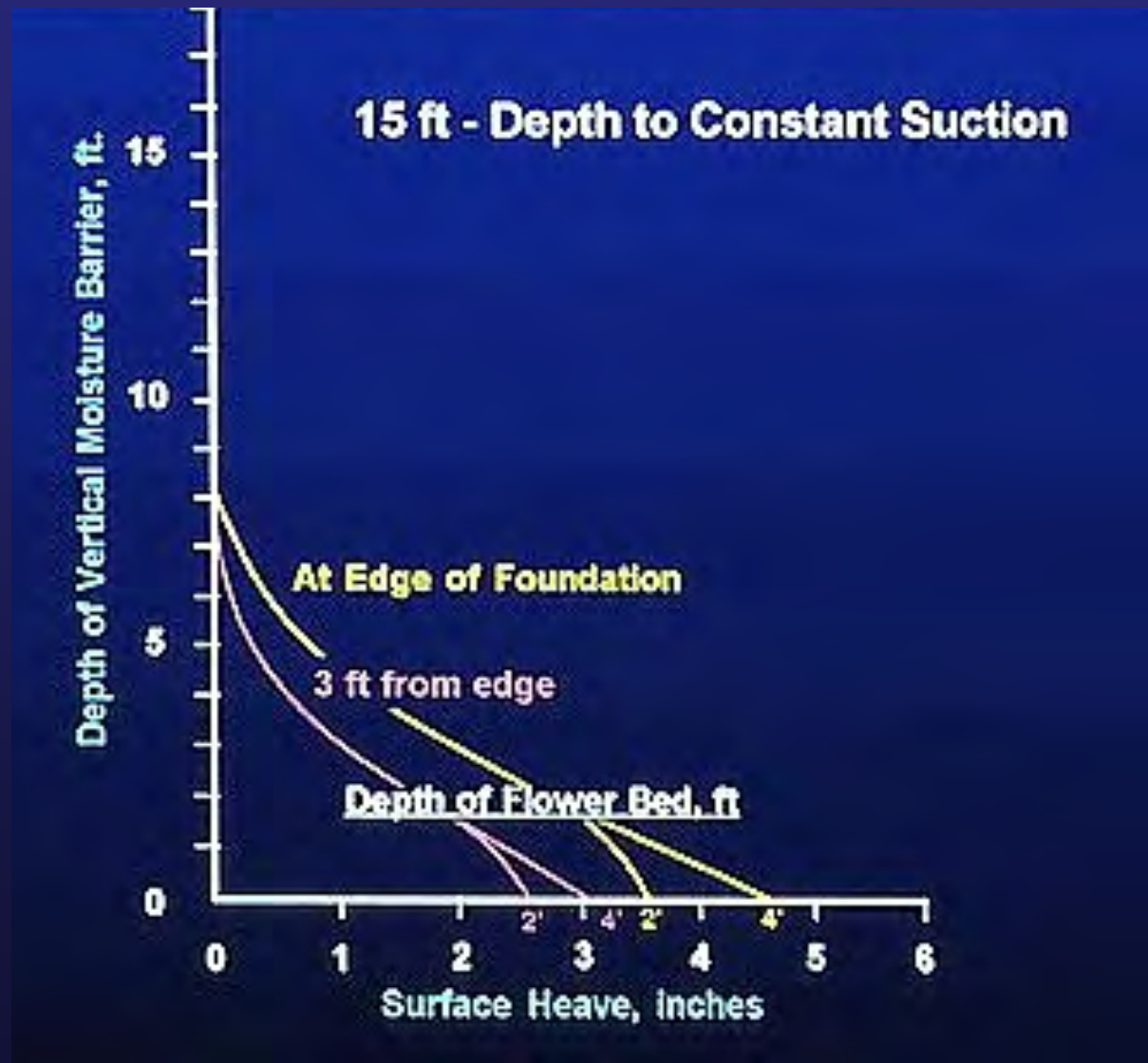




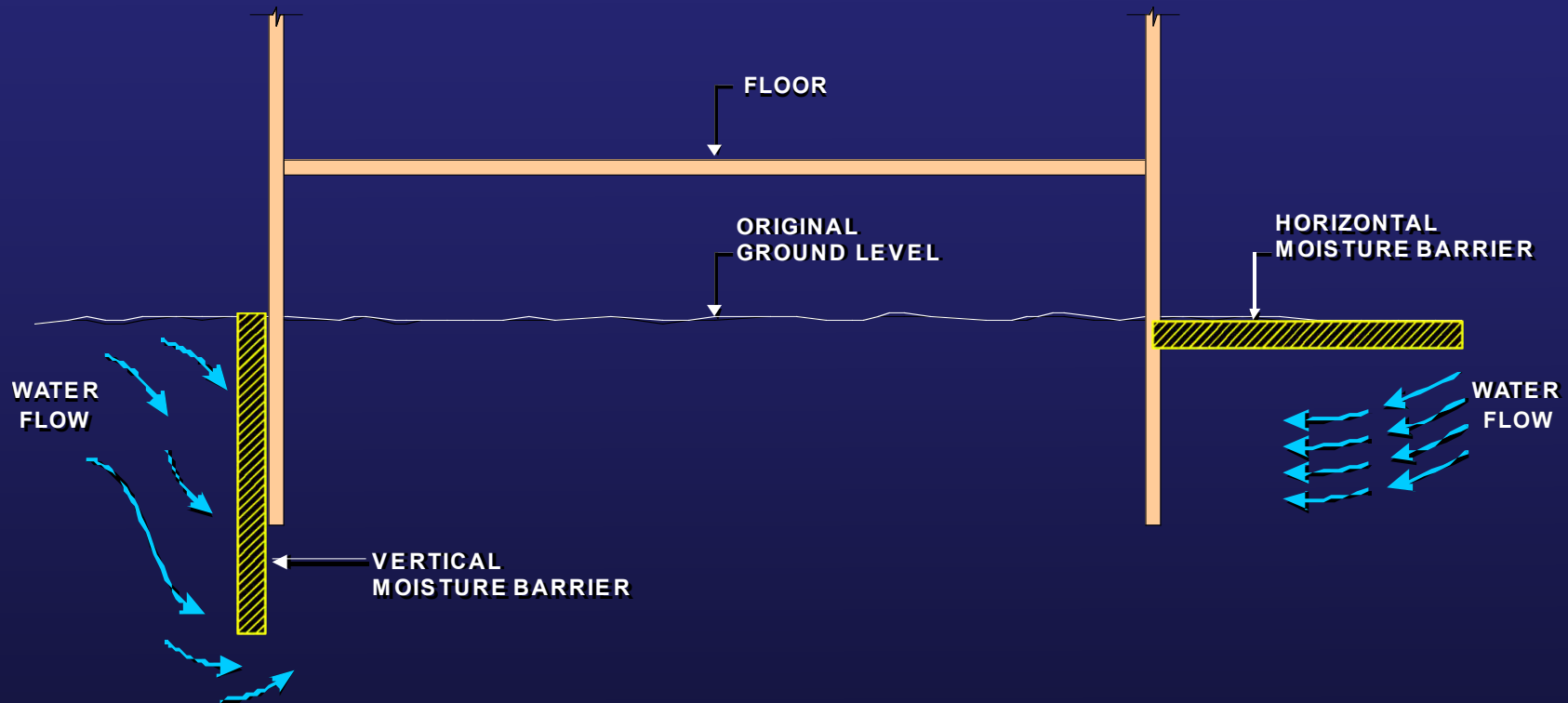
Effects of Flower Beds



