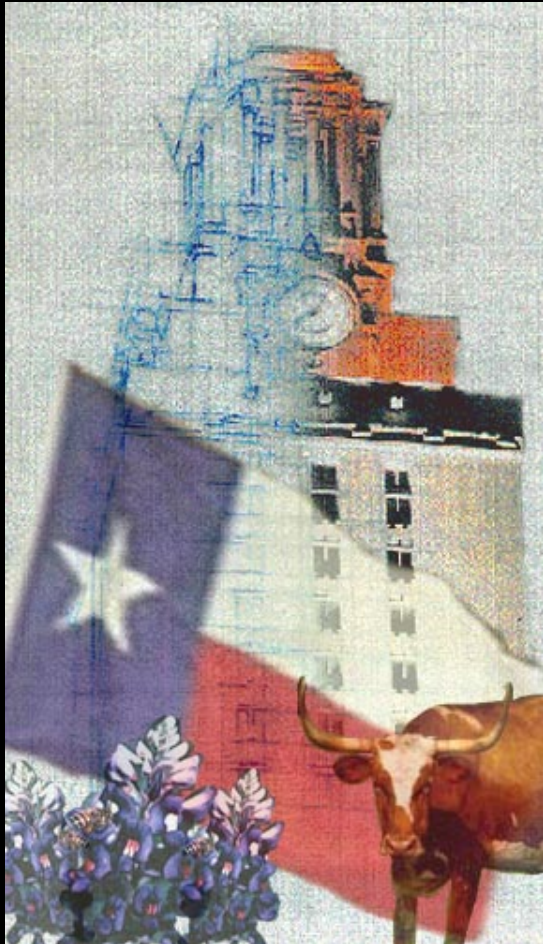


# Characterizing Geotechnical Materials with Seismic Waves: Static and Dynamic Applications



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**Civil, Architectural and**  
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**University of Texas at Austin**

***Foundation Performance Association***  
***Houston, TX***  
***8 November 2017***

# Outline

## 1. Brief Background

- **emphasize small-strain field measurements**
- **laboratory tests used for parametric studies**

## 2. Present a Number of Examples

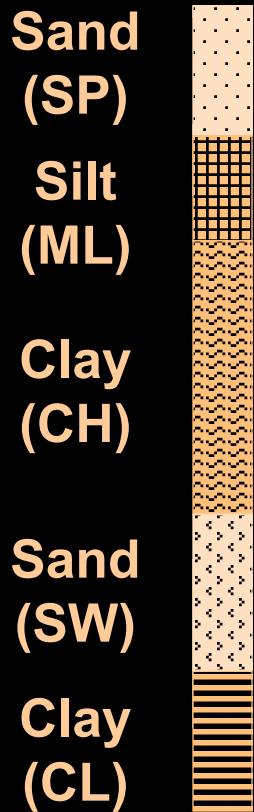
- **static and dynamic problems**

## 3. Show the Link Between Field and Laboratory Seismic Measurements

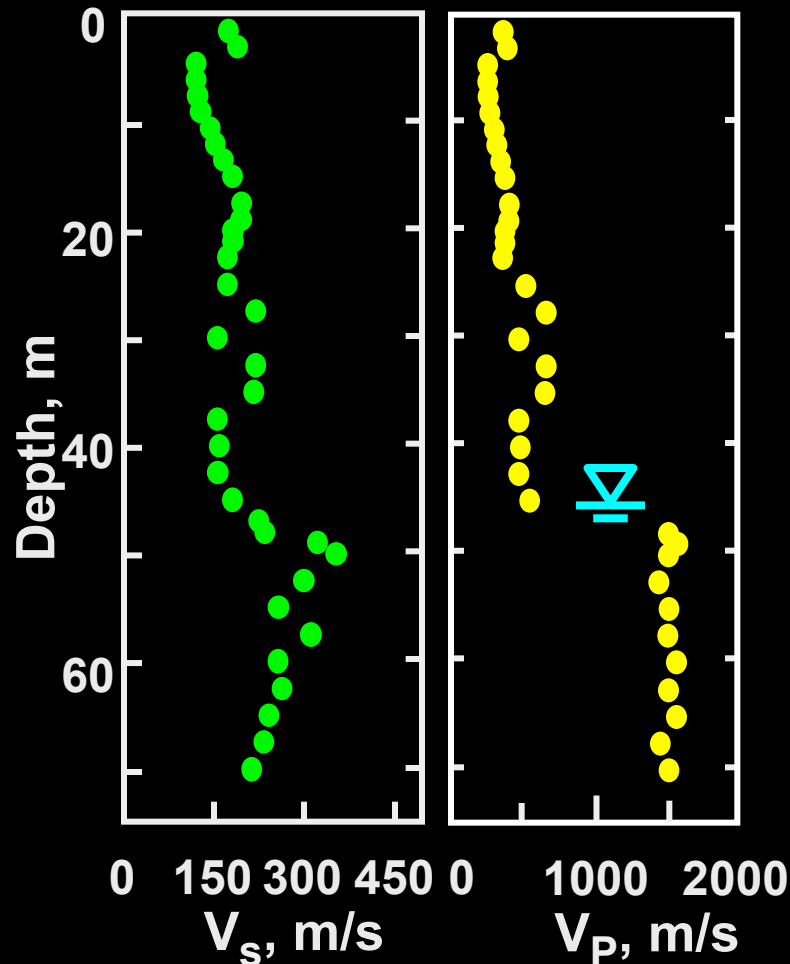
## 4. Concluding Remarks

# 1. Background: Field and Laboratory Seismic (Stress Wave) Measurements

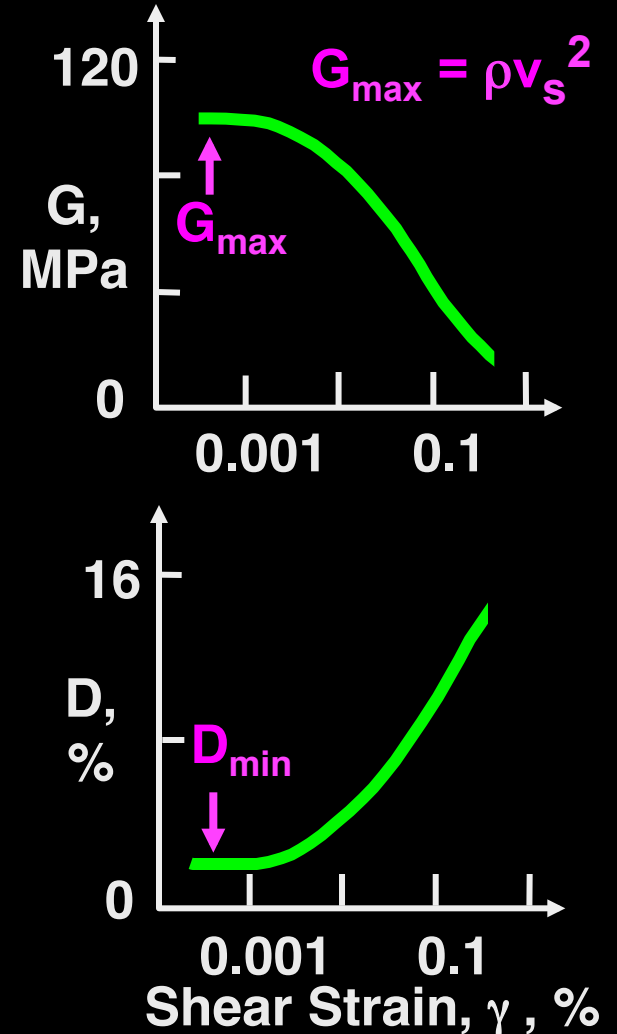
## 1. Soil Profile



## 2. Field: Linear $V_s$ and $V_p$

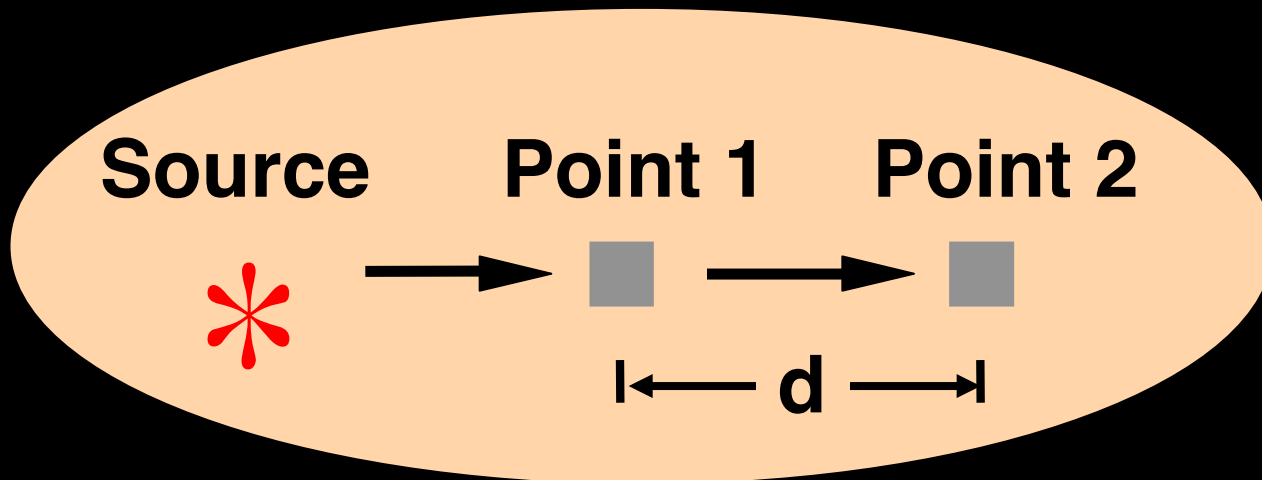


## 3. Lab: Linear and Nonlinear G and D



# 1a. Field: **Seismic Measurements**

**Objective:** **measure time,  $t$ , for a given stress wave to propagate a given distance,  $d$  ... then velocity =  $d/t$**


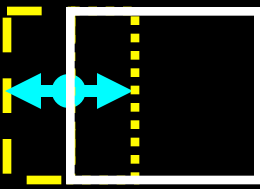
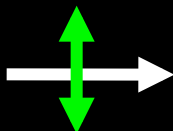
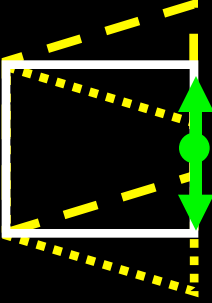


**Key characteristics:**

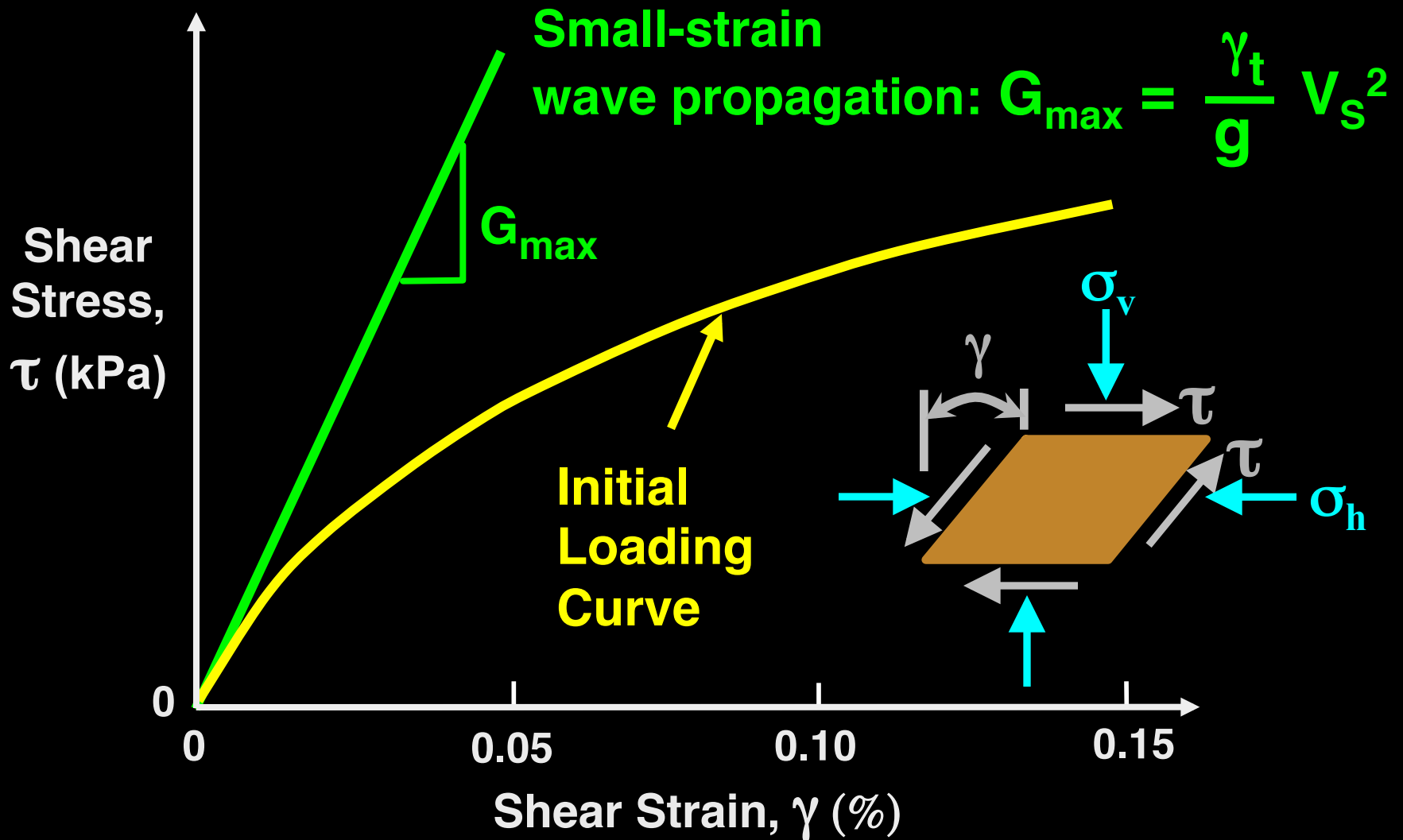
- 1. small-strain (linear) measurements**
- 2. proper sources**
- 3. oriented receivers**



# Field Measurements with Compression (P) and Shear (S) Waves

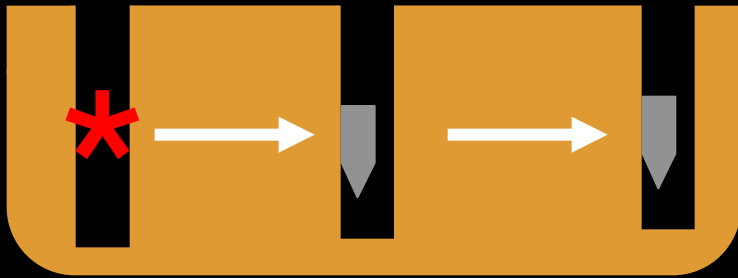
Wave Type	Particle Motion	Distortion	Wave Velocity	Small-Strain Modulus
P			$V_p$	$M_{\max} = \frac{\gamma_t}{g} V_p^2$
S			$V_s$	$G_{\max} = \frac{\gamma_t}{g} V_s^2$

# Small-Strain Seismic Measurements

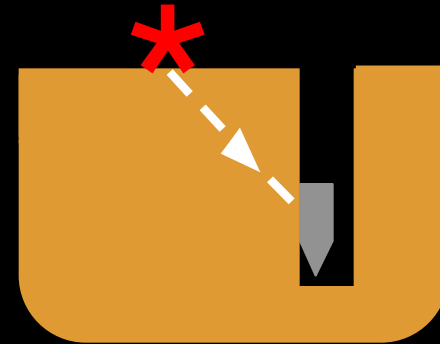


# Field Seismic Methods

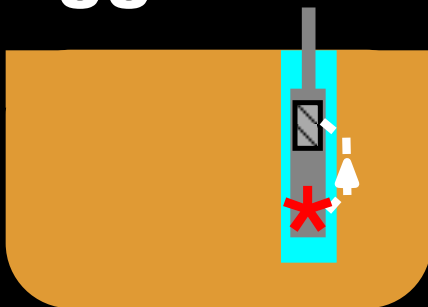
## 1. Crosshole



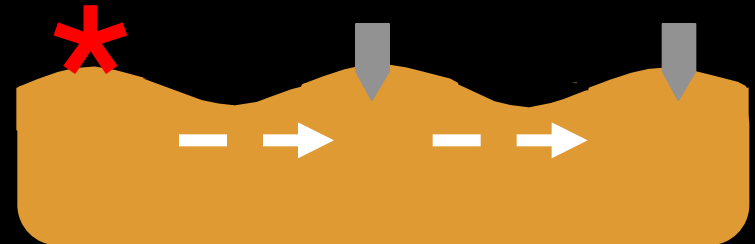
## 2. Downhole (Seismic CPT)