Effects of Flower Beds



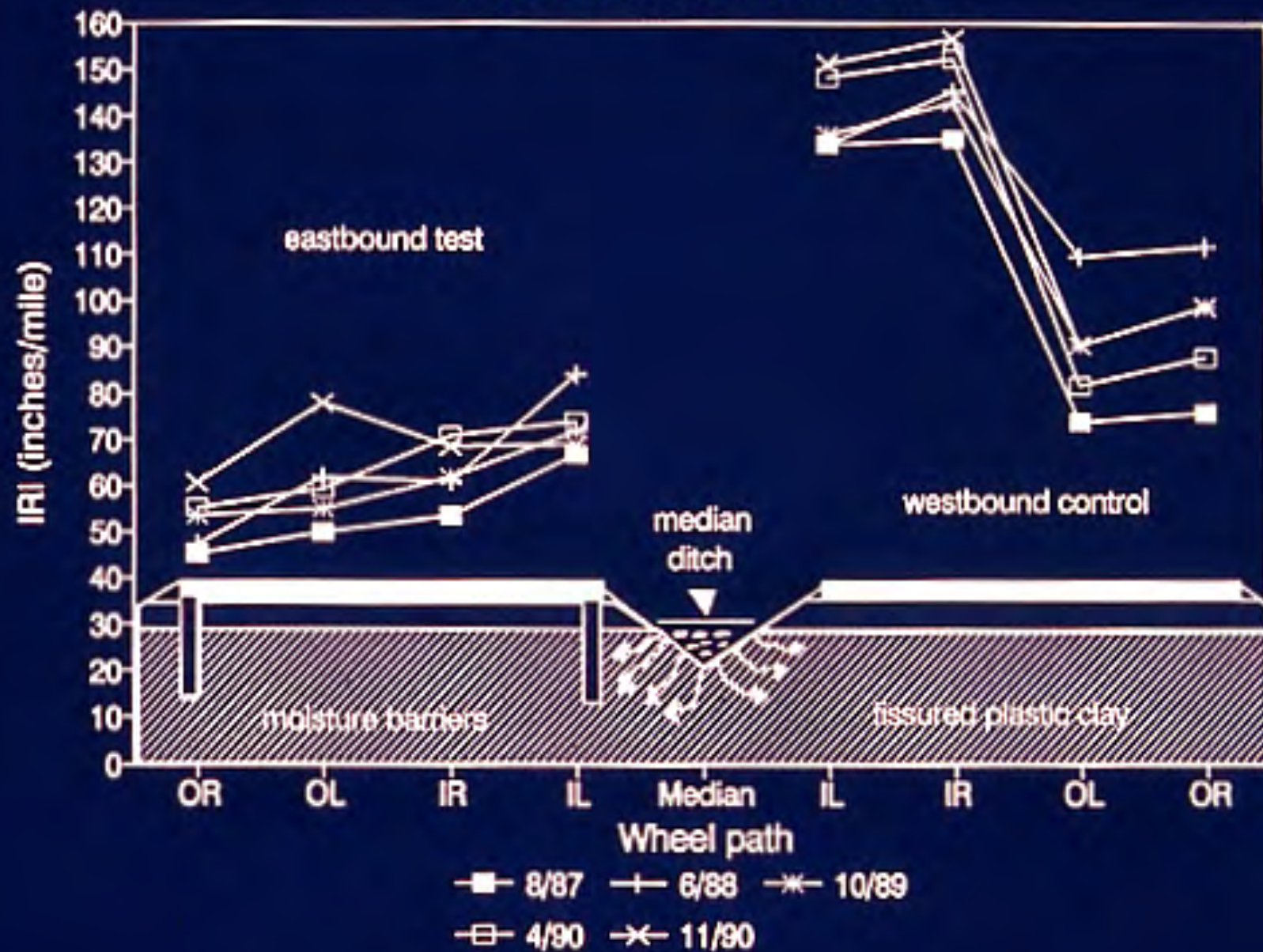
VERTICAL AND HORIZONTAL MOISTURE BARRIERS