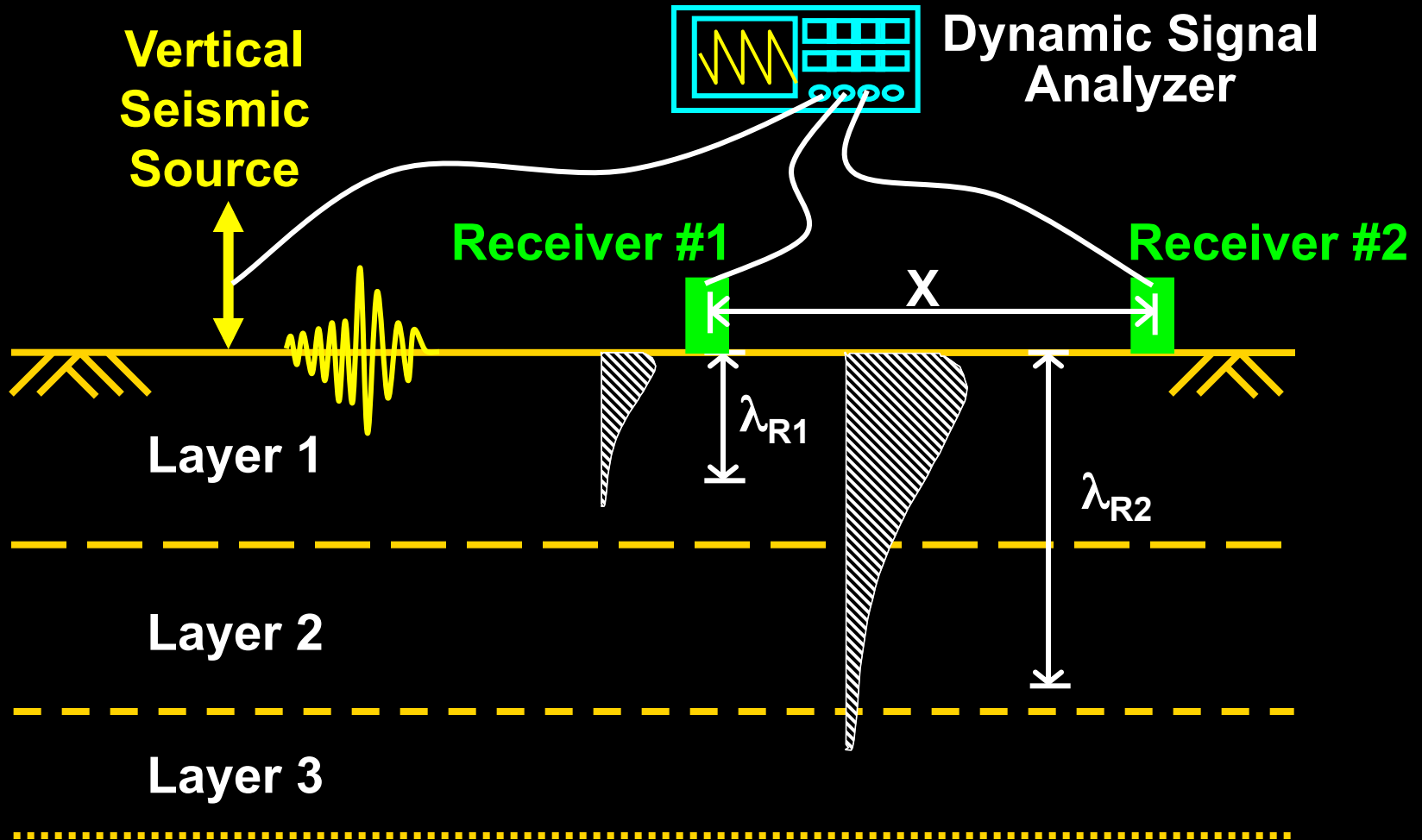
## 3. P-S Suspension Logger



## 4. Surface Waves

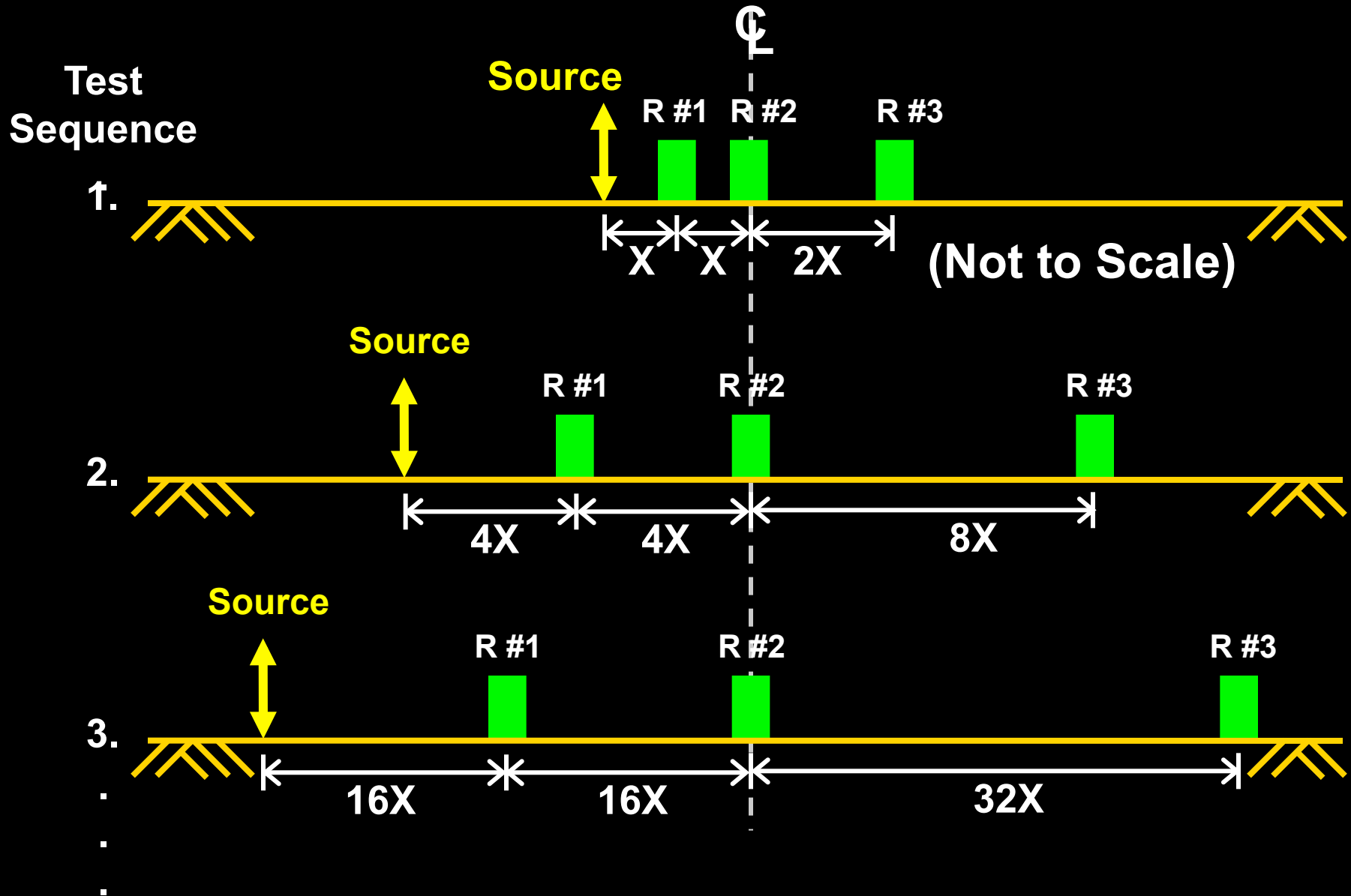


# Overview of SASW<sup>\*</sup>: Generalized Field Arrangement and Sampling



\* SASW = Spectral Analysis of Surface Waves

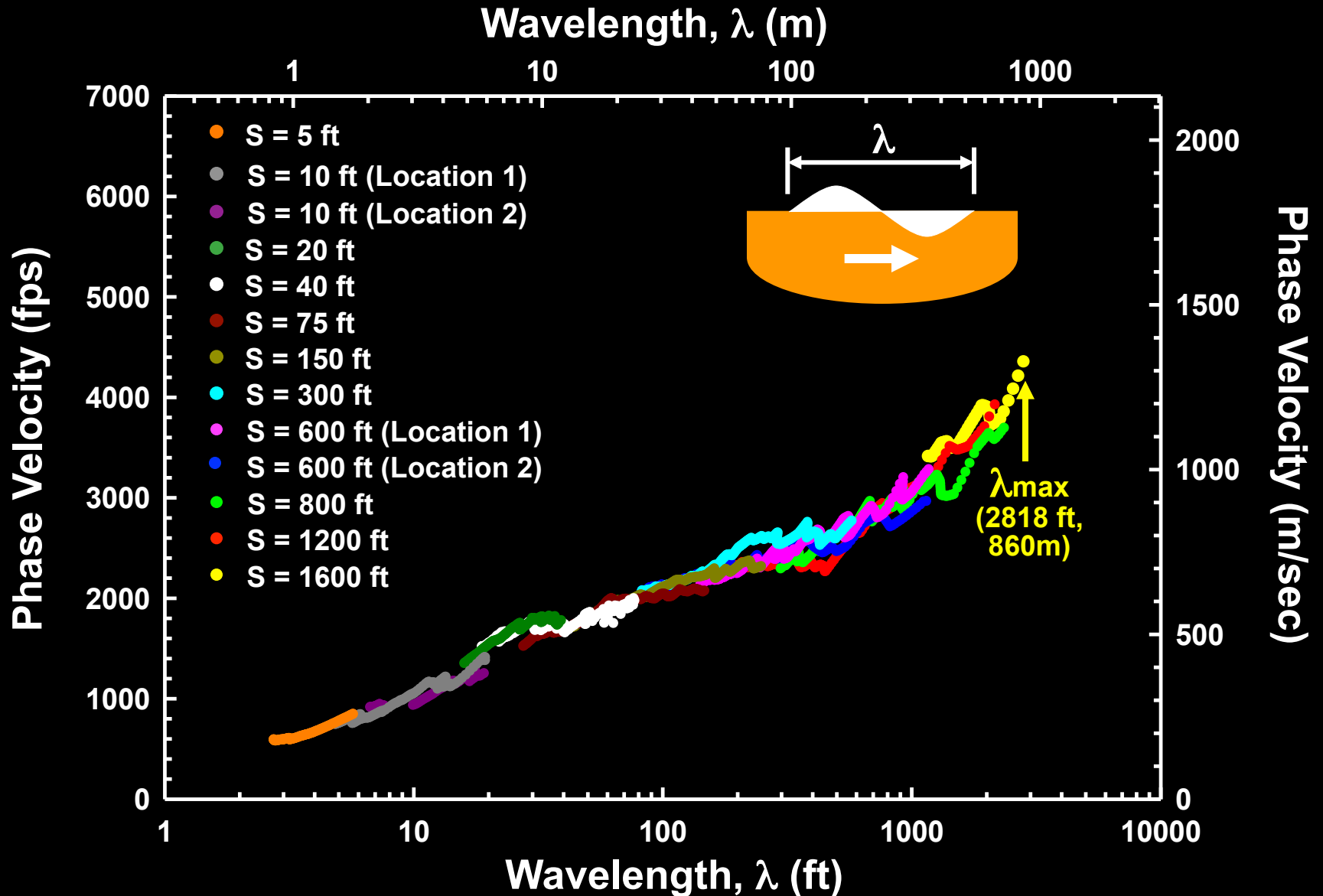
# Multiple Source-Receiver Positions



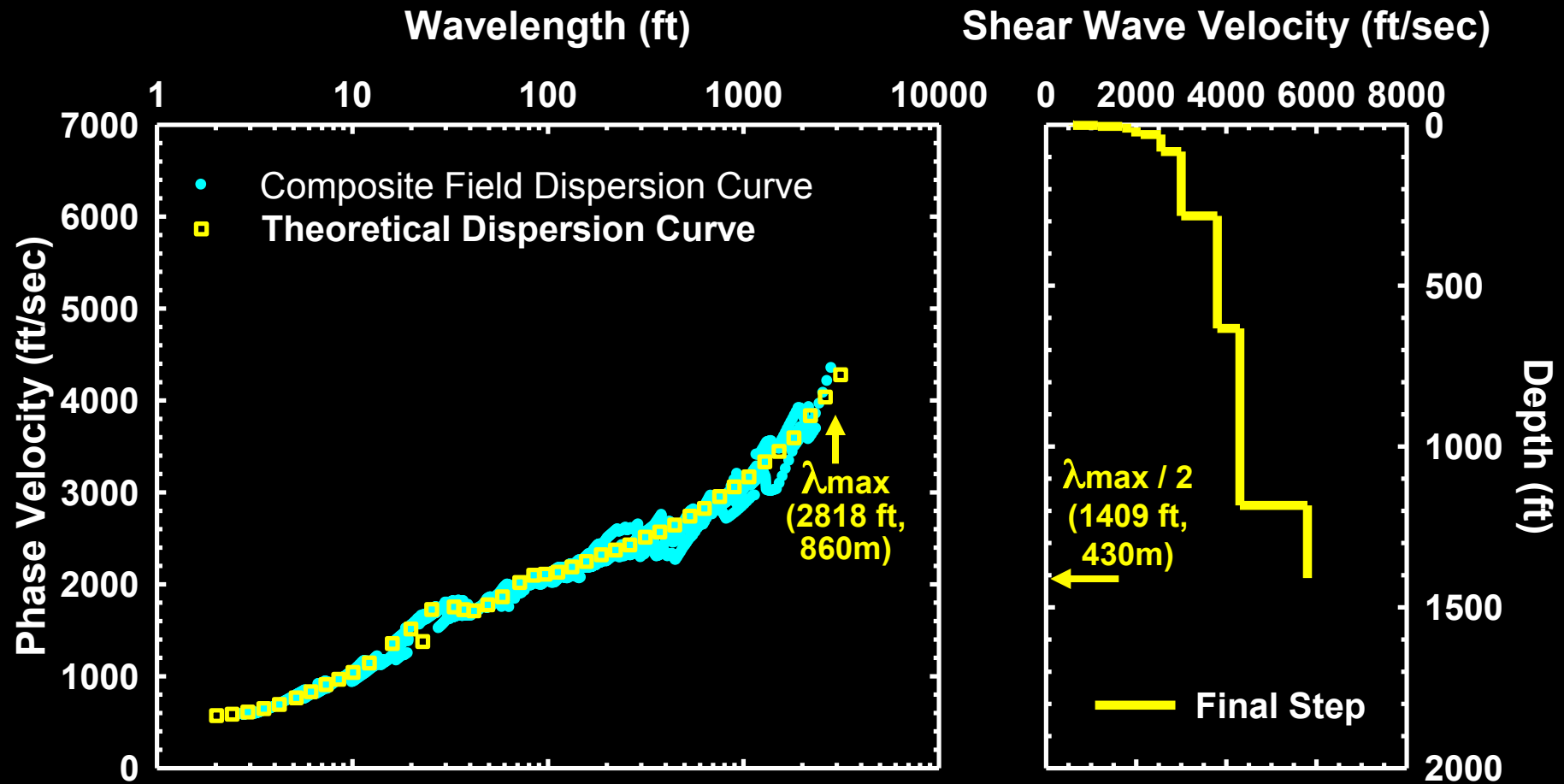
# Liquidator Working as a Seismic Source on Top of Yucca Mountain



# Composite Field Dispersion Curve Generated from All Receiver Spacings

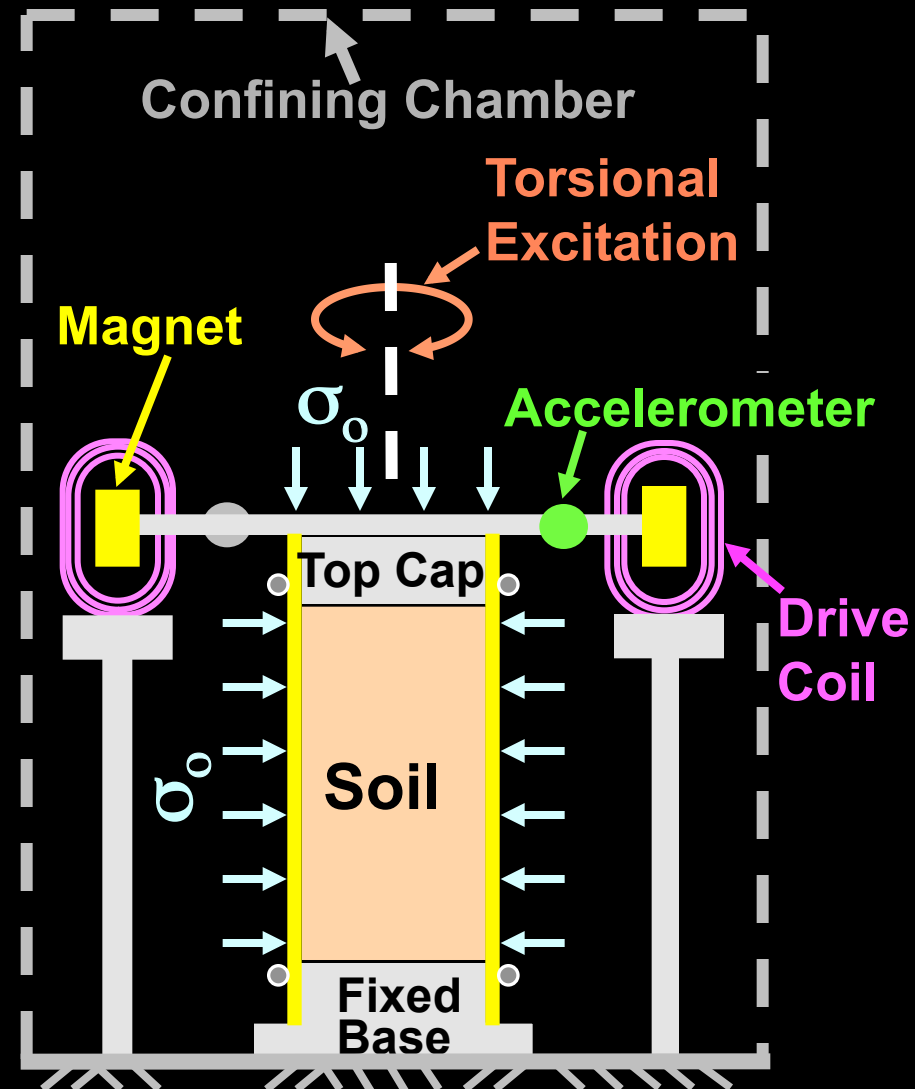
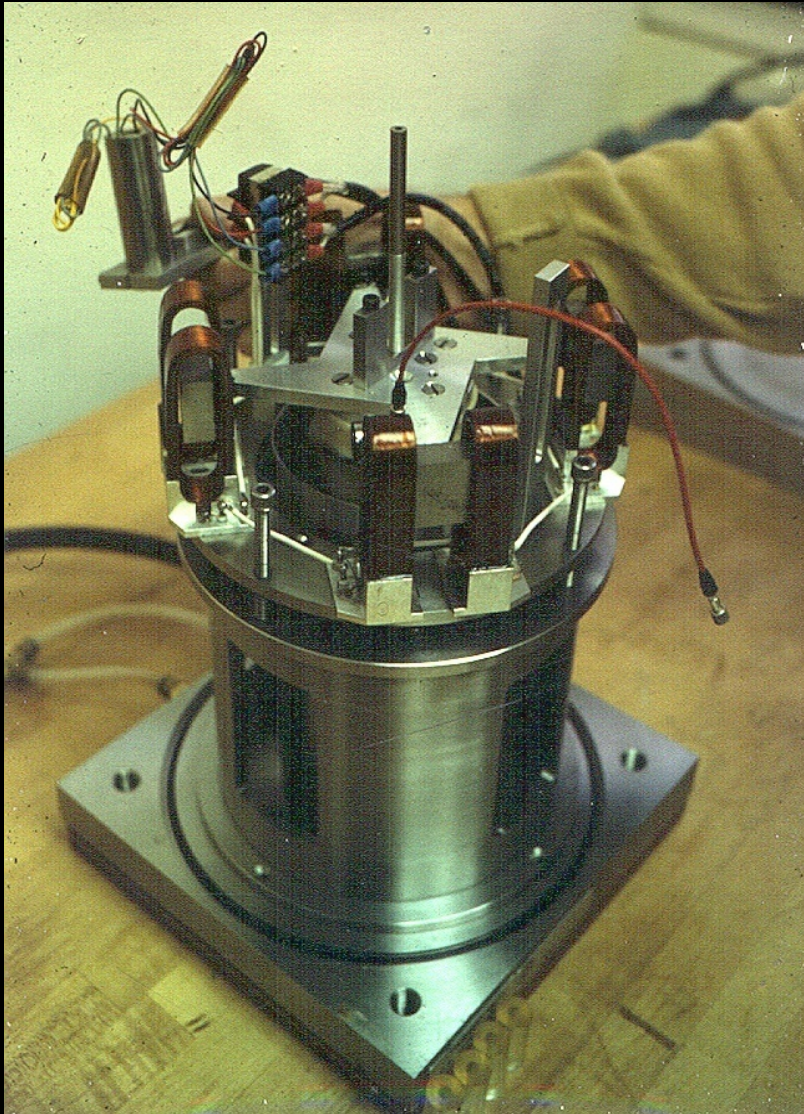


# Best-Match Theoretical Dispersion Curve (Final Step in Forward Modeling)



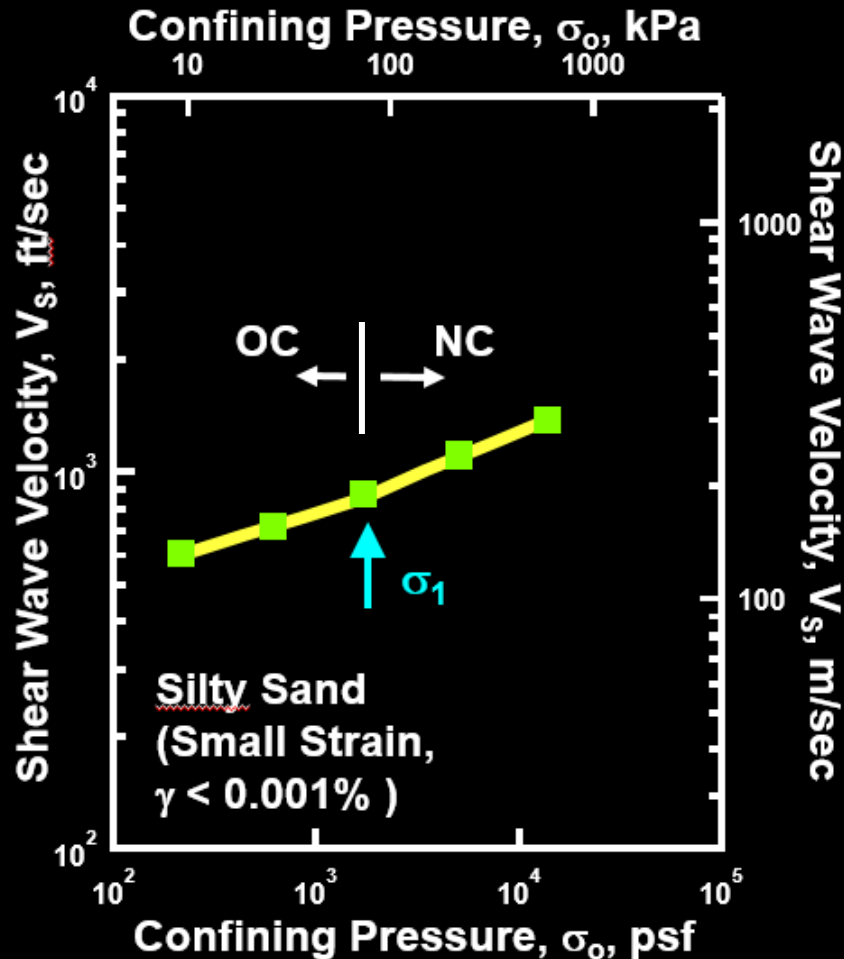


# 1b. Laboratory: Combined Resonant Column and Torsional Shear (RCTS) Test

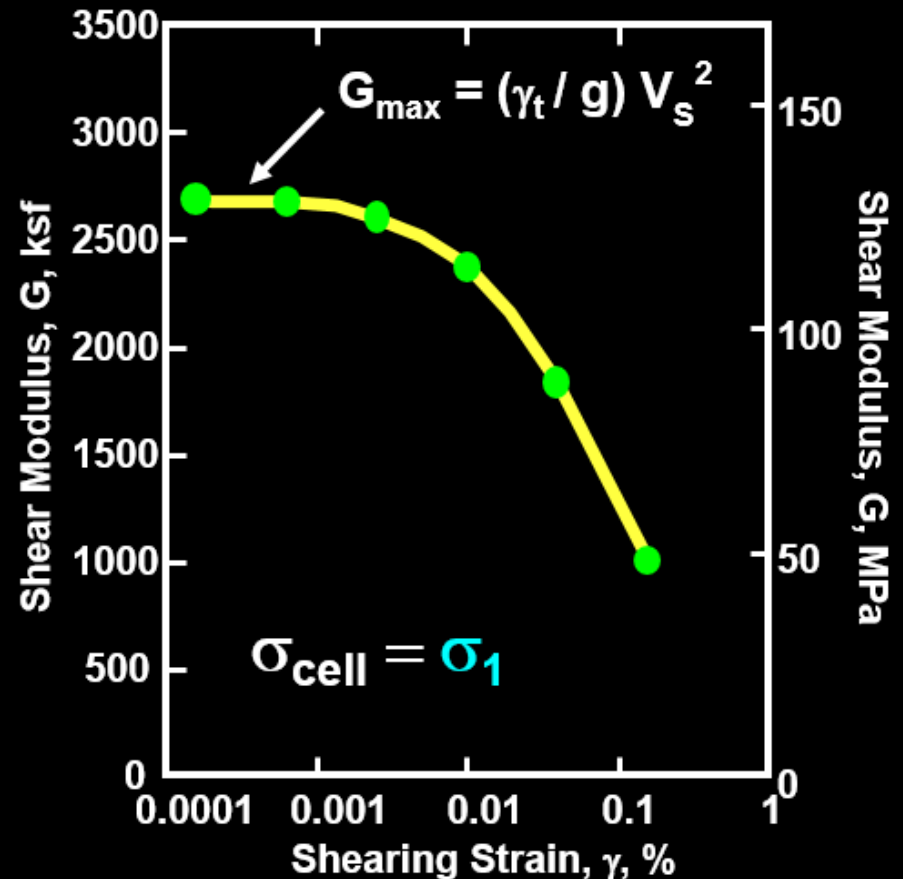


# Laboratory Parametric Studies

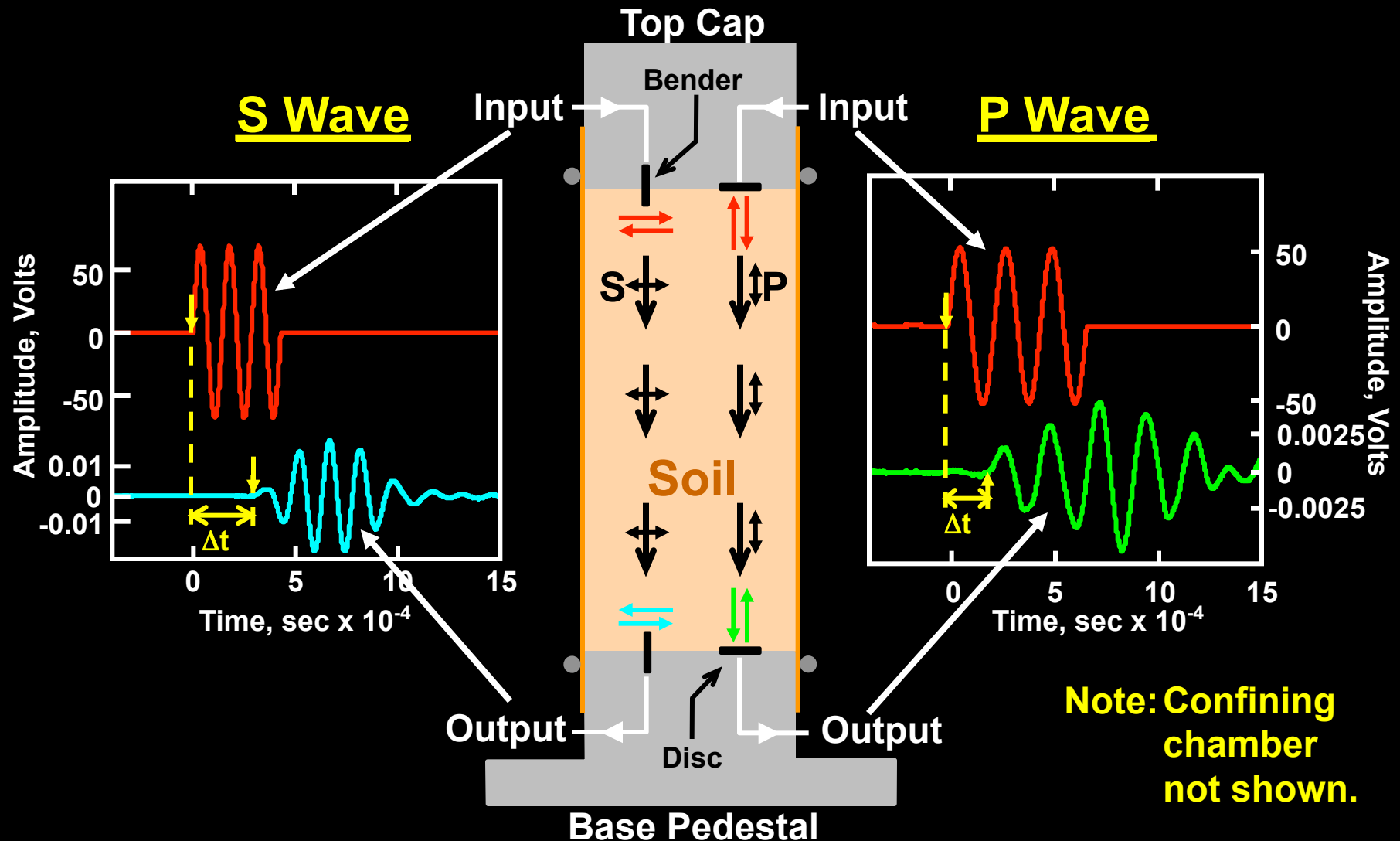
a.  $\log V_s - \log \sigma_o$



b.  $G - \log \gamma$



# Small-Strain $V_p$ and $V_s$ Measurements: Piezoelectric Transducers



## 2. Examples: Applications and Case Histories

- static loading conditions
- dynamic loading conditions

# Static Loading Conditions

## 2.1 Site Characterization

- layering, ground water table, etc.
- underground structures
- tunnel investigations \*
- dams, levees, etc. \*
- SMW landfills

## 2.2 Process Monitoring

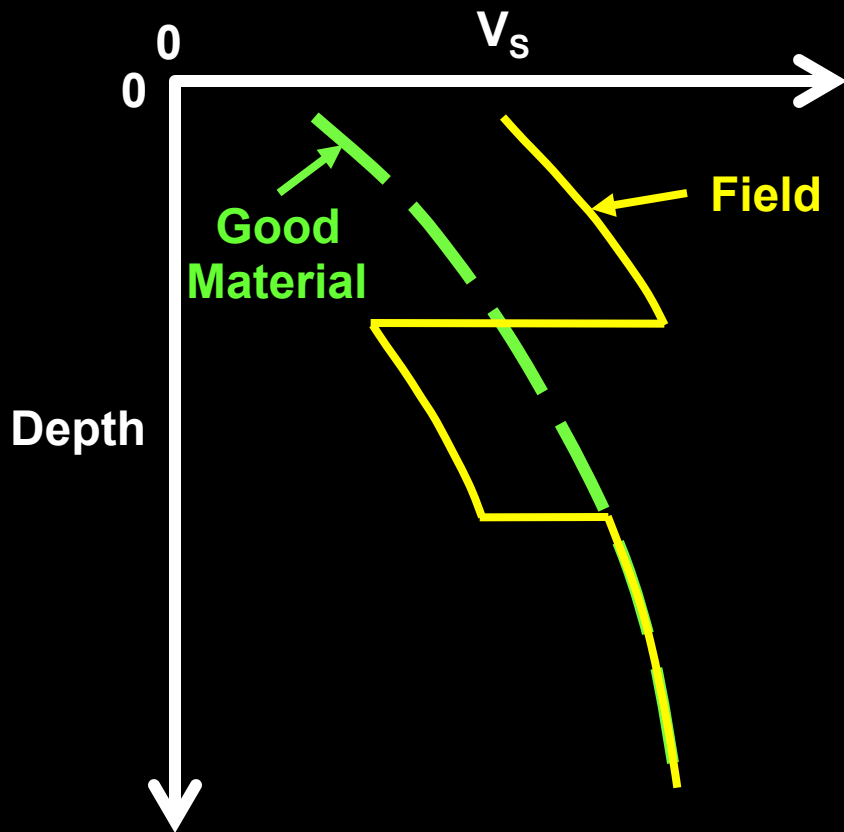
- grouting evaluations
- ground improvement studies \*
- areas of deterioration
- sample disturbance

## 2.3 Movements under Static Loads

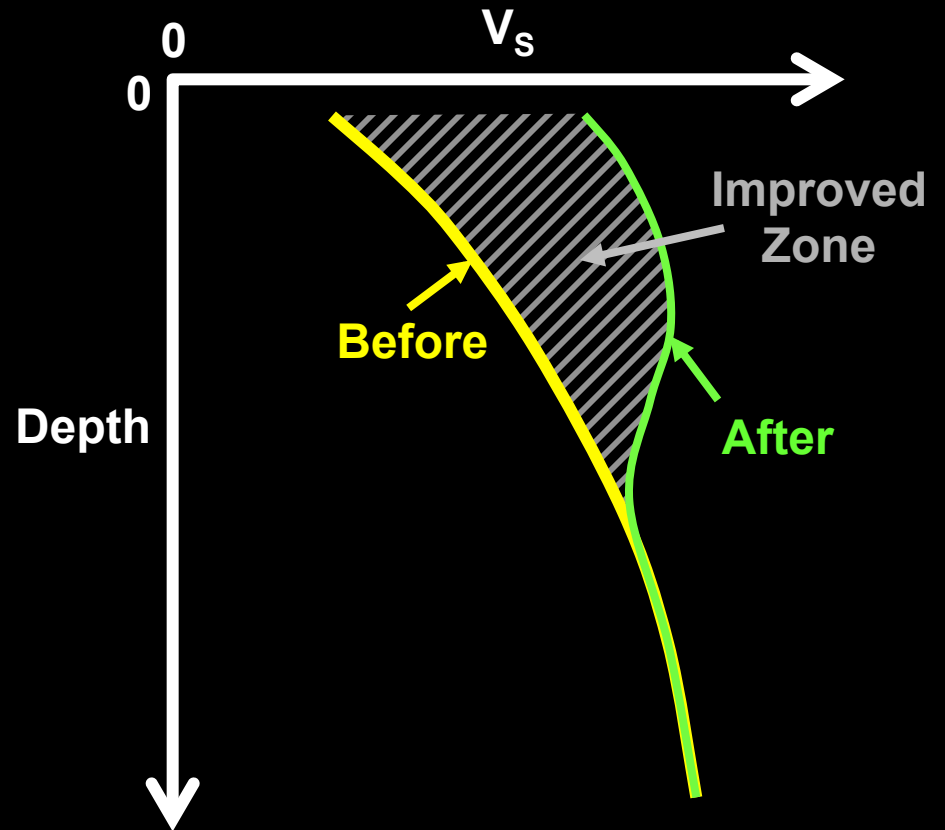
- footing settlements \*
- retaining wall movements