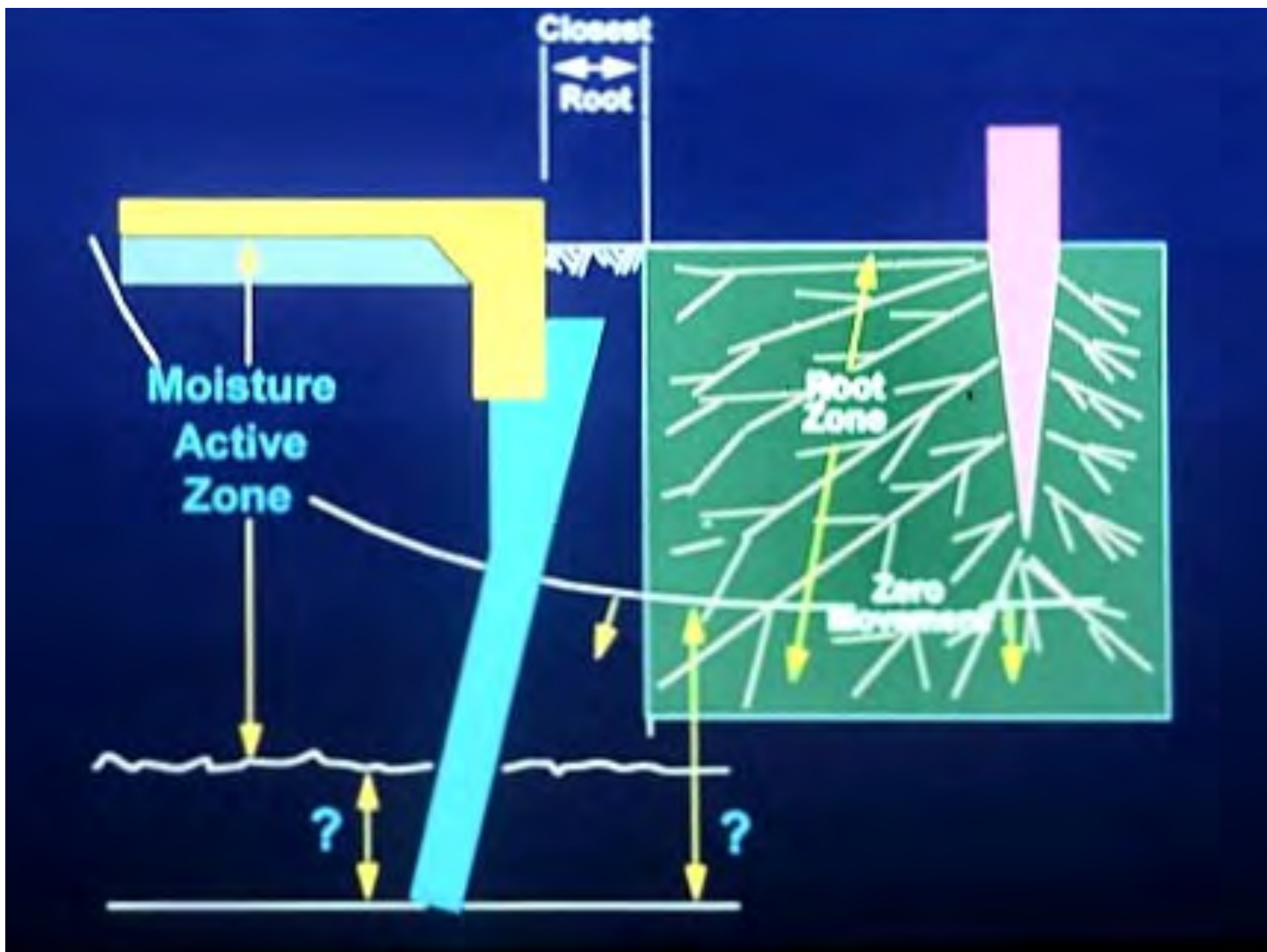


NOTE

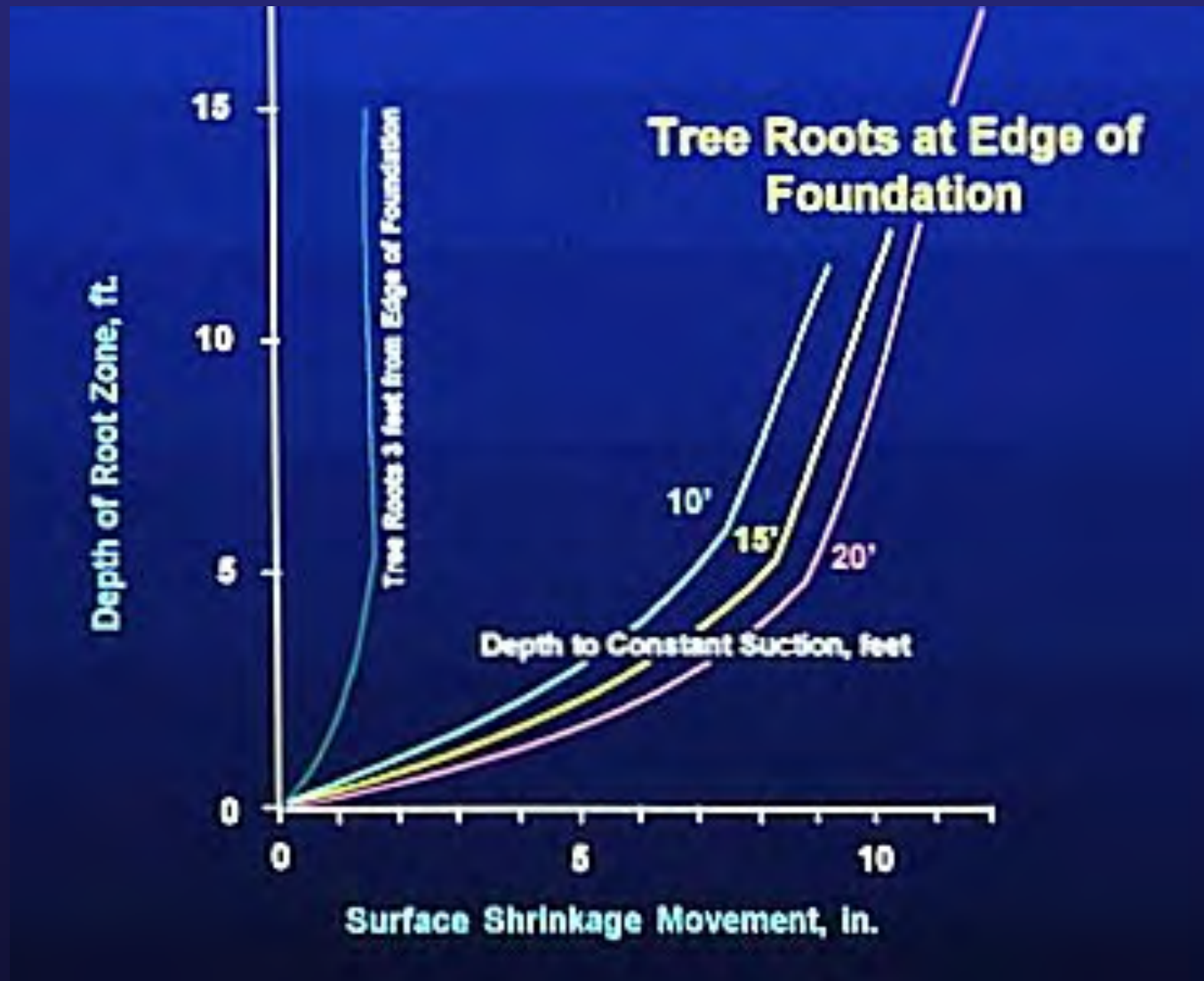
VERTICAL AND HORIZONTAL MOISTURE BARRIERS DECREASE THE AMOUNT OF MOISTURE THAT GETS BENEATH THE WALLS OF THE BUILDING. EFFECTIVE DEPTHS OF VERTICAL MOISTURE BARRIERS ARE BETWEEN 2.5 AND 4 FEET. EFFECTIVE WIDTHS OF HORIZONTAL MOISTURE BARRIERS ARE BETWEEN 4 FEET AND e_m , THE EDGE MOISTURE VARIATION DISTANCE.