# General Approach

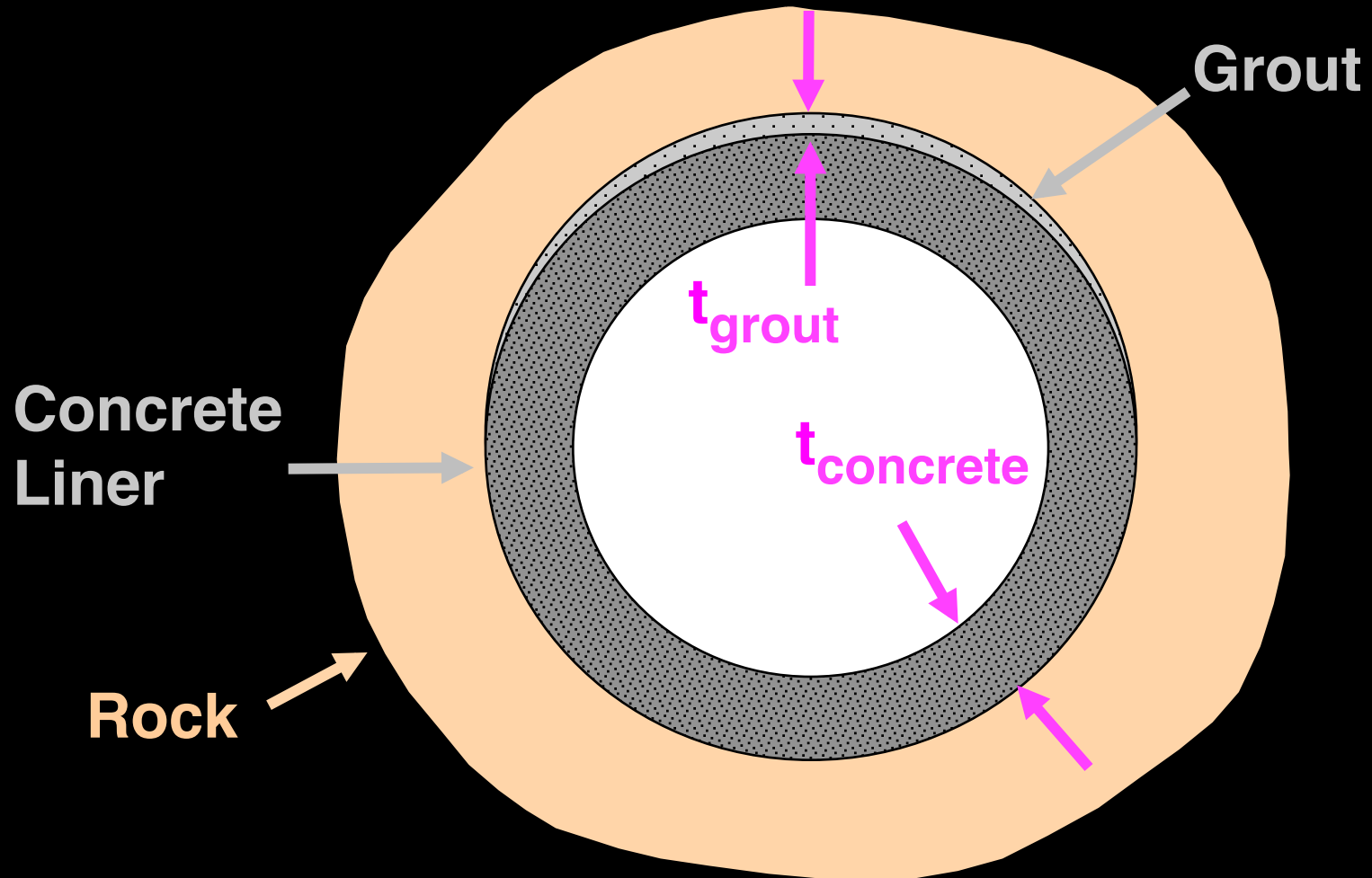
## Estimate Material Quality



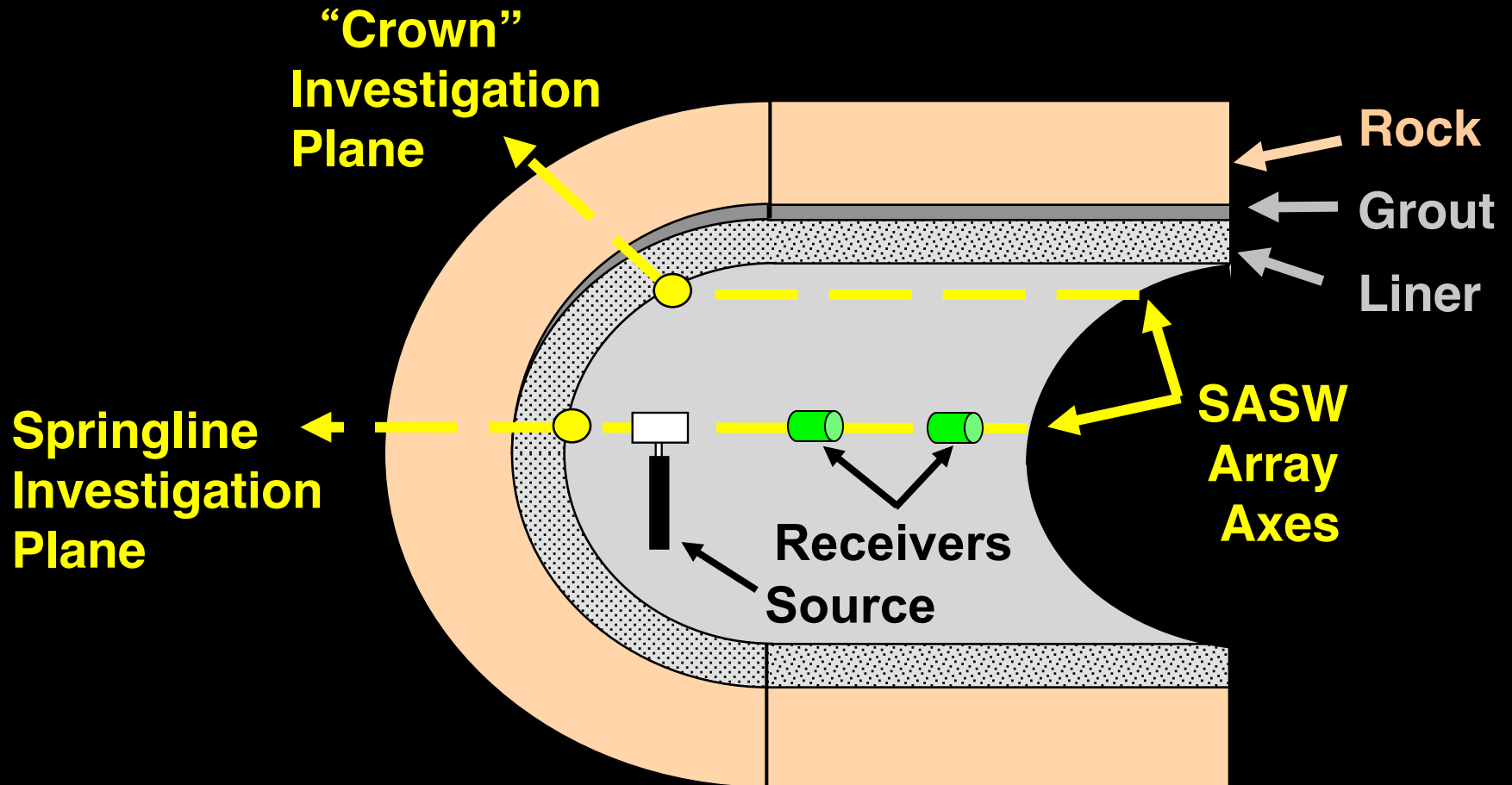
## Evaluate Changed Condition



## 2.1a Site Characterization: Tunnel Investigation

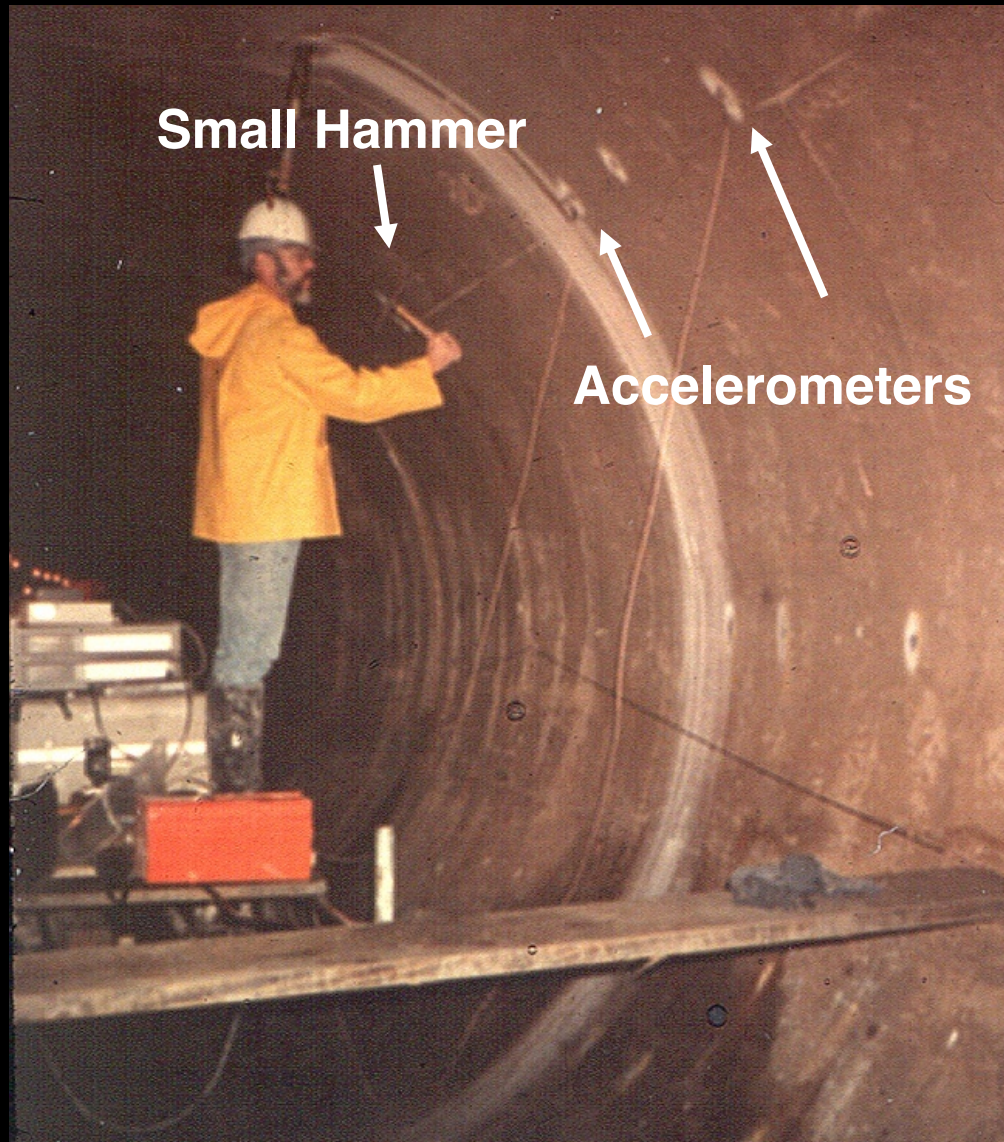


# SASW Testing Arrangement and Planes of Investigation

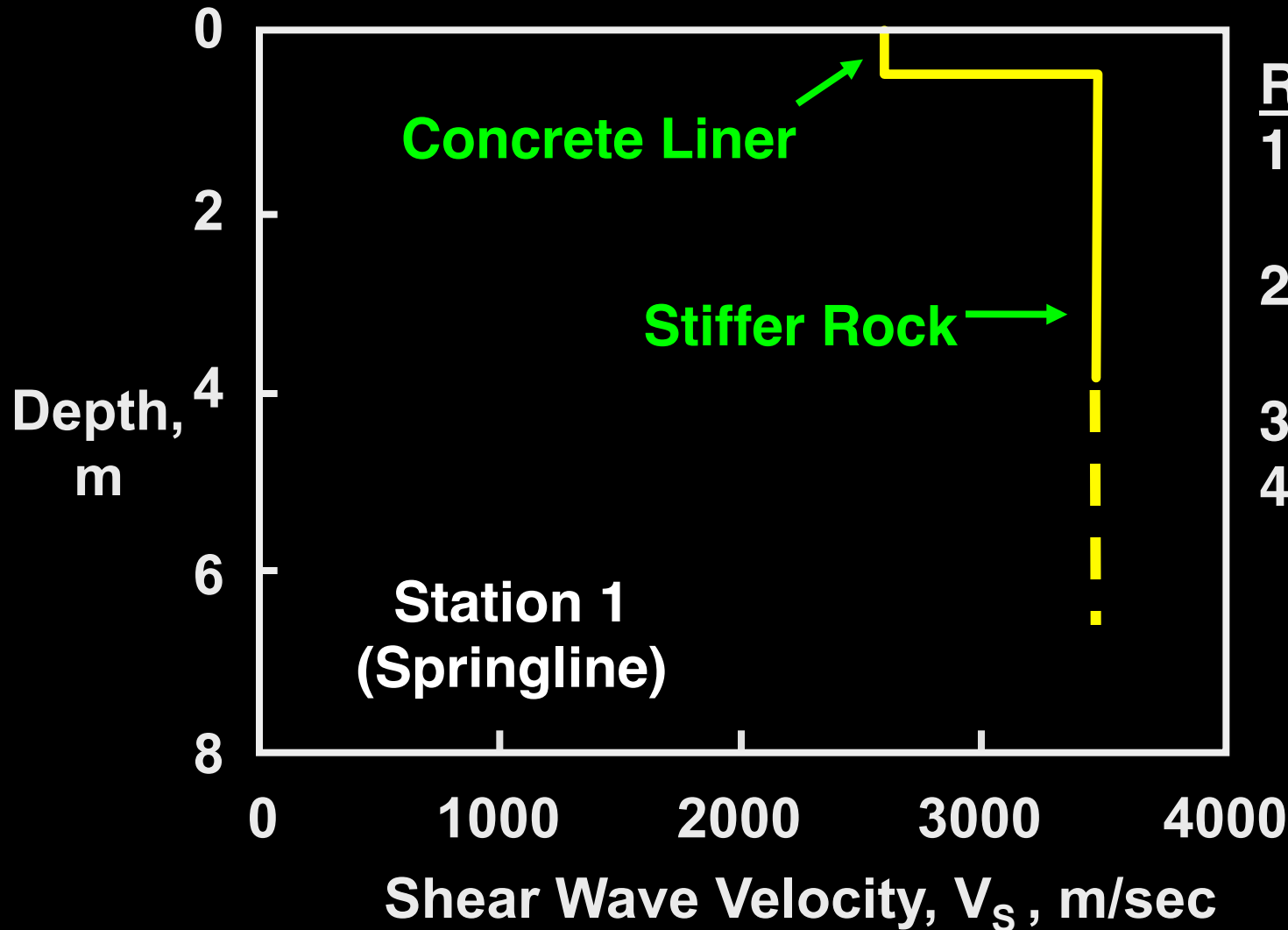




# Conducting SASW Tests



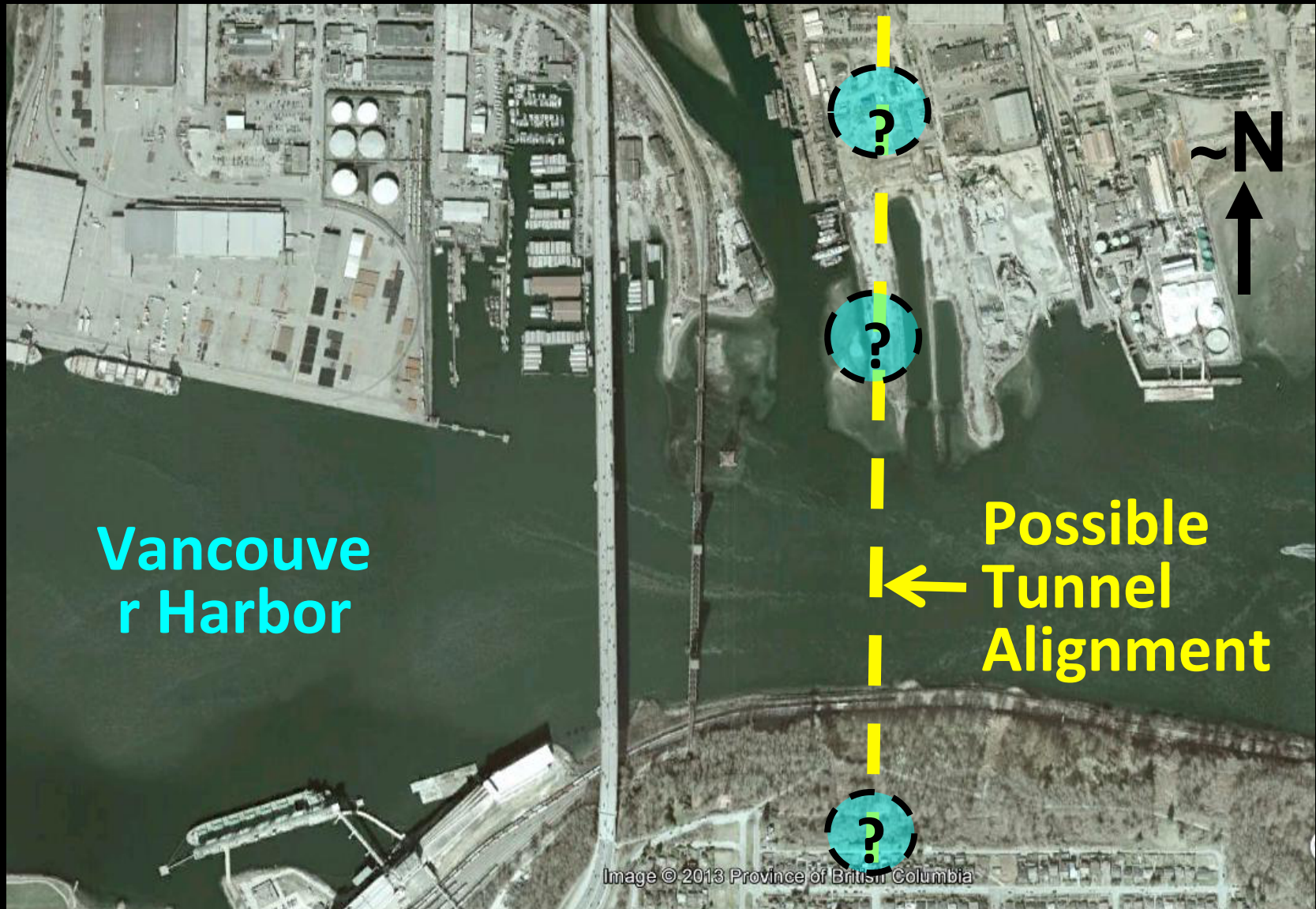
# Interpreted $V_s$ Profile Behind Tunnel Wall at Springline



## Results:

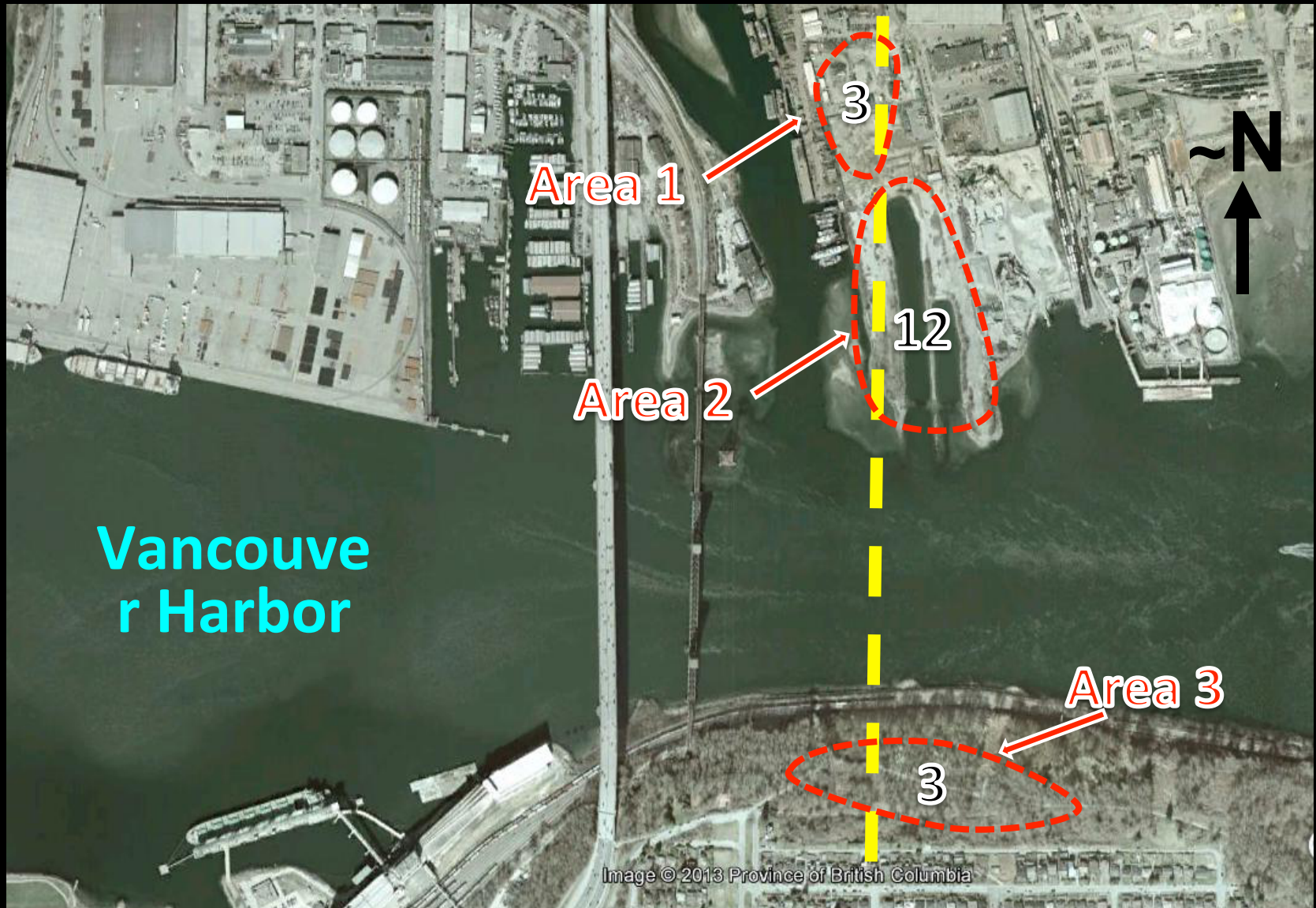
1. high-quality concrete
2. thickness: ~ 0.3 m
3. no voids
4. rock stiffer than liner

## 2.1b Site Characterization: **Proposed Locations of Water Tunnel Shafts**

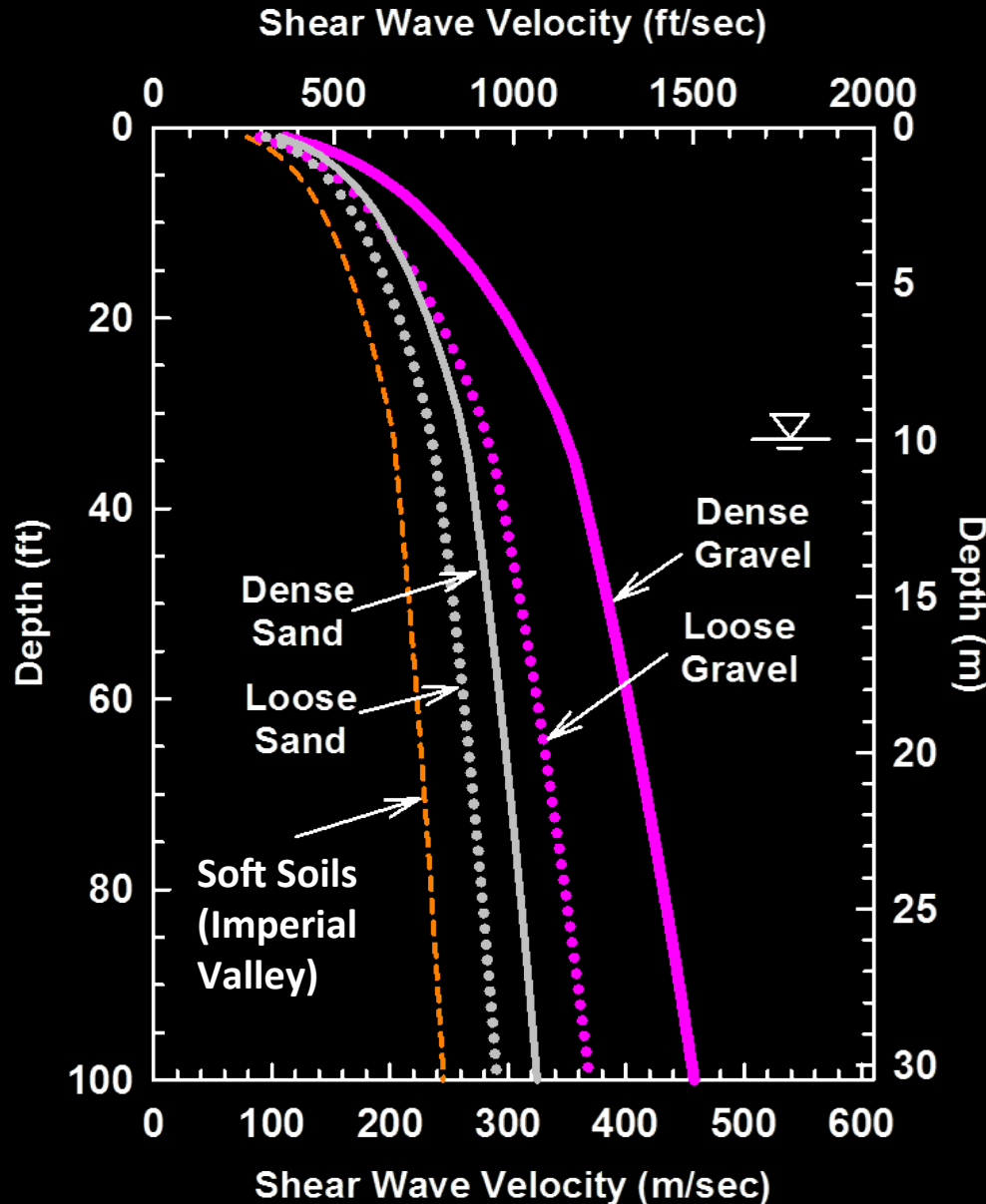




# SASW Testing Locations



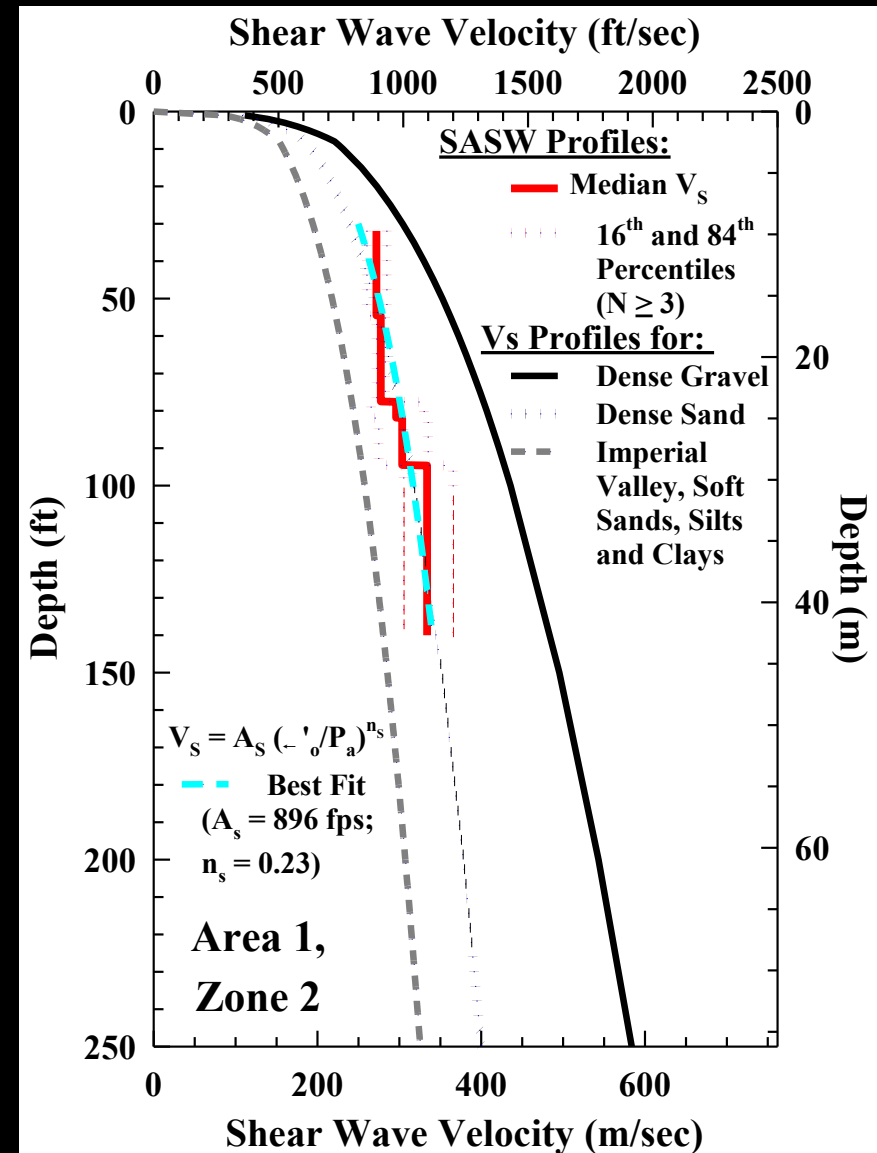
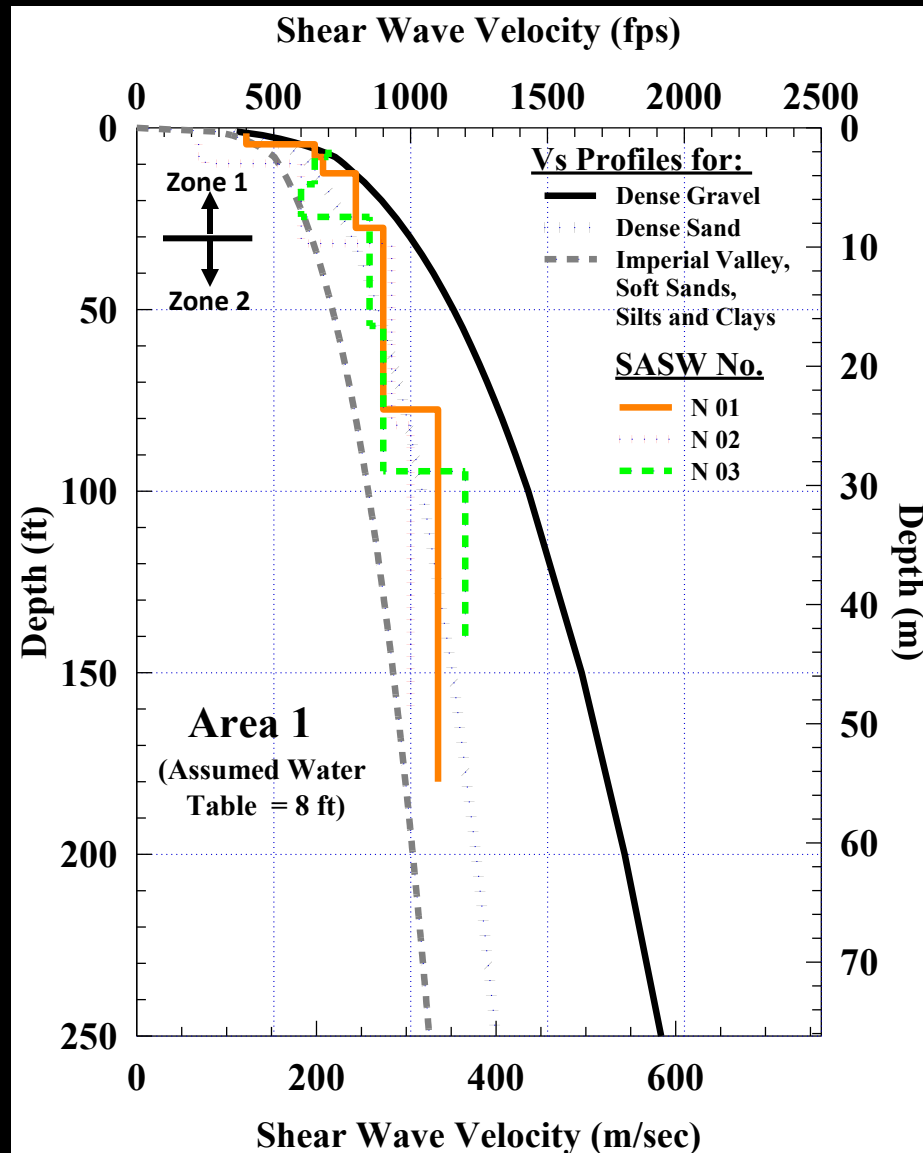
# $V_s$ Template



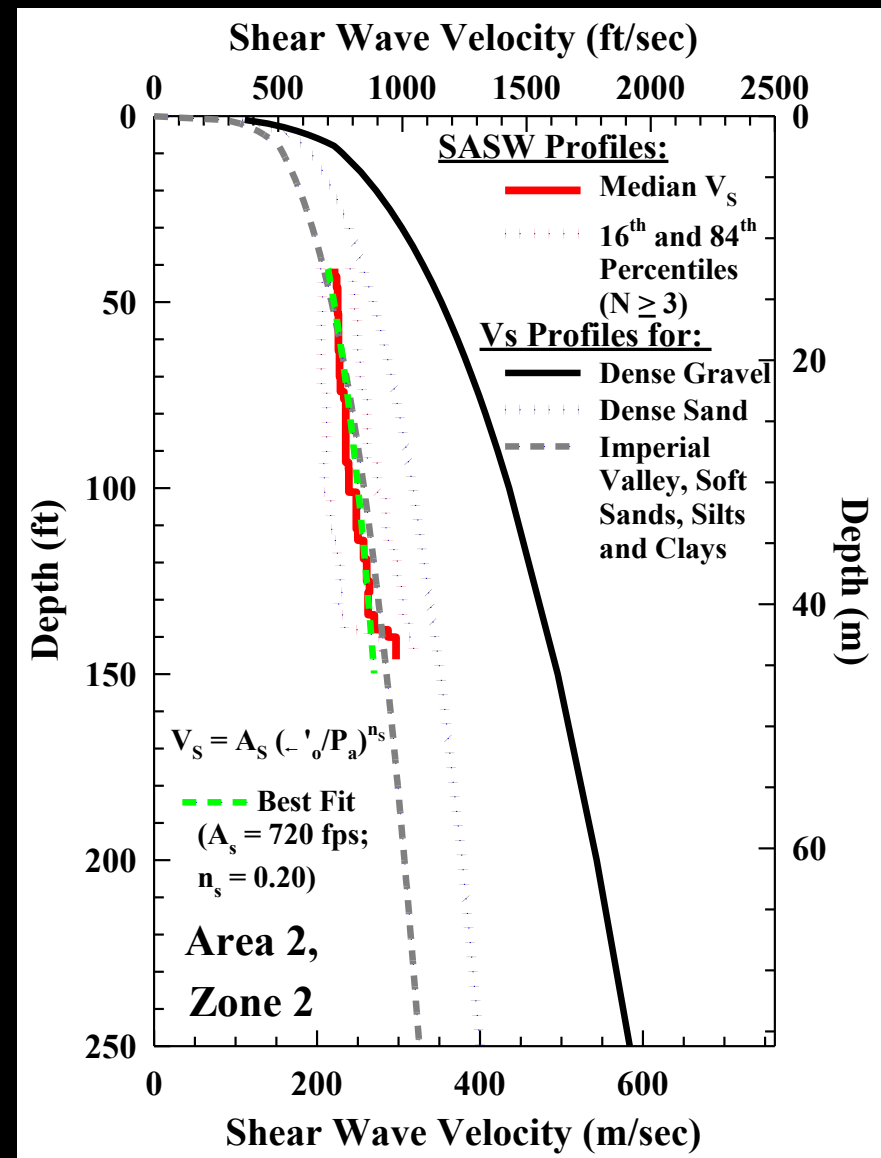
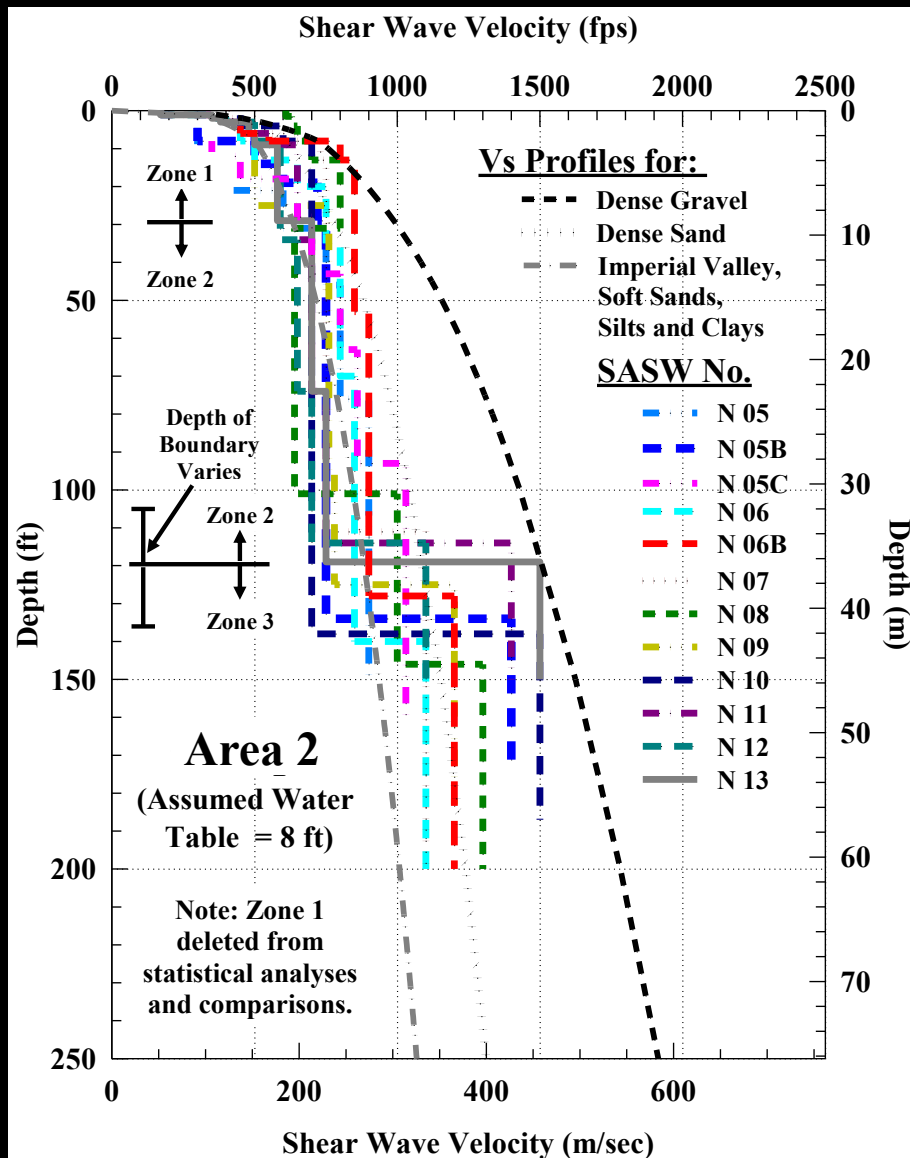
$$V_s = A_s (\sigma_o' / P_a)^{n_s}$$

- $A_s = V_s$  at  $\sigma_o' = 1 \text{ atm}$
- $K_o$  assumed equal to 0.5

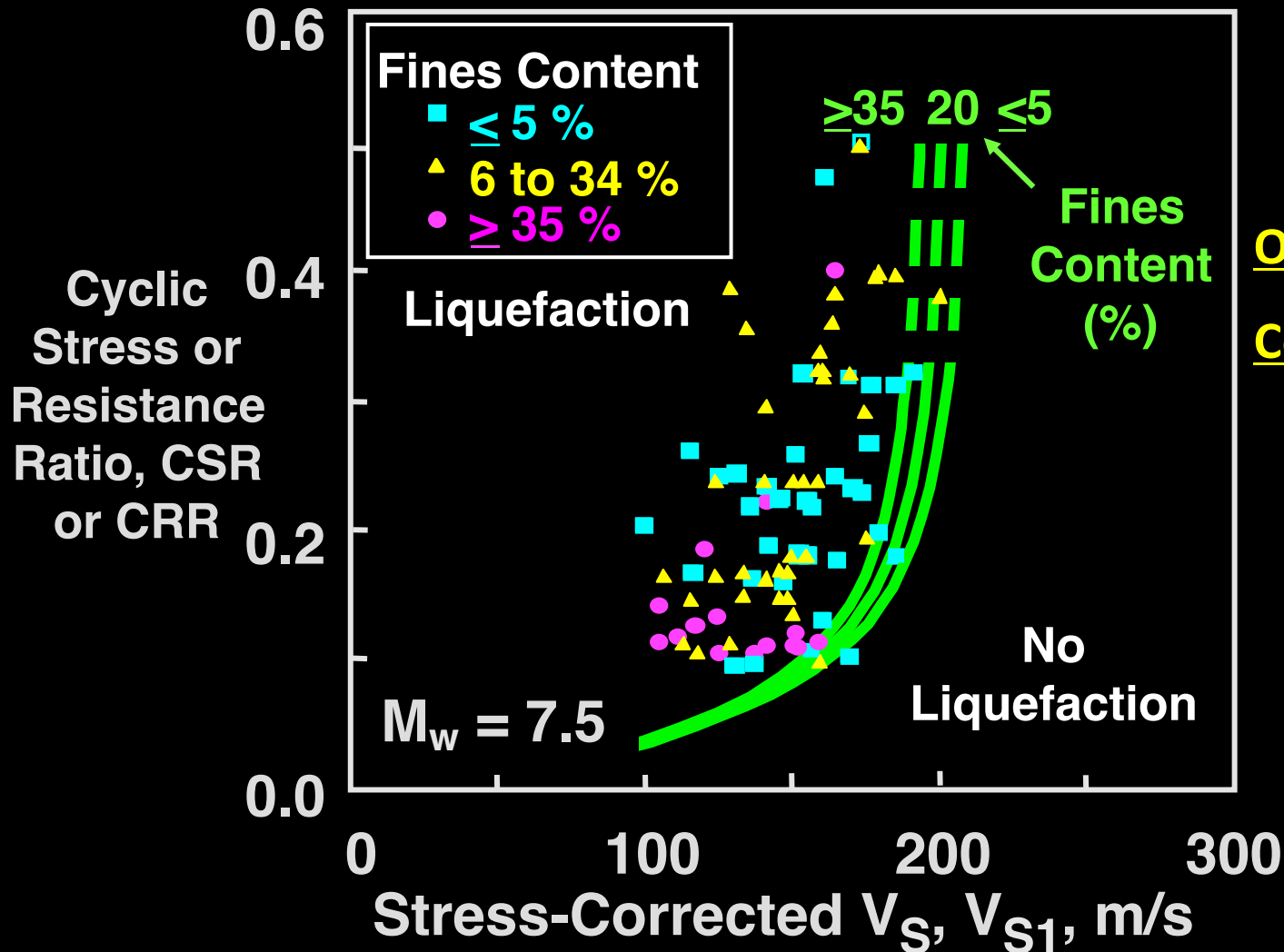
# $V_s$ Profiles in Area 1: Relative Character and Variability of Granular Materials?



# V<sub>s</sub> Profiles in Area 2: Relative Character and Variability of Granular Materials?



# Liquefaction Resistance from $V_s$ (Andrus and Stokoe, 2000)



Overburden-Stress

Correction for  $V_s$ :

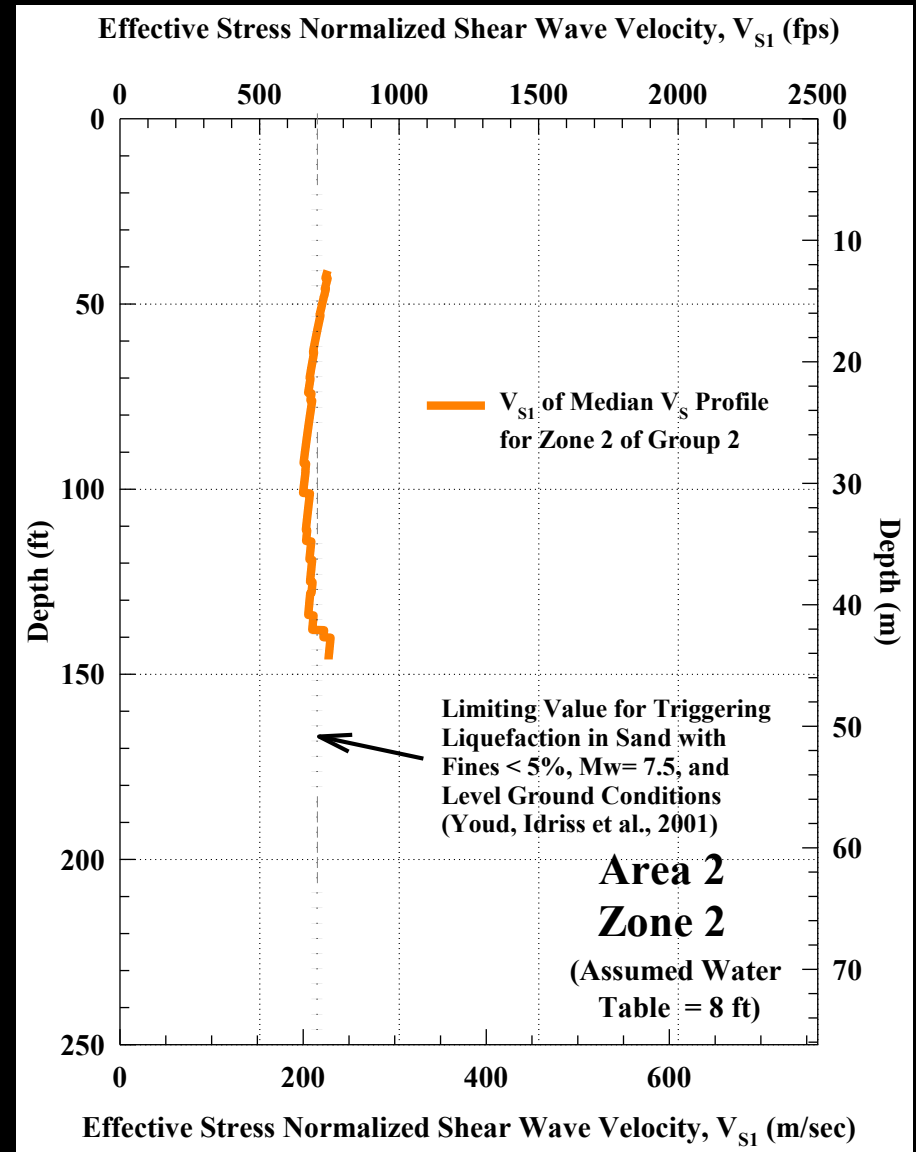
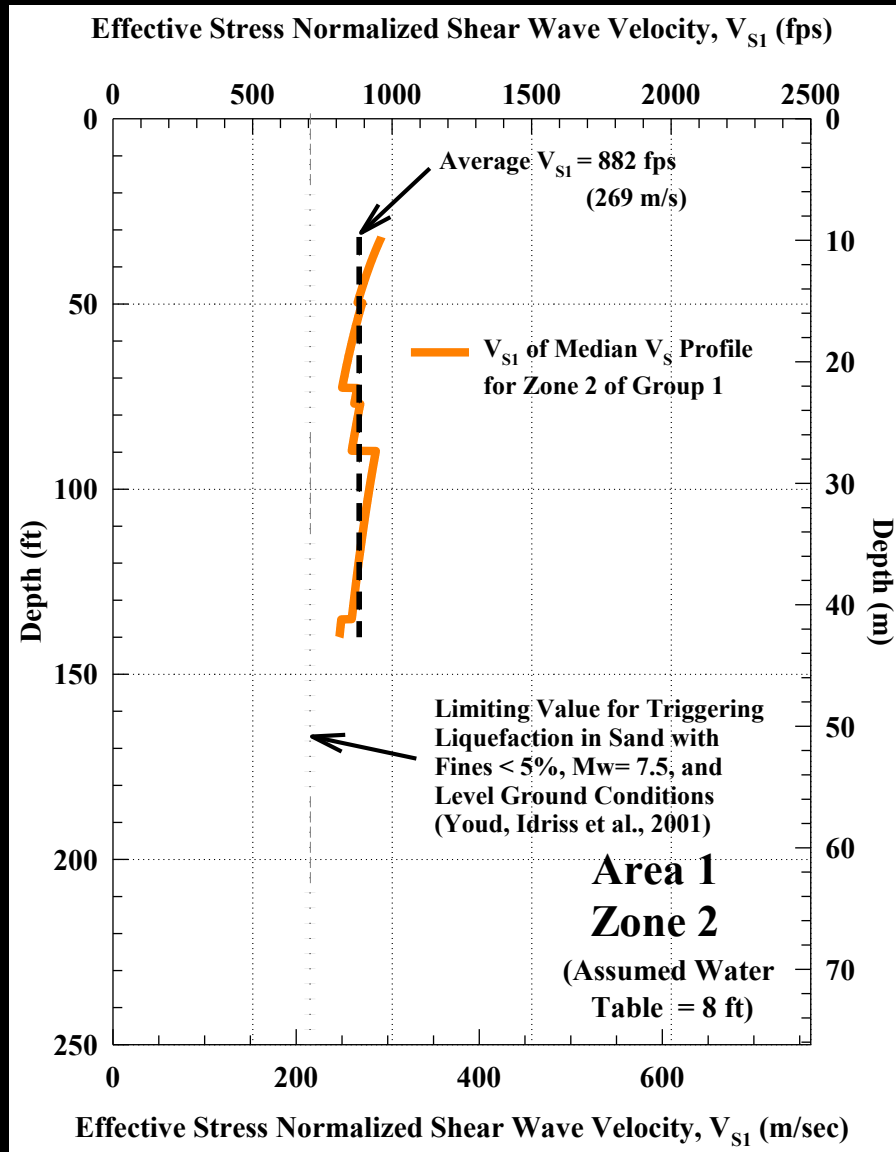
$$V_{s1} = V_s (P_a / \sigma'_{vo})^{0.25}$$