IRI cross-section IH-30 Greenville 6 Ft. Fabric

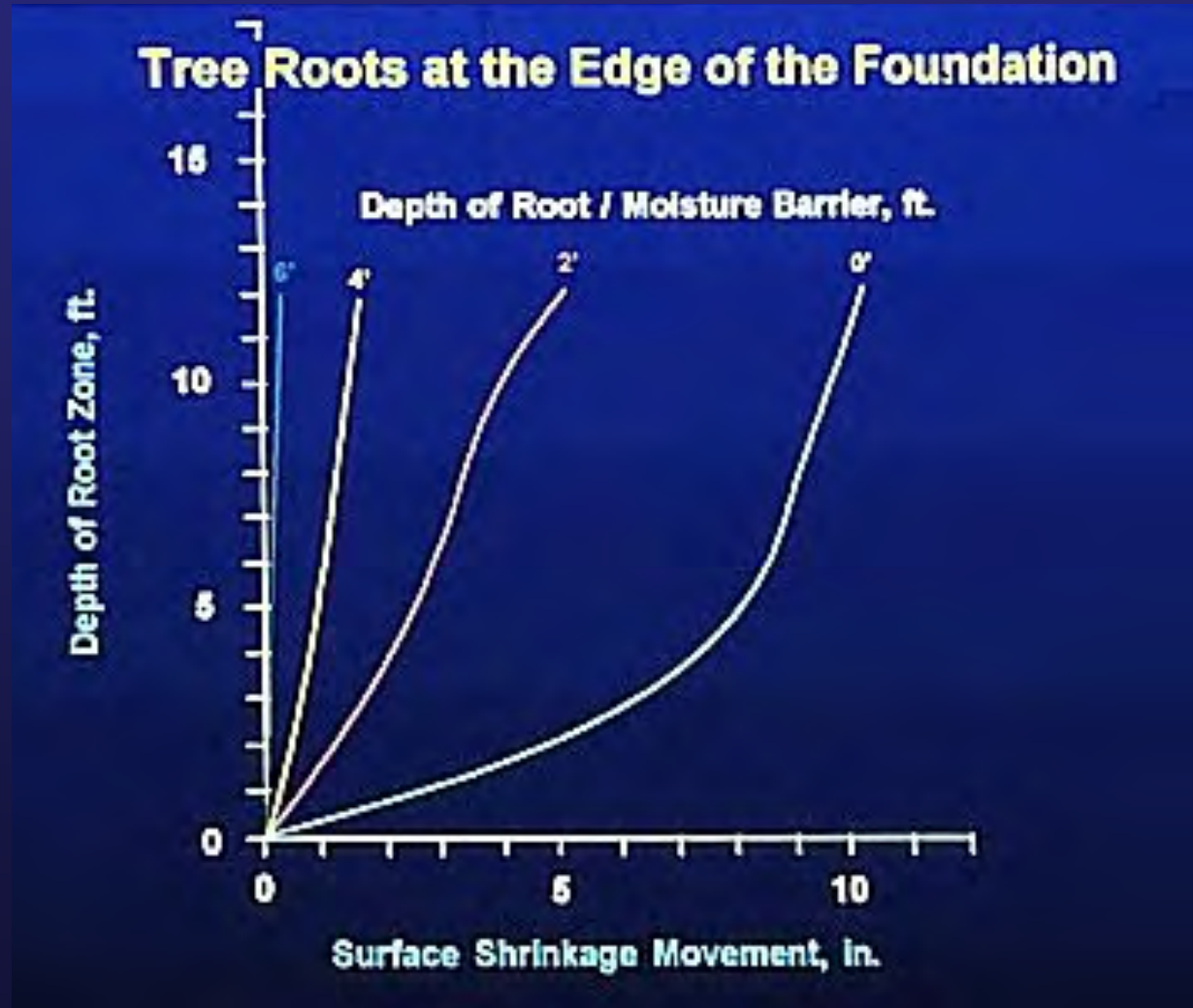




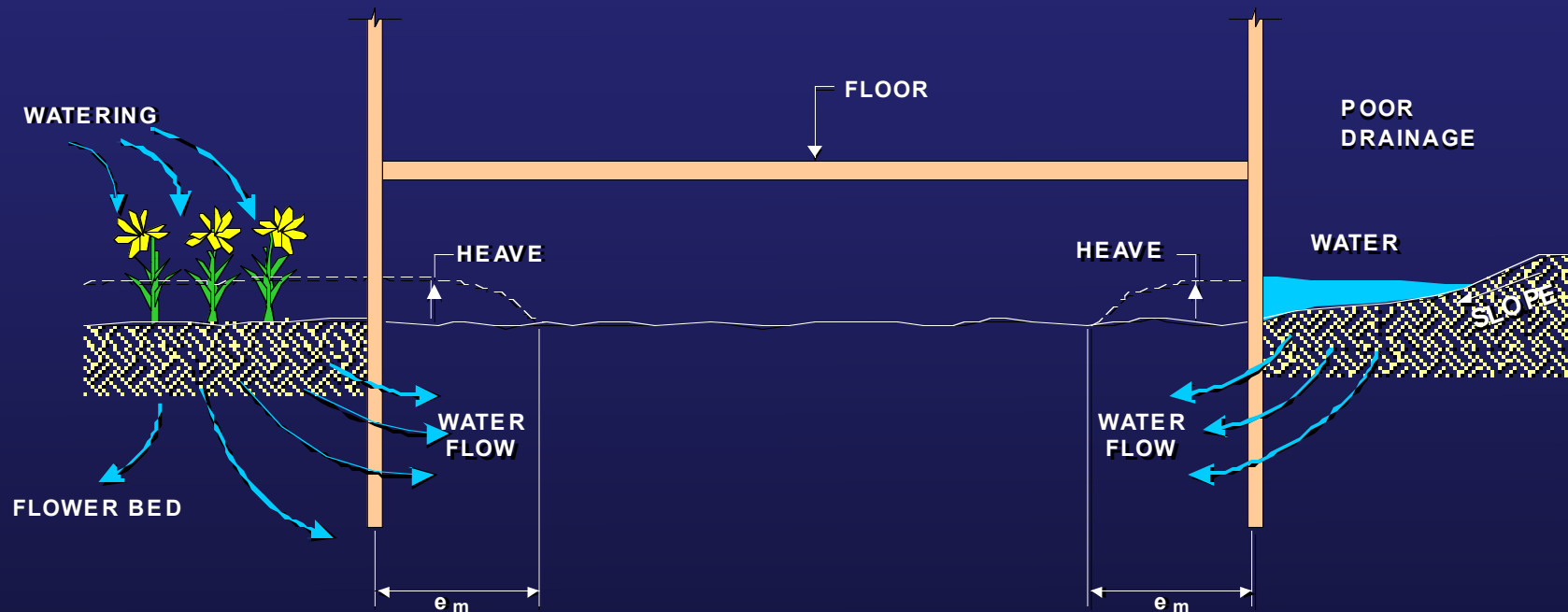
Effects of Trees



Effects of Trees



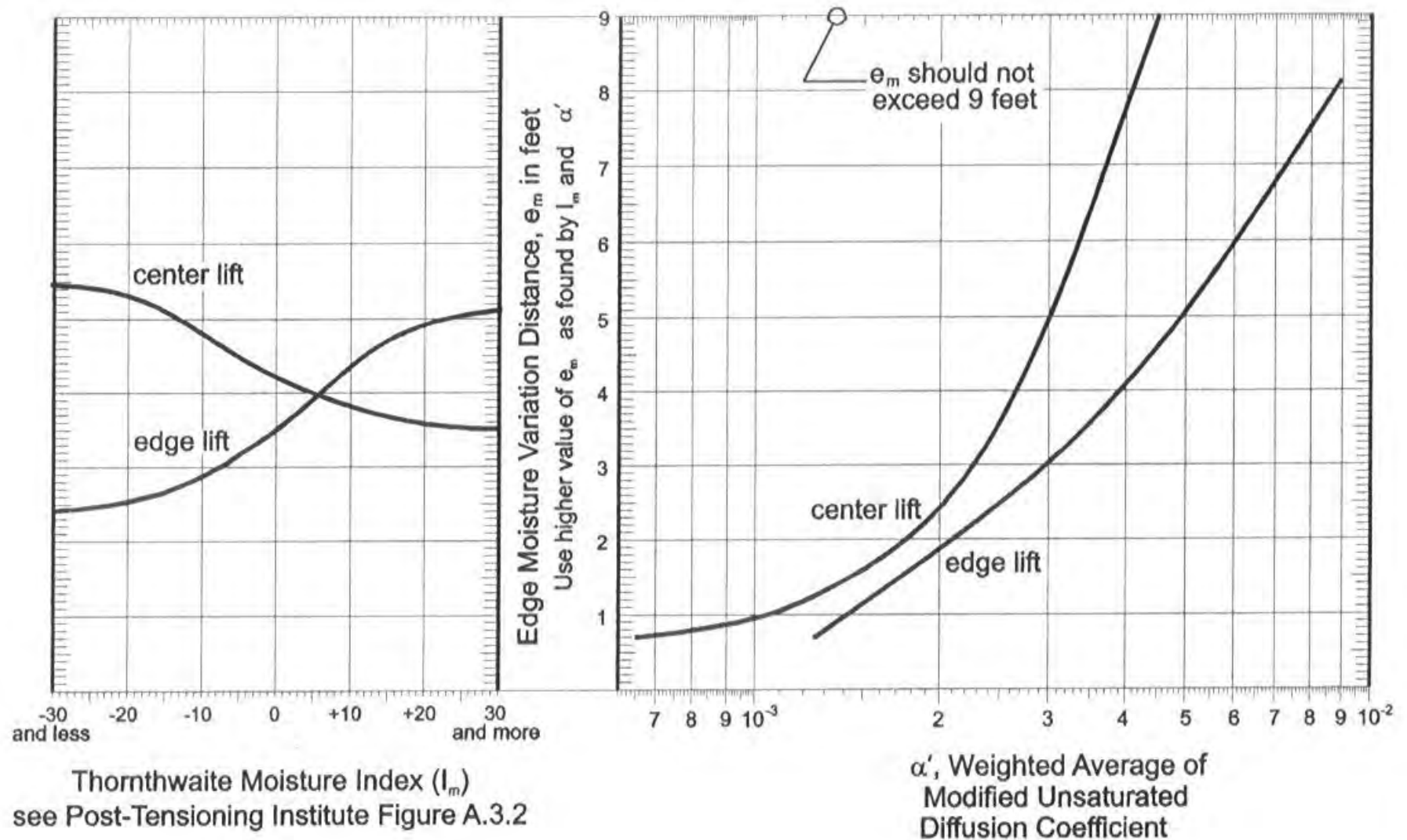
VERTICAL AND HORIZONTAL MOISTURE BARRIERS



NOTE

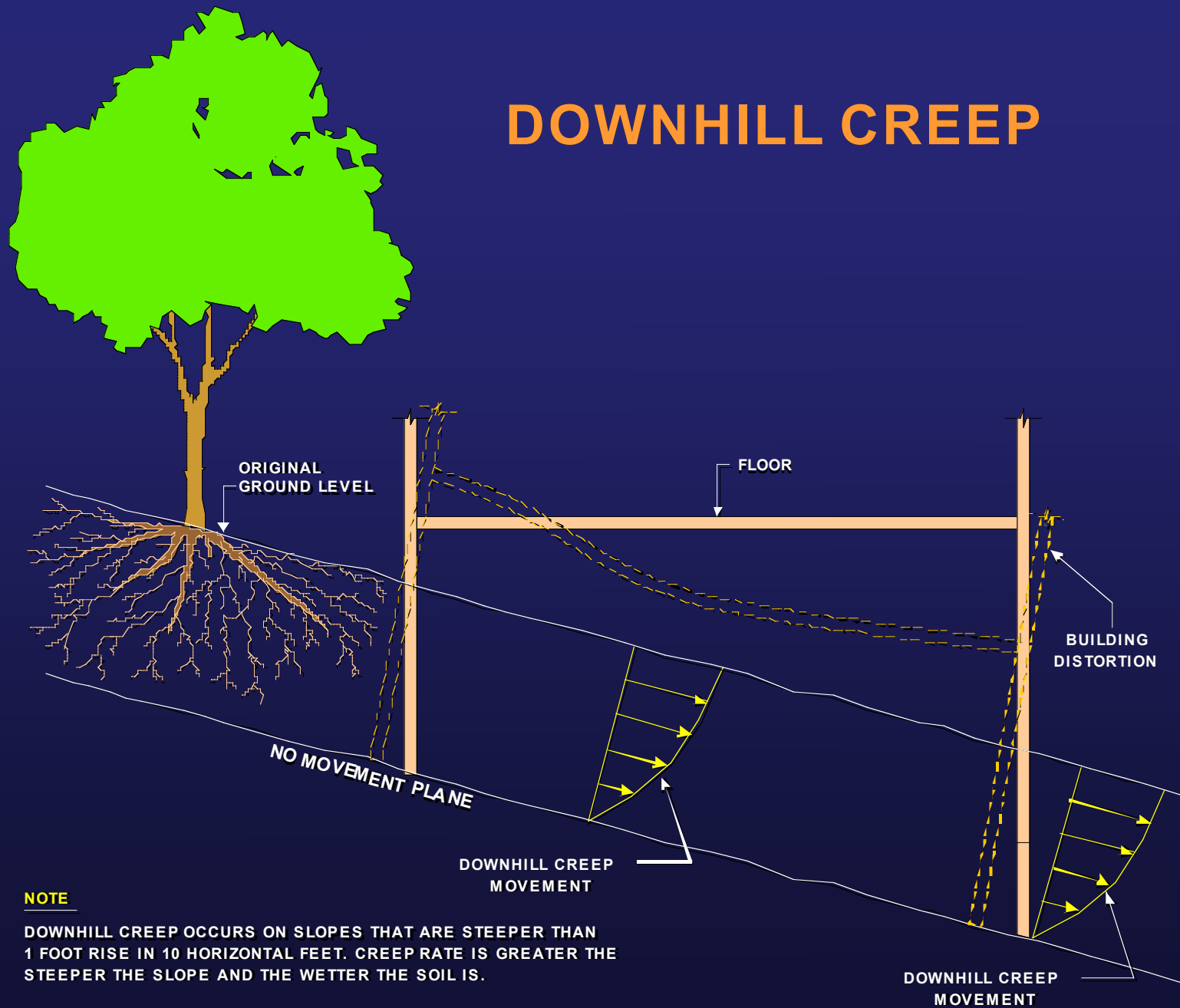
AMOUNT OF HEAVE DEPENDS ON THE AMOUNT OF WATER THAT IS MADE AVAILABLE TO THE SOIL AT THE EDGE OF THE BUILDING AND THE TYPE OF SOIL. e_m IS THE EDGE MOISTURE VARIATION DISTANCE WHICH VARIES TYPICALLY BETWEEN 3 AND 9 FEET DEPENDING ON THE TYPE OF SOIL.

Figure 8 - e_m Selection Chart





DOWNHILL CREEP

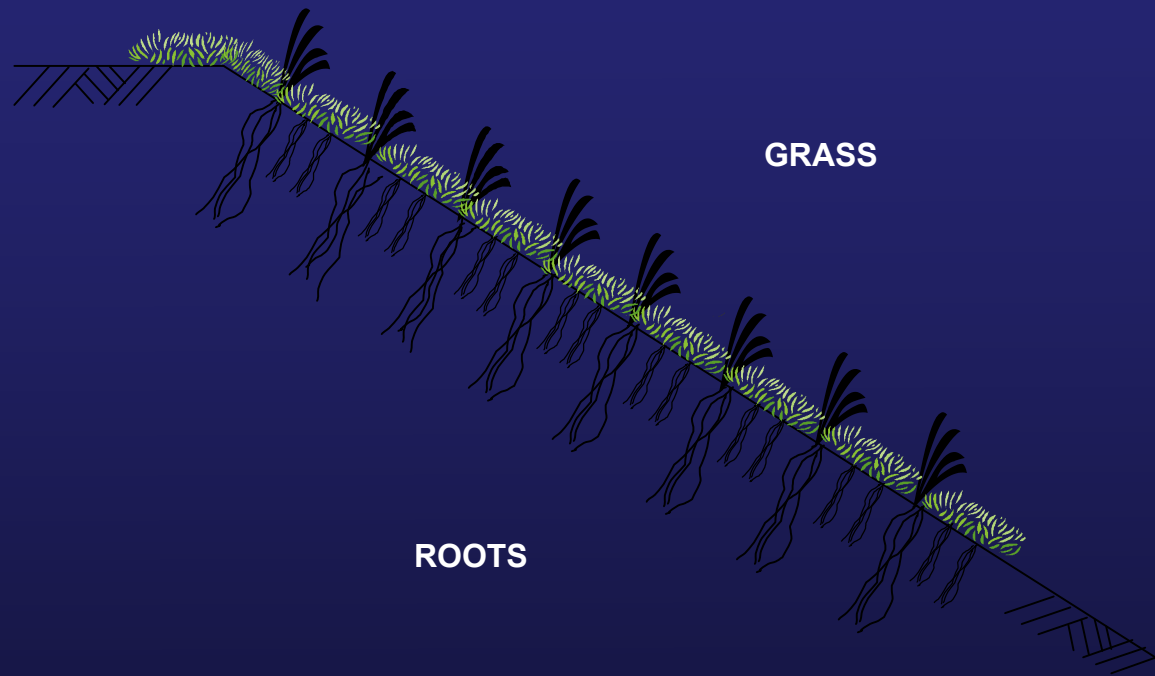


NOTE

DOWNHILL CREEP OCCURS ON SLOPES THAT ARE STEEPER THAN 1 FOOT RISE IN 10 HORIZONTAL FEET. CREEP RATE IS GREATER THE STEEPER THE SLOPE AND THE WETTER THE SOIL IS.