$$P_a = 100 \text{ kPa}$$

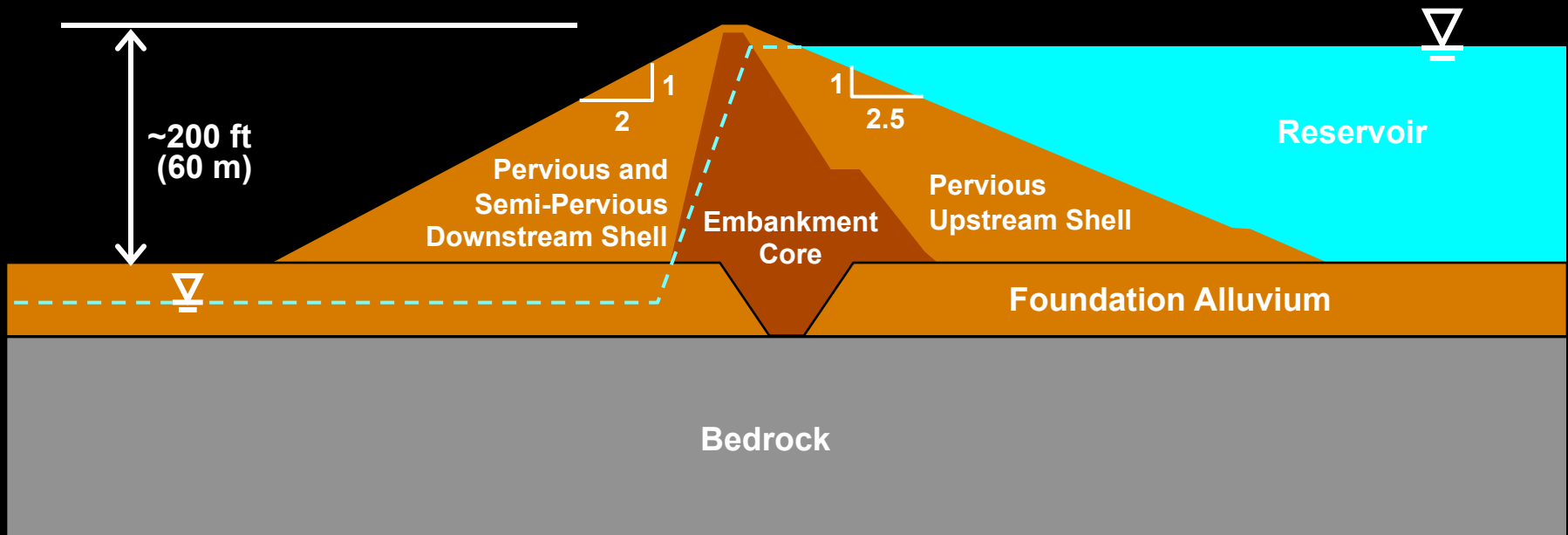
$$\sigma'_{vo} = \text{depth} * \gamma_t$$



# Likelihood of Liquefaction Triggering



## 2.1c Dam Investigation: “Quality” of Alluvium Within and Beneath an Embankment Dam

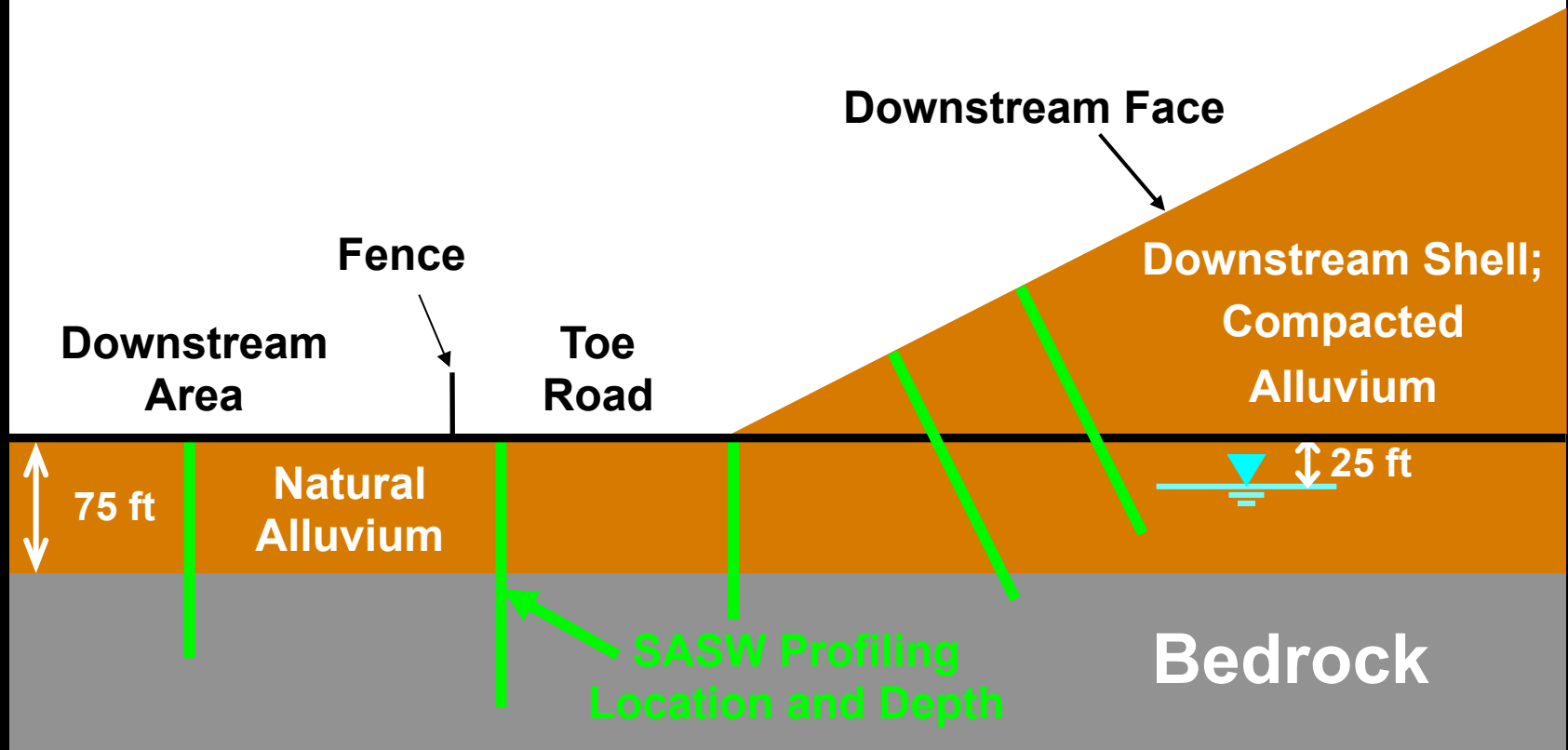


# Approximate SASW Testing Locations



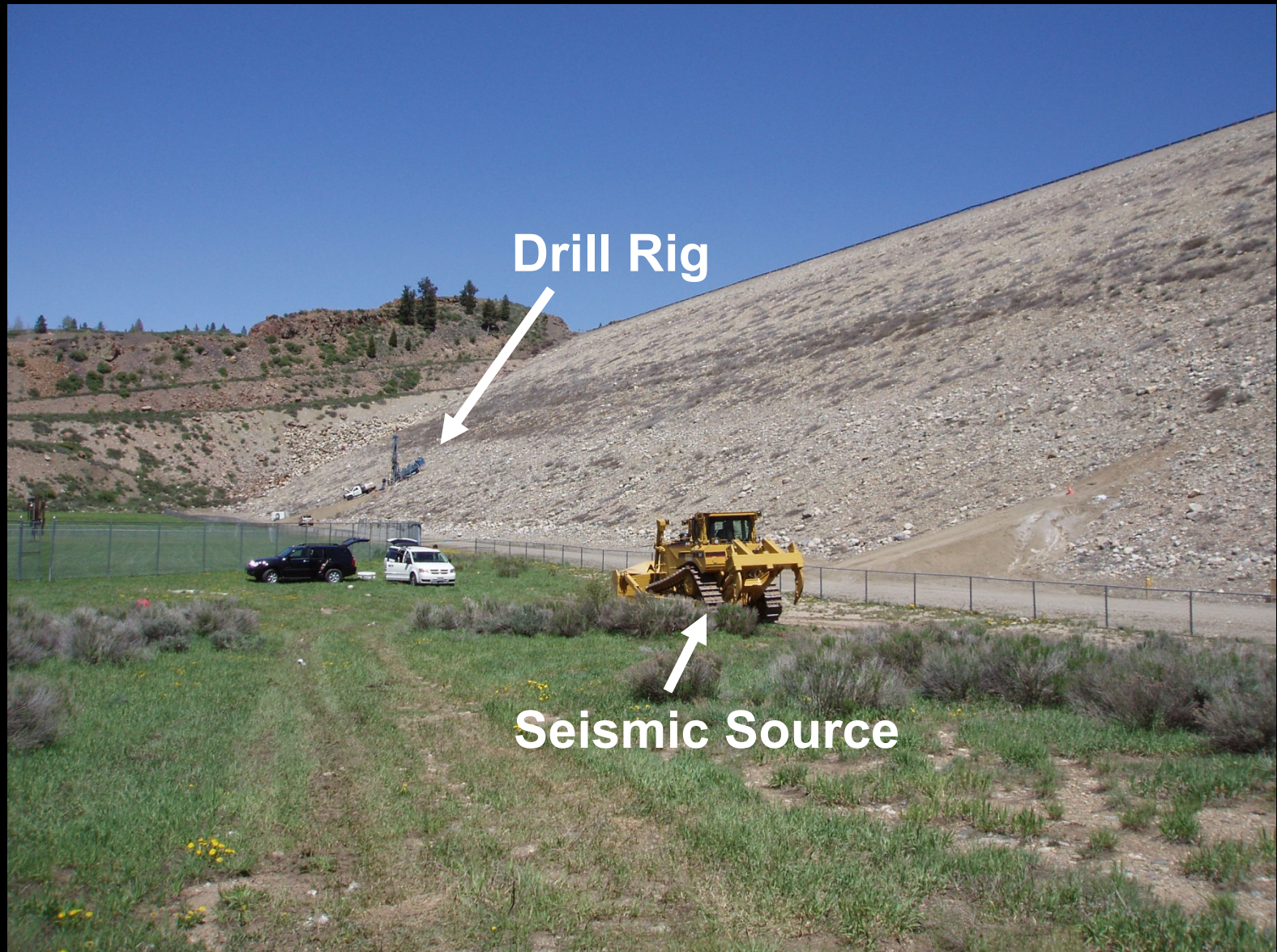
# SASW Test Locations - Downstream Face and Downstream Area

**Note: All Testing Arrays Parallel to Crest**

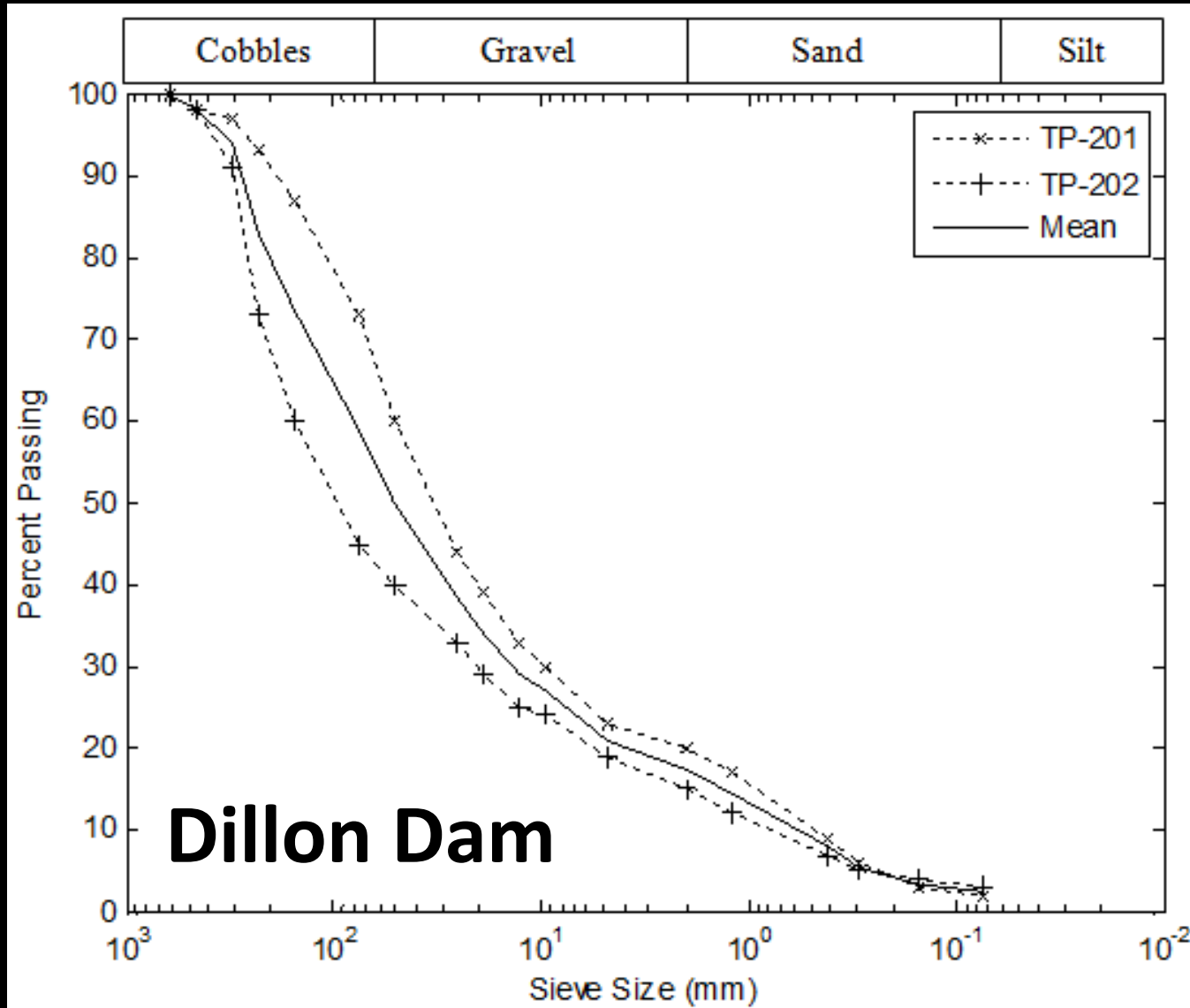




# Dillon Dam Site



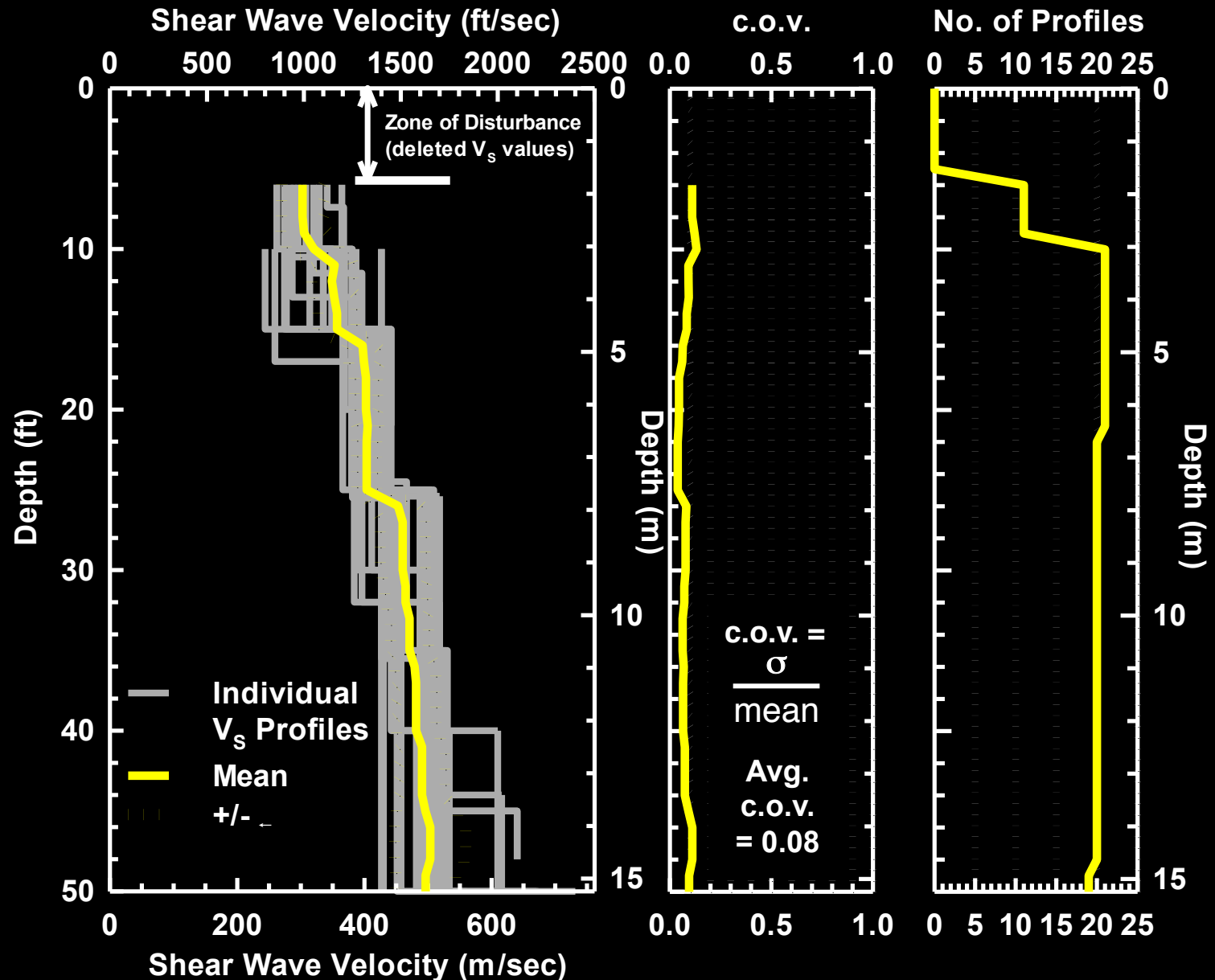
# Gradation Curves from Field Samples of Foundation Alluvium