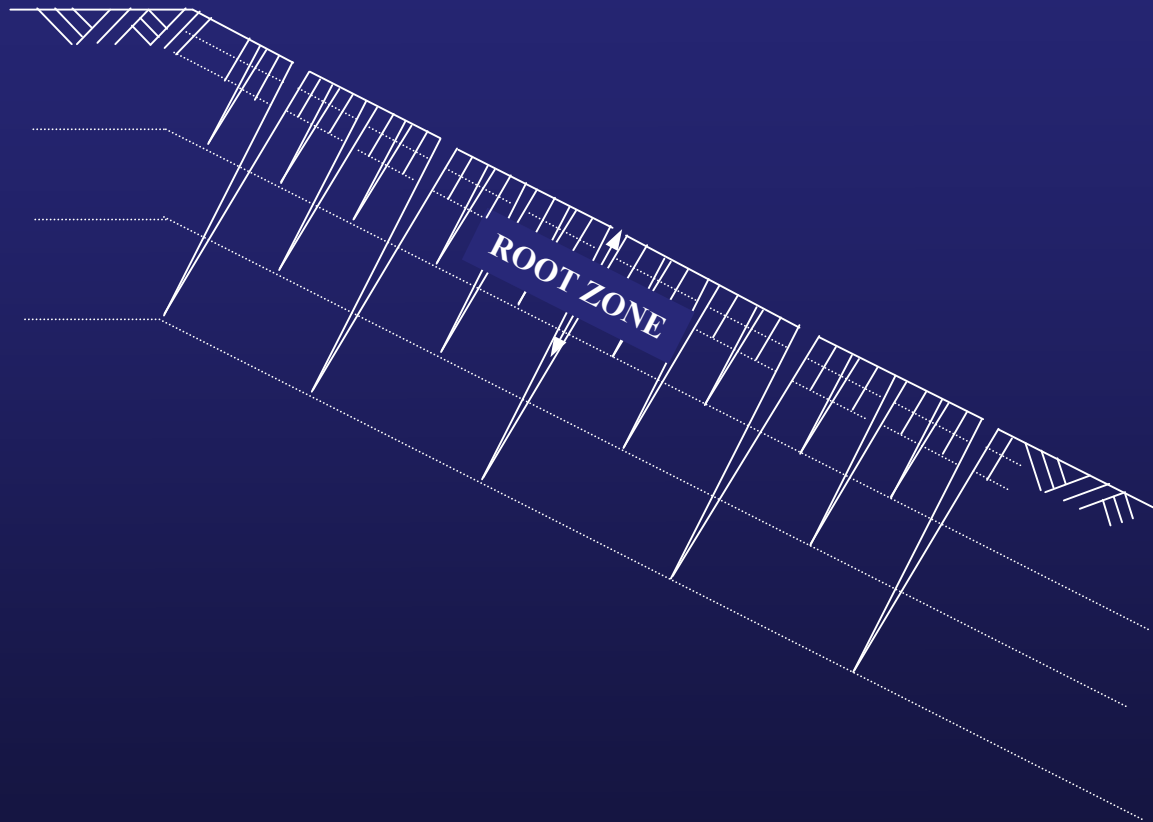


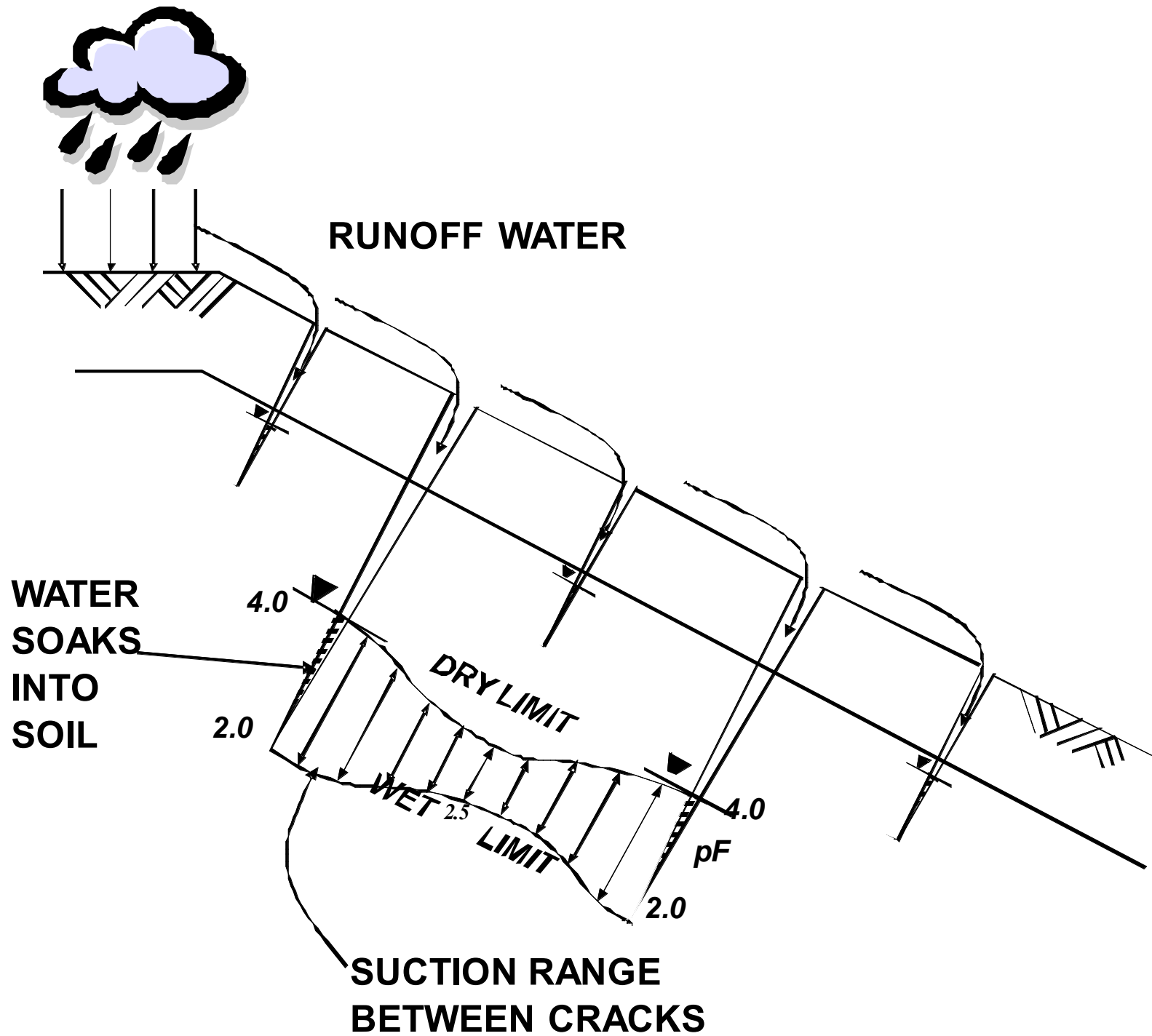
Shallow Slope Failure



**During dry periods roots extract water
From the soil and cause shrinkage cracks**

Crack Spacing Gets Larger with Depth





Foundation soil properties

Moisture Conditions

- ▣ Beside Raised Floors
- ▣ Beneath Raised Floors

Differential Movements

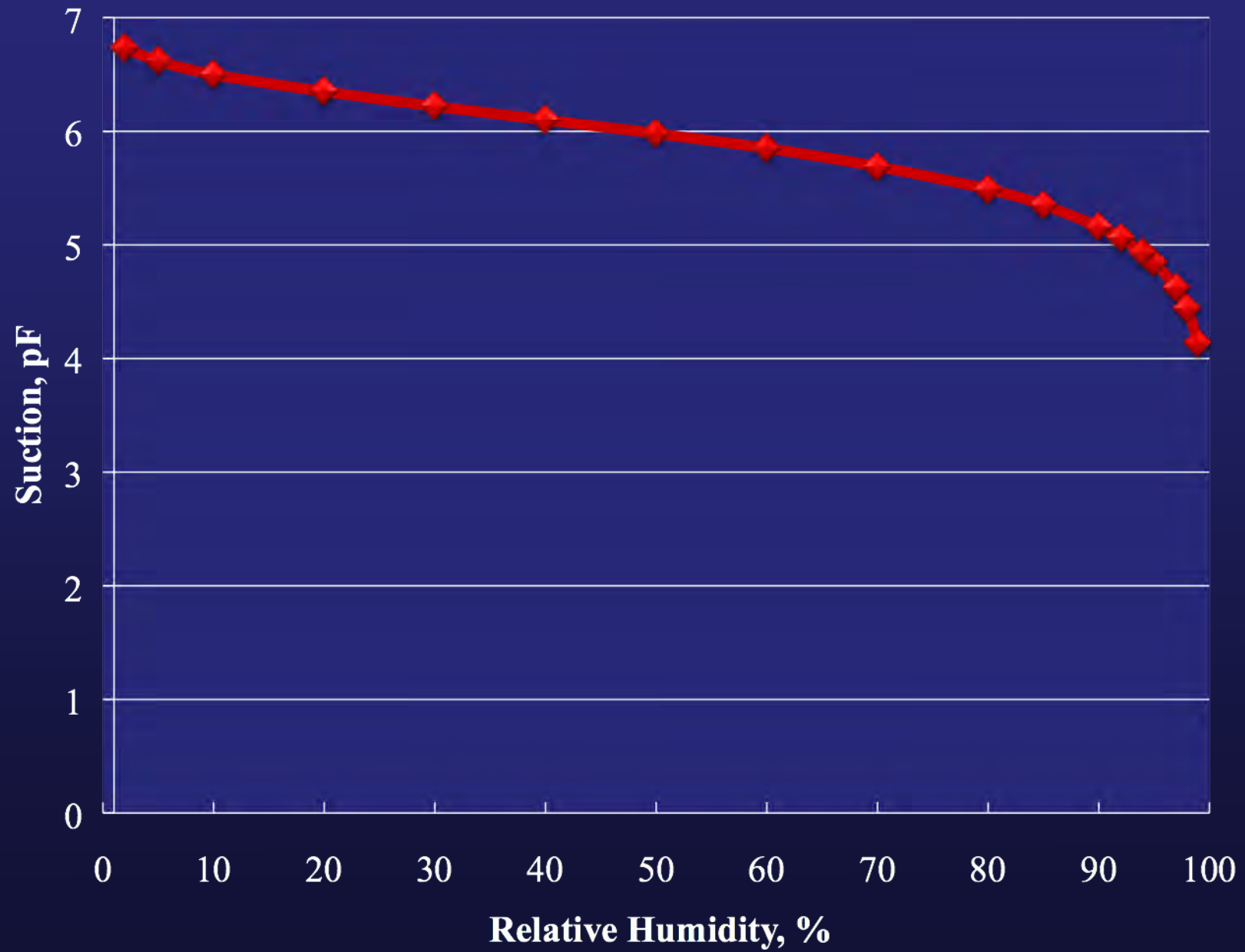
Soil Properties

Site Investigation

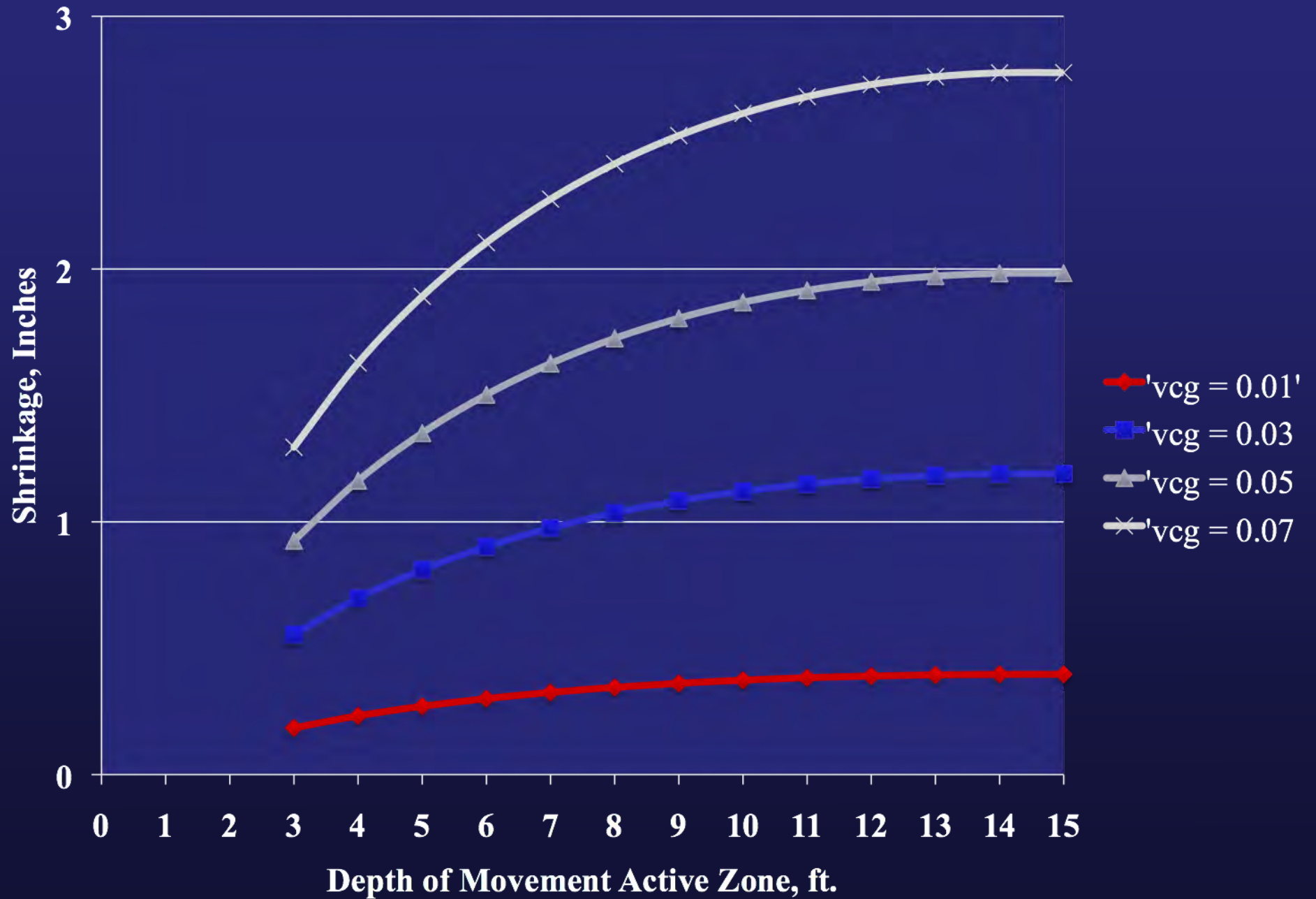
Raised Floor Foundation Boundary Conditions