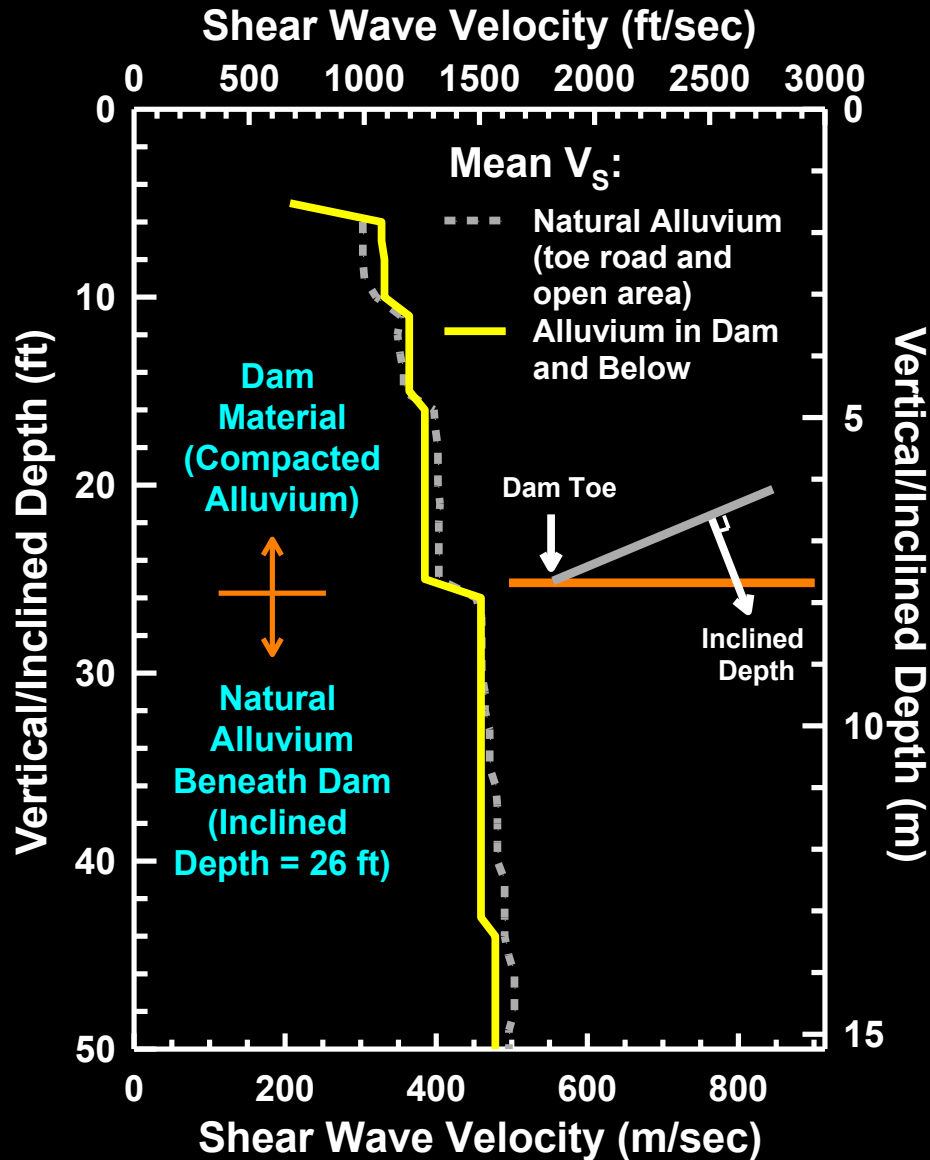
$D_{50} \sim 50 \text{ mm}$   
 $C_u \sim 130$   
 $PI = 0$

**Dillon Dam**

# Statistical Analysis of Natural Alluvium



# Comparison of Mean $V_s$ Profiles - Natural Alluvium and Compacted Alluvium

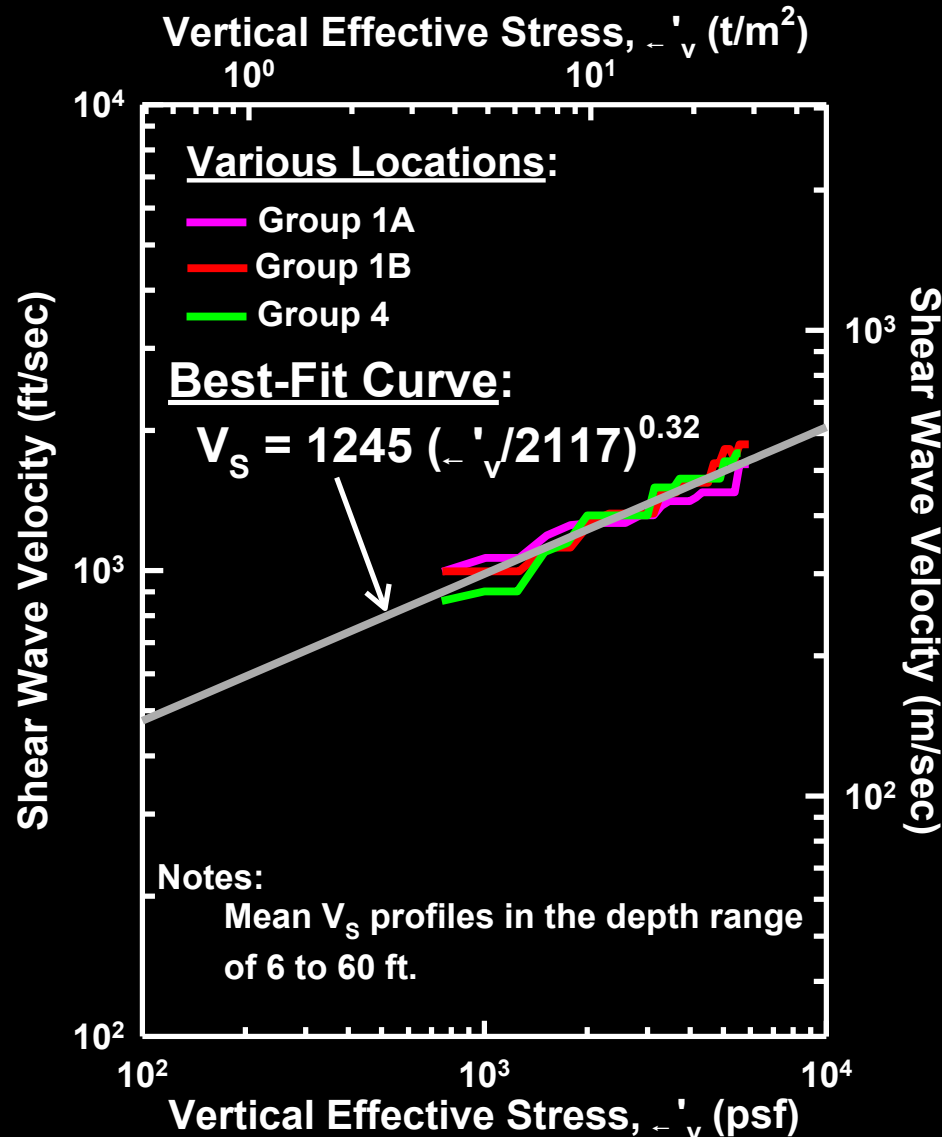


## Results:

1. Natural alluvium is stiff ( $V_s \geq 300$  m/s); hence, dense.
2. Compacted alluvium in dam is similar to natural alluvium so:
  - (a) dense and
  - (b) not cemented.
3. No loose zone of alluvium under toe of dam.
4. Average c.o.v.  $< 0.1$



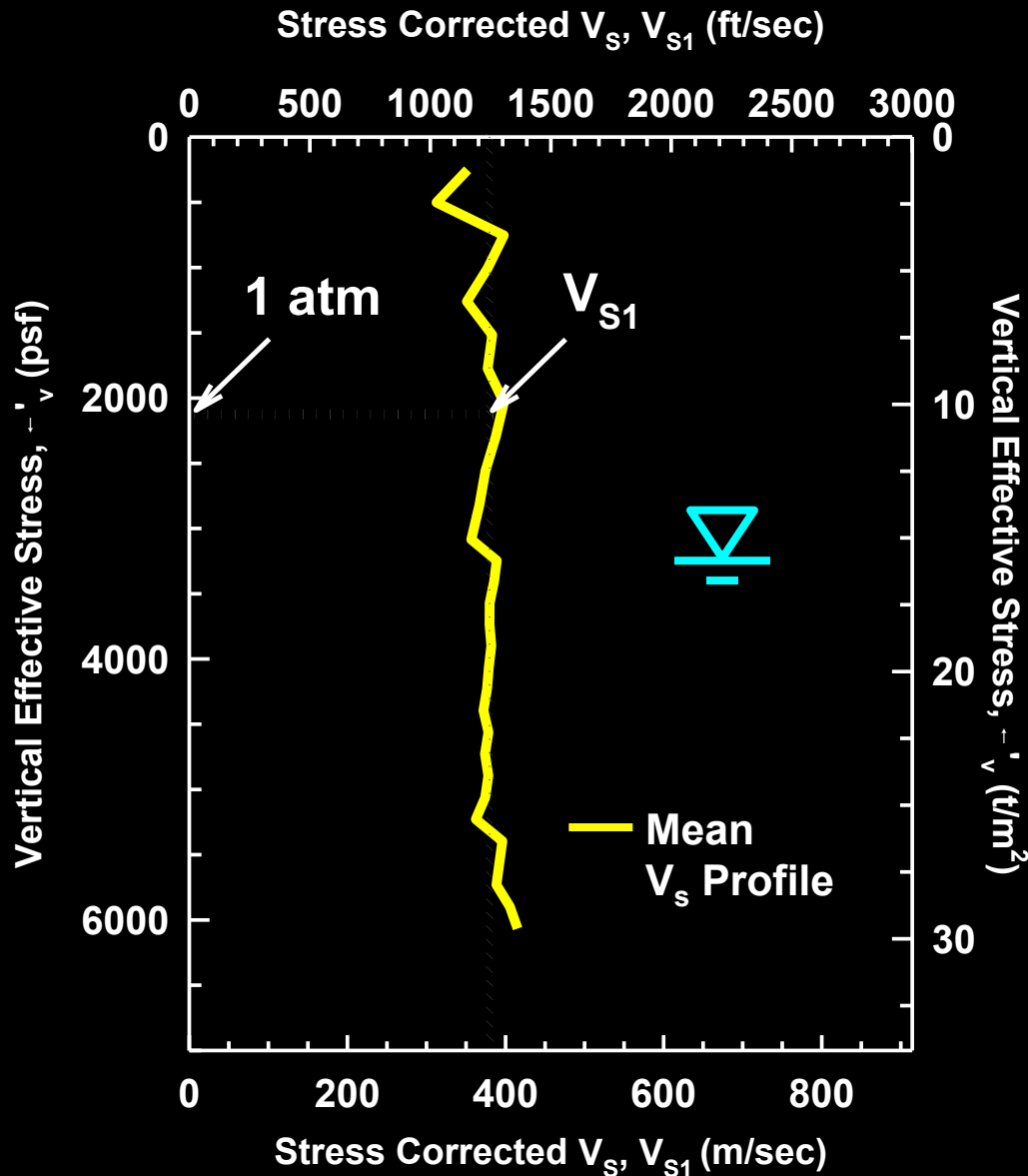
# Best-Fit Curve for the Field $\log V_s - \log \sigma'_v$ Relationship of the Natural Alluvium



## Results:

- $n_s = 0.32$  is reasonable for uncemented gravelly soils.
- $V_s$  at depth  $\sim 1$  ft (0.3 m) equals 527 fps (161 m/s) which represents material with:
  - large  $D_{50}$  ( $> 25$  mm),
  - large  $C_u$  ( $> 35$ ) and
  - no cementation.
- $\log V_s - \log \sigma'_v$  is representative of a normally consolidated soil (... with no plasticity).

# Calculated $V_{s1}$ Profile for Natural Alluvium Using $n_s = 0.32$



## Overburden-Stress

### Correction for $V_s$ :

$$V_{s1} = V_s (P_a / \sigma'_v)^{0.32}$$

$$P_a = 100 \text{ kPa}$$

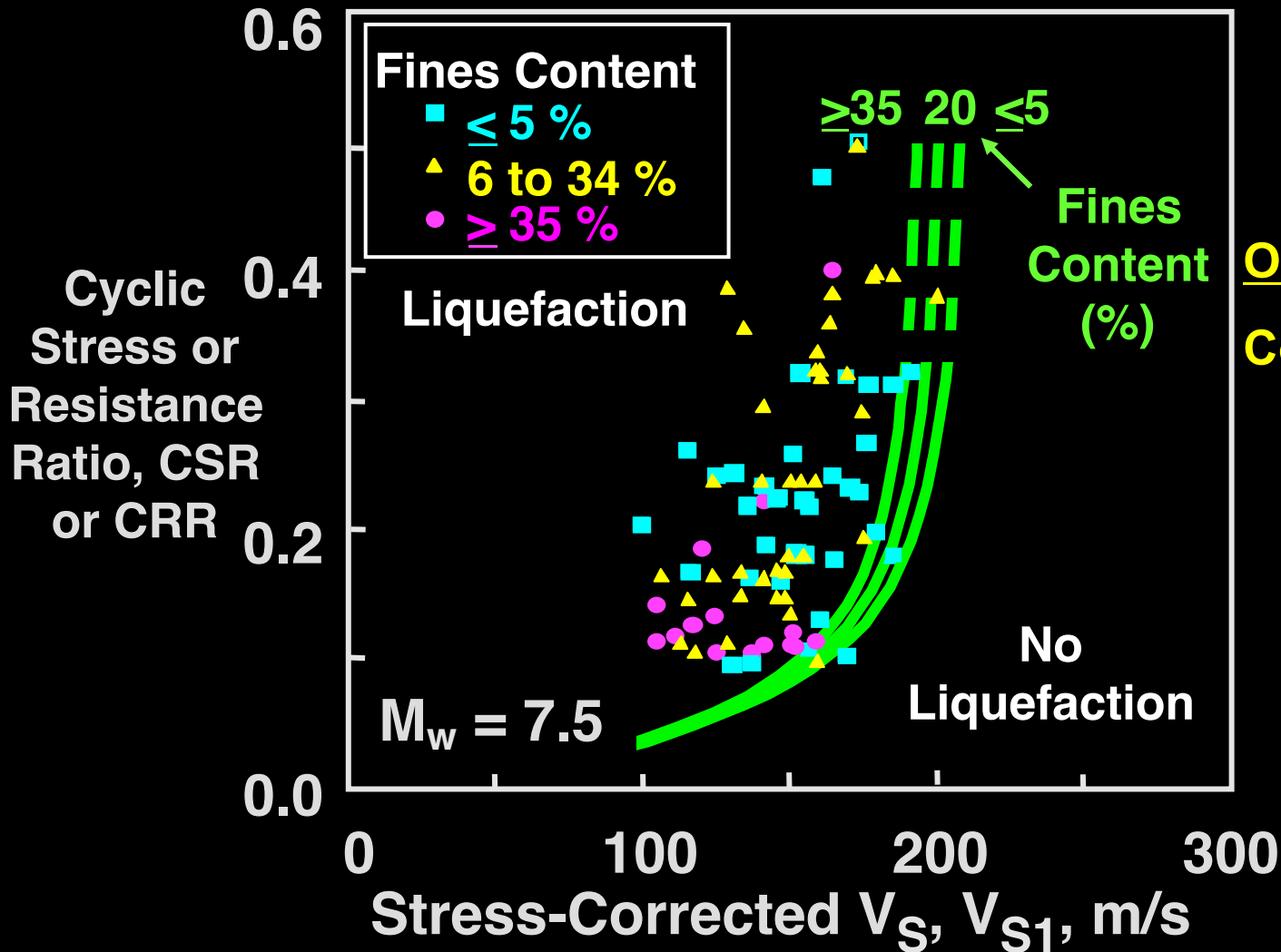
$$\sigma'_v = \text{depth} * \gamma_t$$

### Average $V_{s1}$

Assumed  $\gamma_t \sim 138 \text{ pcf}$

Avg.  $V_{s1} = 1245 \text{ fps}$   
(380 m/s)

# Liquefaction Resistance from $V_s$ (Andrus and Stokoe, 2000)



Overburden-Stress

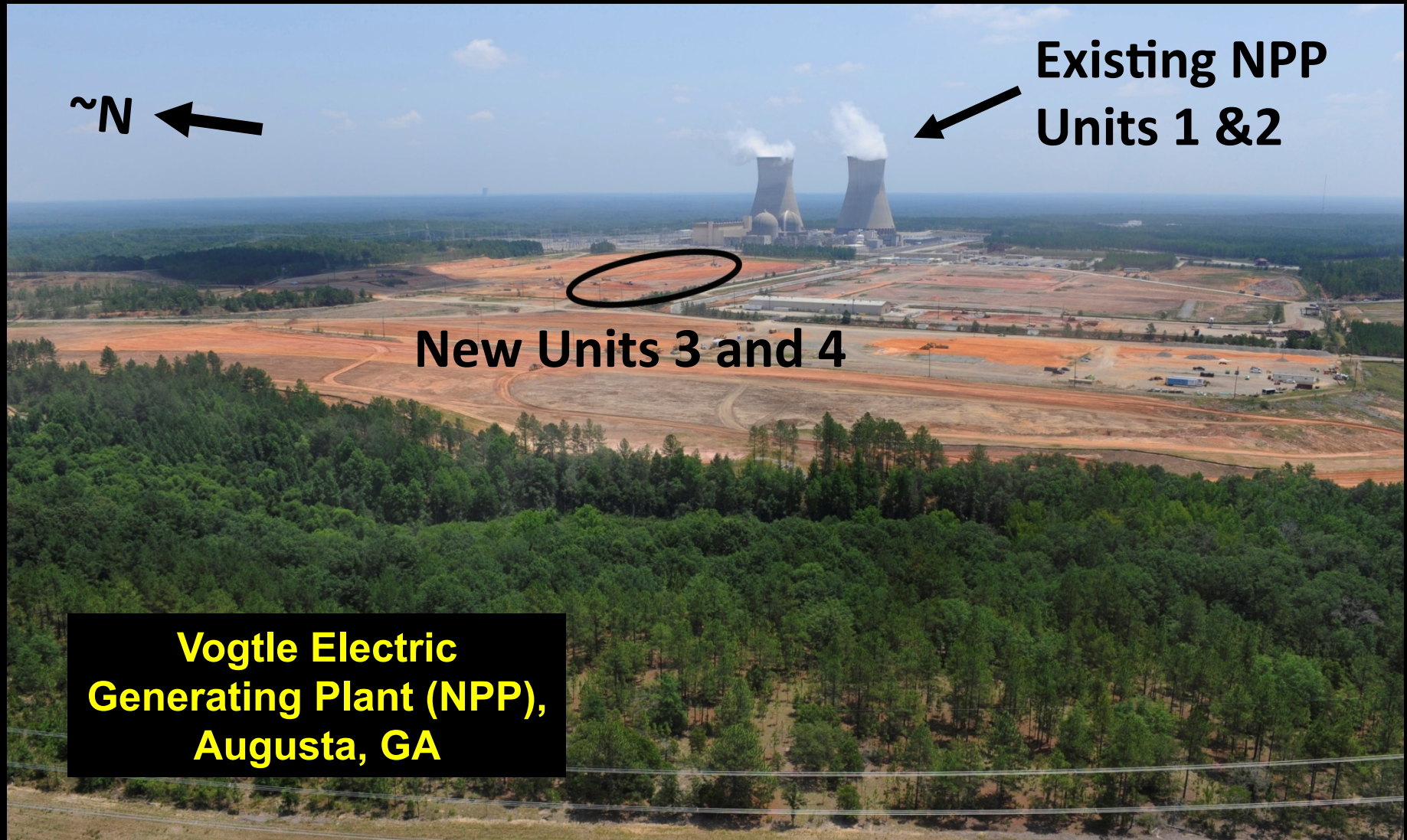
**Correction for  $V_s$ :**

$$V_{s1} = V_s (P_a / \sigma'_{vo})^{0.25}$$

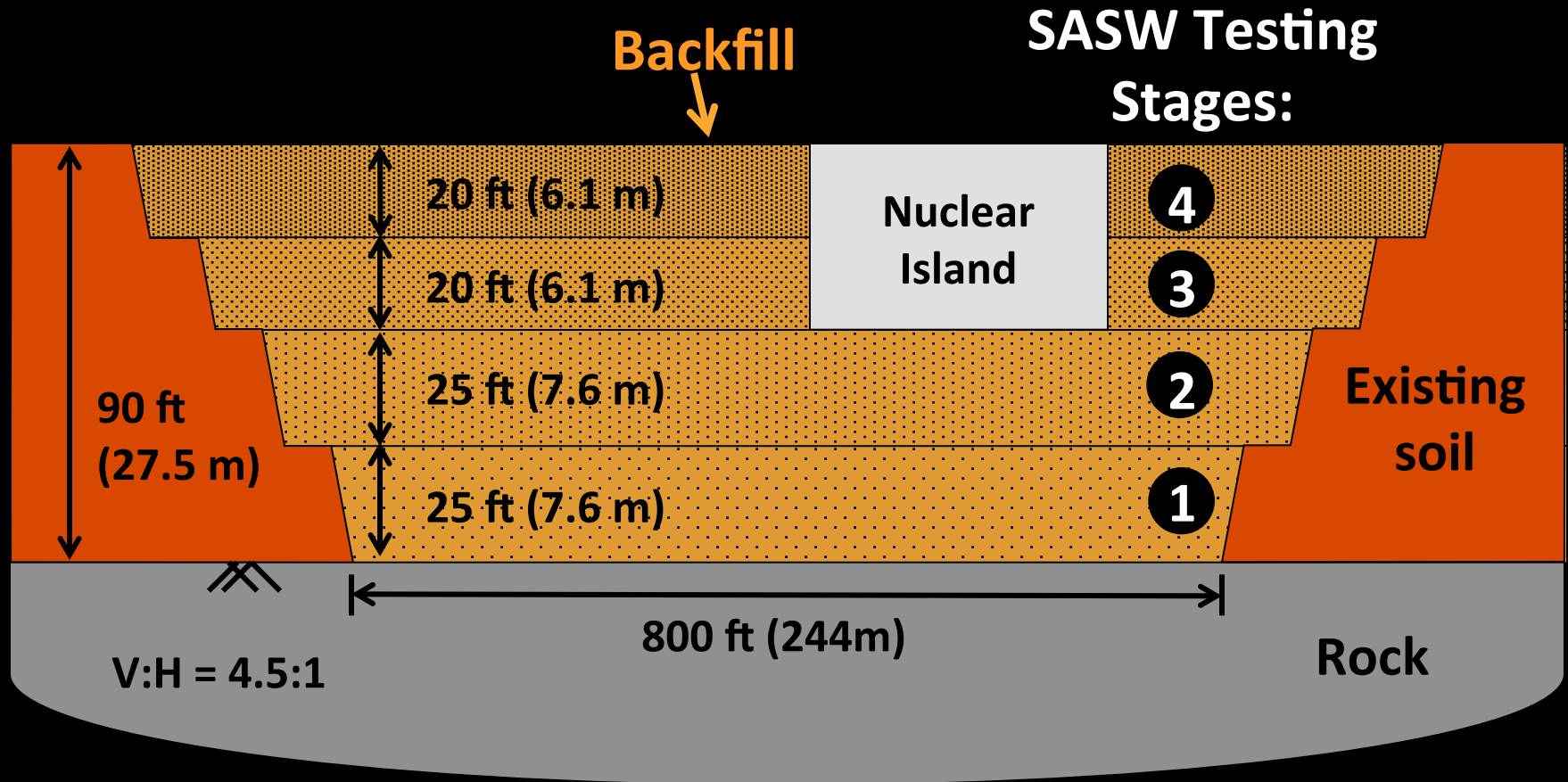
$$P_a = 100 \text{ kPa}$$

$$\sigma'_{vo} = \text{depth} * \gamma_t$$

## 2.2a Process Monitoring: Evaluating Compaction of a Thick Granular Fill



# Cross-Section of Backfill at Units 3 and 4



- Notes:
1. Material in backfill is SP, SP-SM, SM ; nonplastic fines.
  2. Loose lifts of 12 in. (30 cm).
  3. Minimum compaction of 95% modified Proctor (avg. ~ 98%).