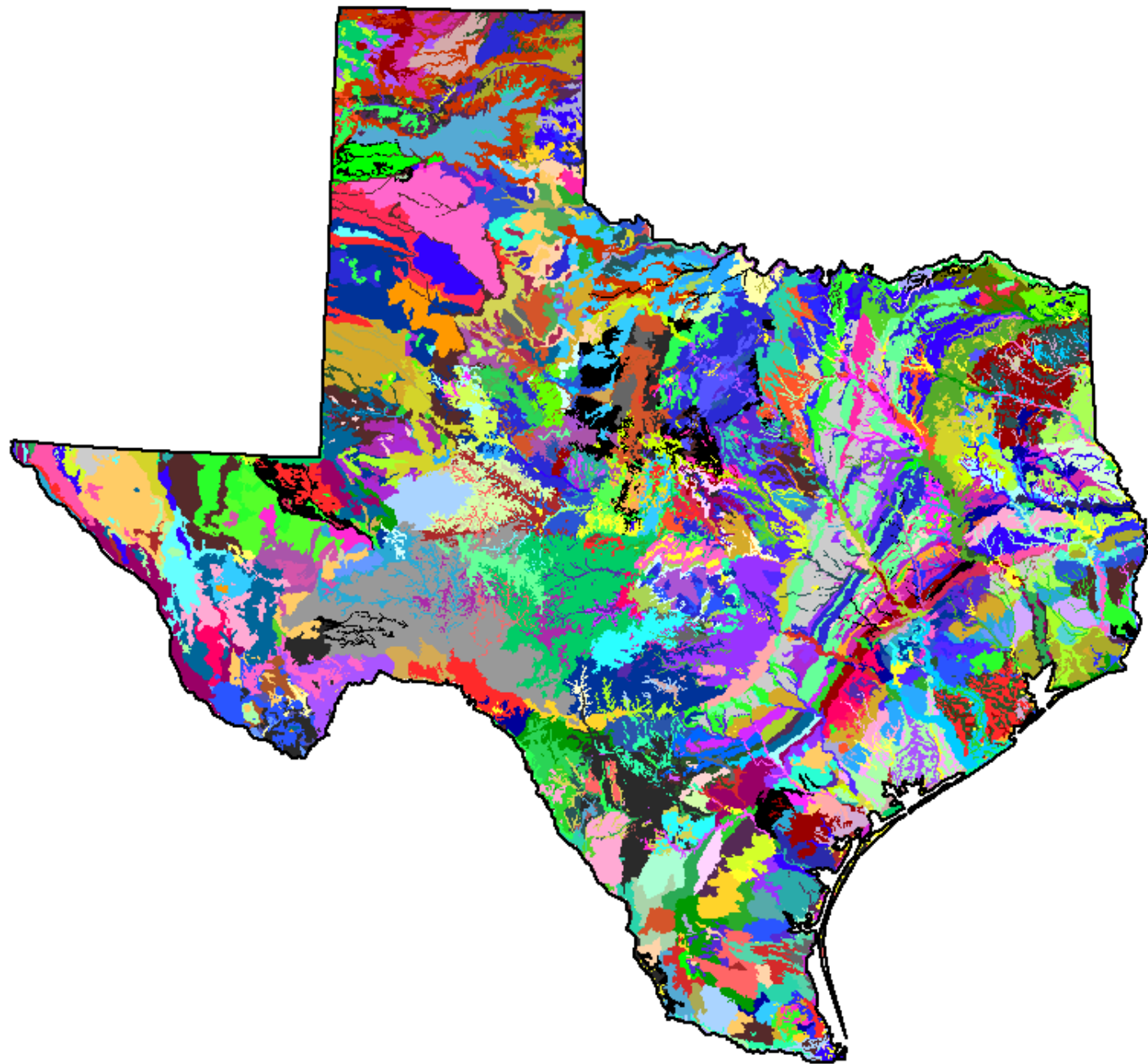
<u>OUTSIDE</u>	<u>pF</u>	<u>pF DRY</u>	<u>R.H.</u>
<u>WET</u>		<u>BENEATH, %</u>	
FLOWER BED	2.9	6.50	10
LAWN WATER	3.0	6.35	20
TREE	4.5	6.22	30
		6.10	40
		5.98	50

Suction, pF vs Relative Humidity, %




Shrinkage, in. vs Depth of Active Zone, ft.





YaA	Yahola fine sandy loam, 0 to 1 percent slopes, rarely flooded	858.7	0.2%
ZaB	Zack fine sandy loam, 1 to 5 percent slopes	11,763.7	3.1%
ZaC2	Zack fine sandy loam, 2 to 5 percent slopes, eroded	1,729.5	0.5%
ZaD	Zack fine sandy loam, 5 to 8 percent slopes	3,194.0	0.8%
ZaE3	Zack fine sandy loam, 8 to 25 percent slopes, severely eroded	269.9	0.1%
ZcB	Zack-Urban land complex, 1 to 5 percent slopes	7,841.9	2.1%
ZcD	Zack-Urban land complex, 5 to 8 percent slopes	547.6	0.1%
ZuB	Zulch fine sandy loam, 1 to 3 percent slopes	11,440.6	3.0%
Totals for Area of Interest		377,977.9	100.0%



 **Warning:** Soil Map may not be valid at this scale.


You have zoomed in beyond the scale at which the soil map for this area is intended to be used. Mapping of soils is done at a particular scale. The soil surveys that comprise your AOI were mapped at 1:20,000. The design of map units and the level of detail shown in the resulting soil map are dependent on that map scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Outline

- Elements of design
- Site conditions
- Slabs-on-ground
- Raised floor foundations
- costs

Elements of Design

- Structural requirements
 - Moments
 - Shear
 - Deflection

As determined by site conditions
- Costs

Site Conditions

- Soils
- Site hazards
 - Trees
 - Slopes
 - Drainage
- Building geometry

Contrasting Design Approaches for Slab-on-Ground and Raised Floor Foundations on Expansive Soils

Robert L. Lytton

Houston Foundation Performance Association

Houston, Texas

December 9, 2009