# Creating 90-ft (27.5-m) Deep Excavation





# Relative Locations of Units 3 and 4



Plant Vogtle Units 3 and 4 foundation excavation,  
with water vapor rising from cooling towers in background. April, 2010.



# Backfilling Nearly Complete

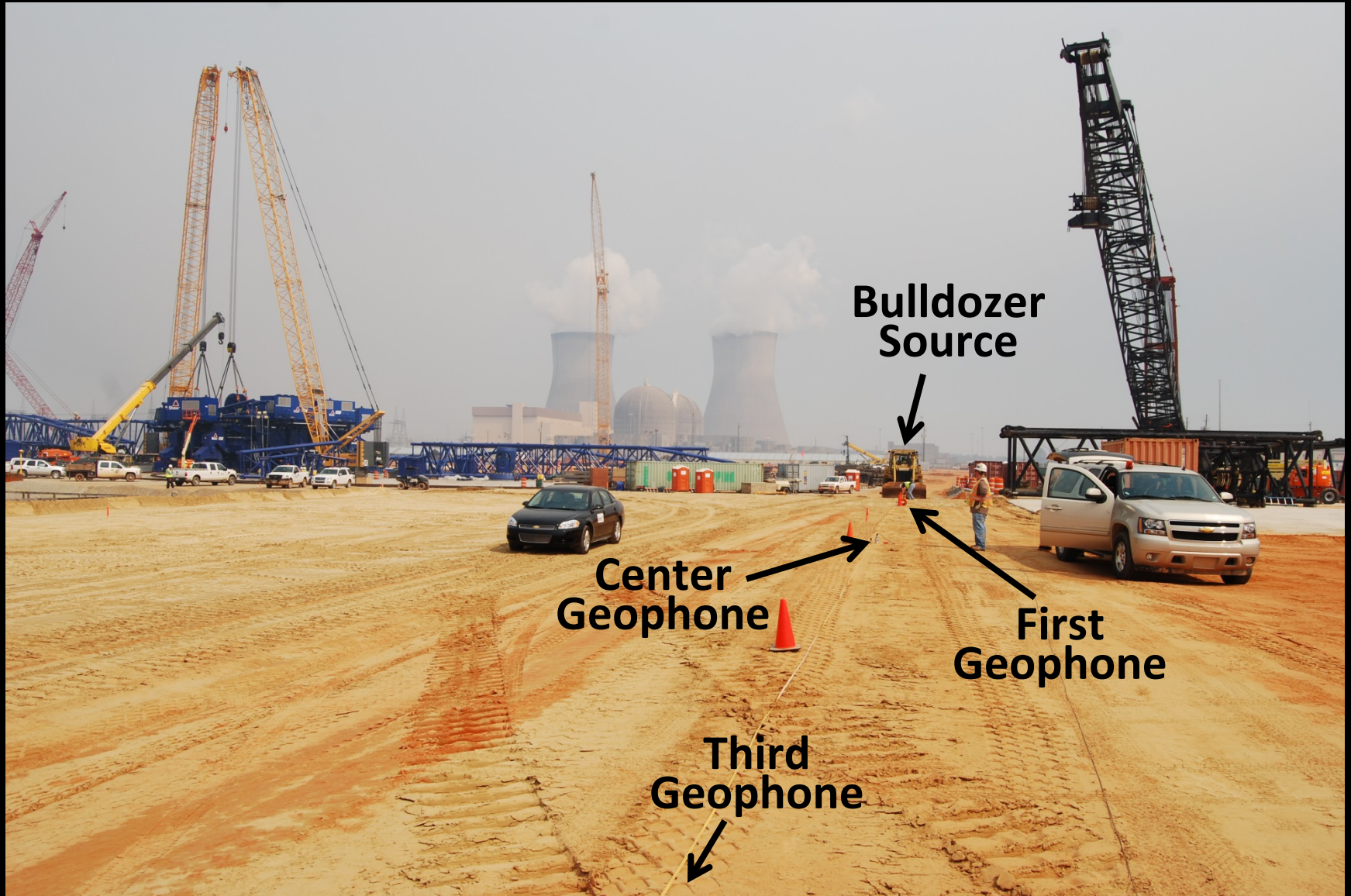


Aerial photograph of Vogtle 3 and 4 construction site. Unit 3 is located at left and top of photo and Unit 4 to the right and bottom. Heavy lift derrick crane foundation in center.  
August 11, 2011

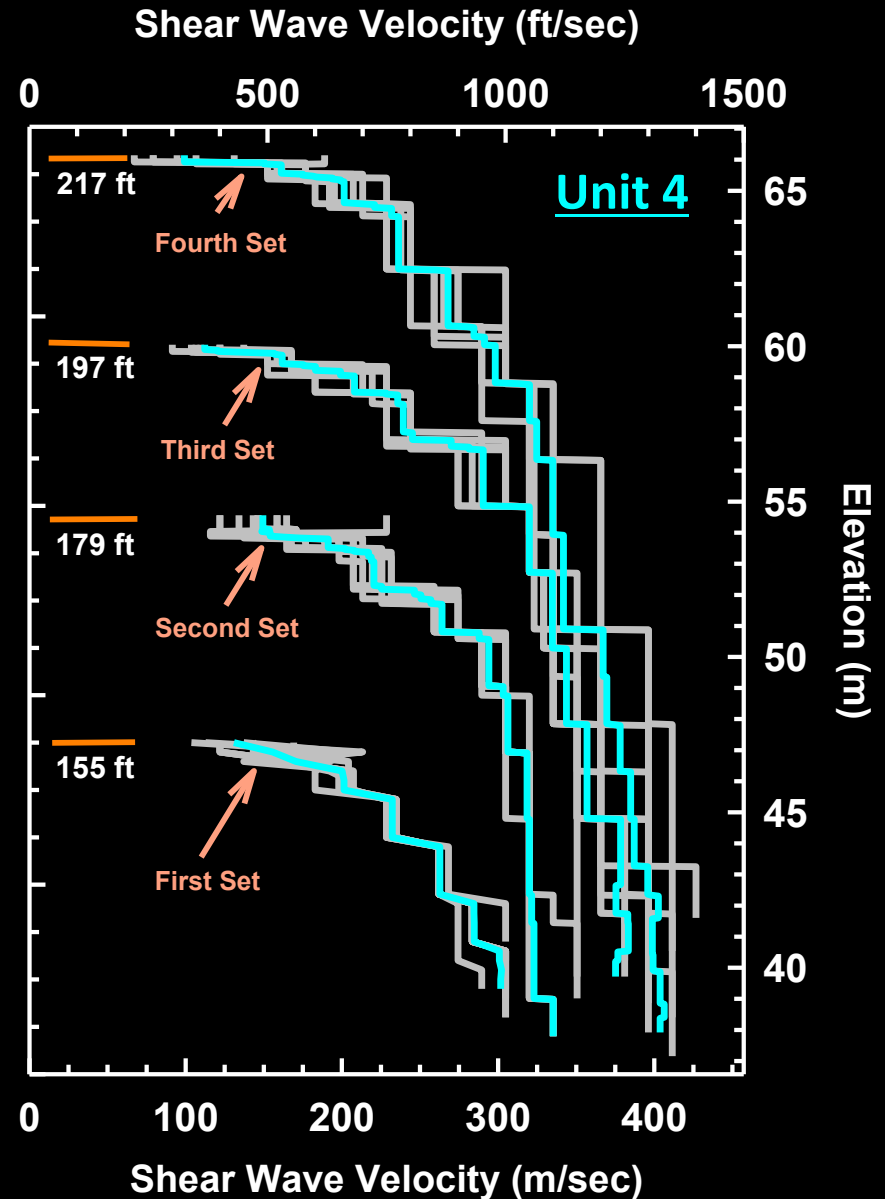
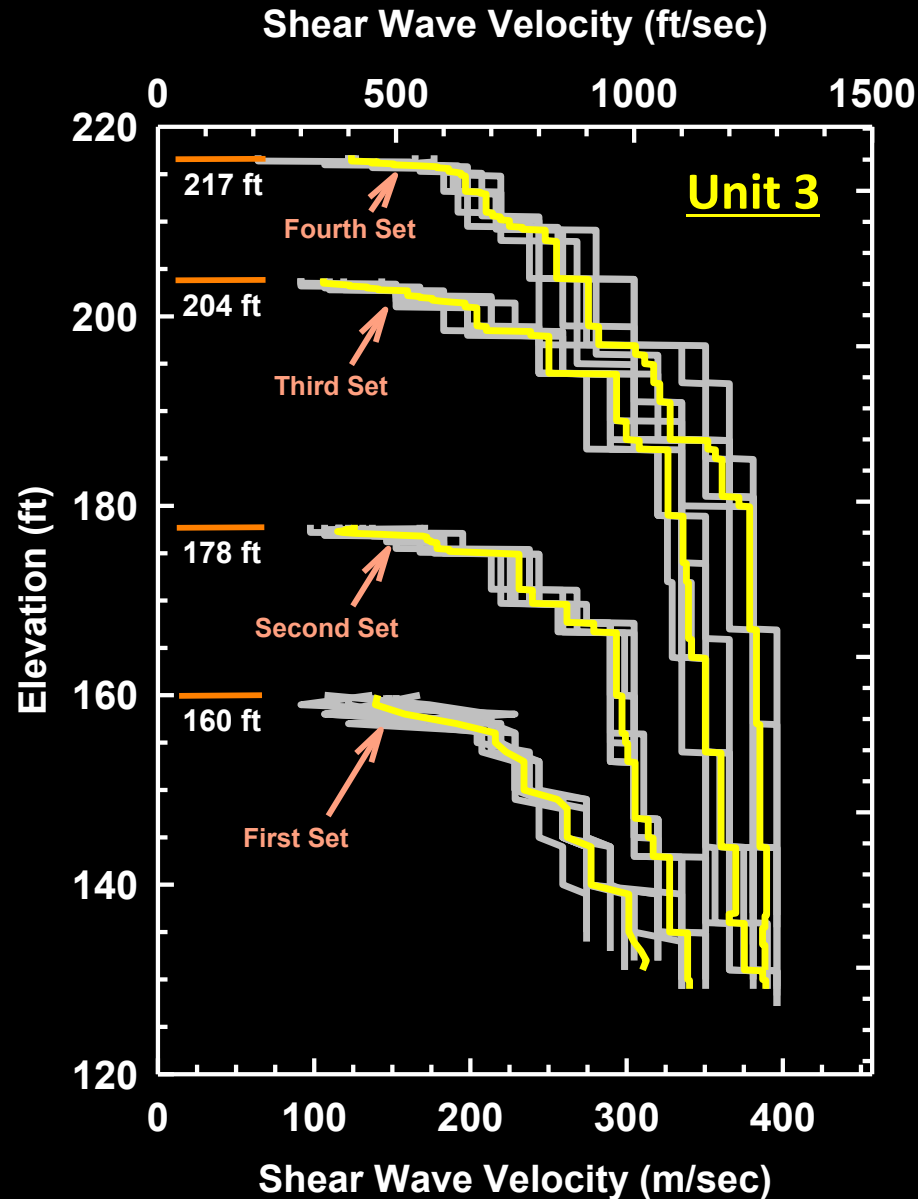
© 2011 Southern Company, Inc. All rights reserved.



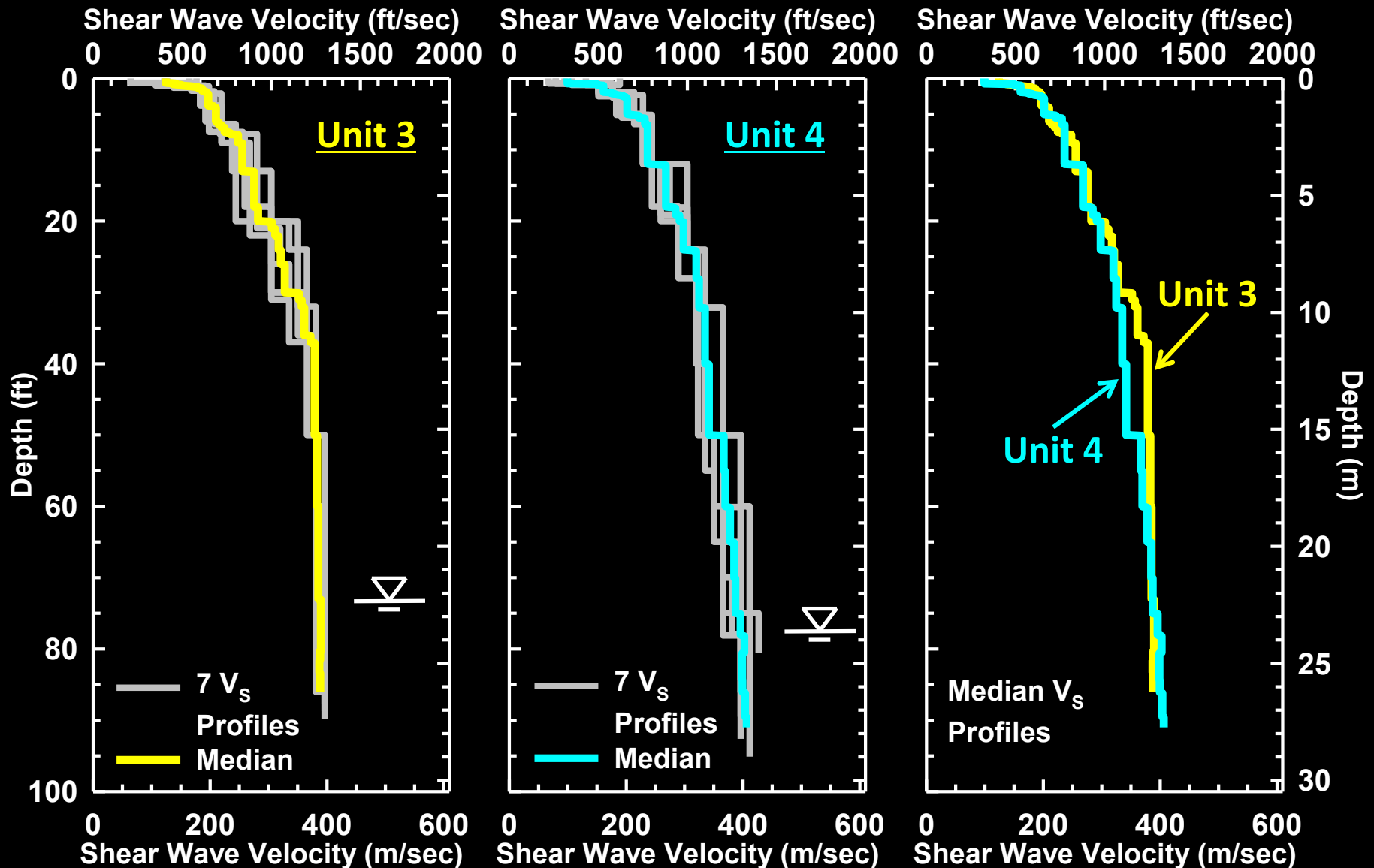
# SASW Testing on Completed Backfill



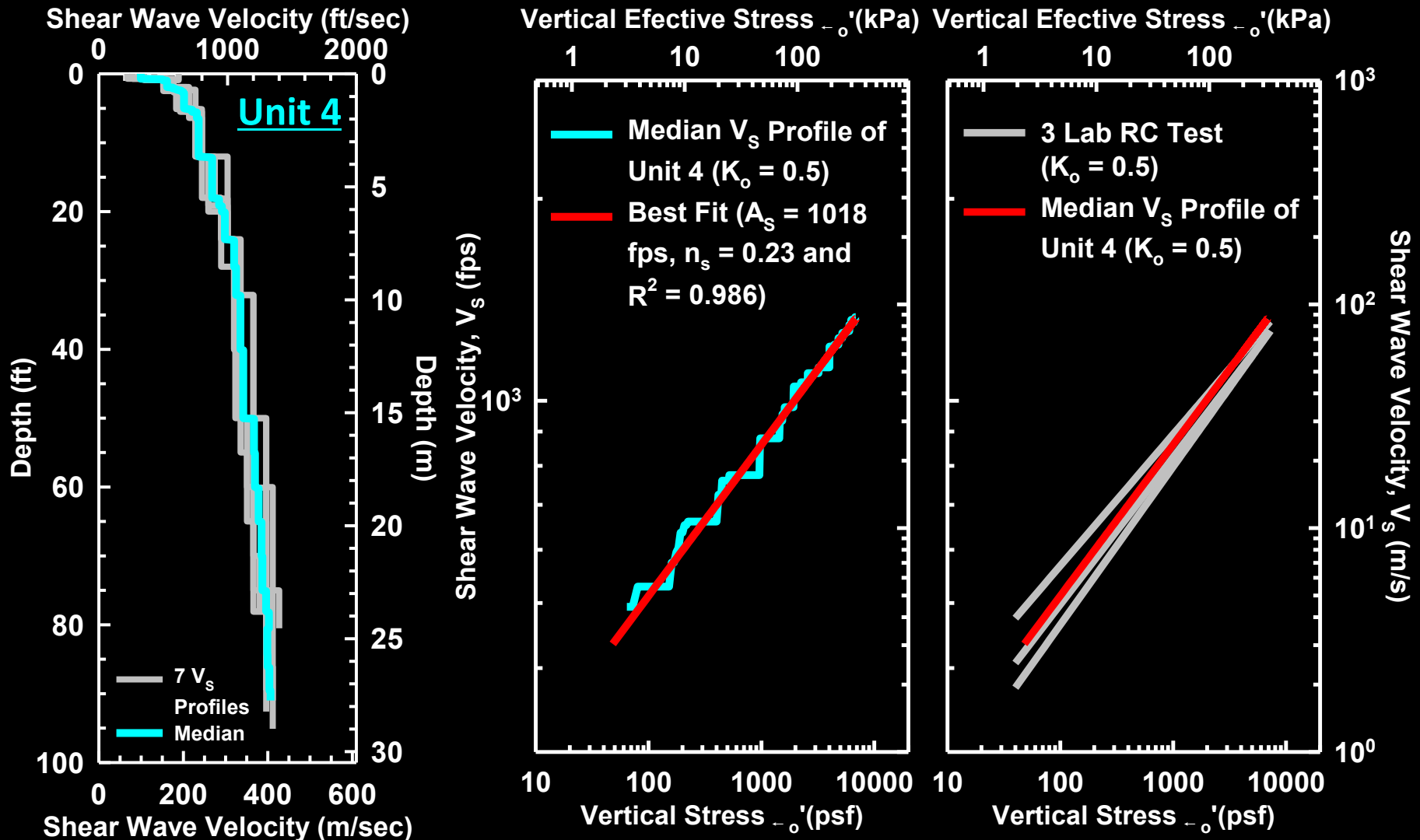
# Seismic Testing during Backfilling Process



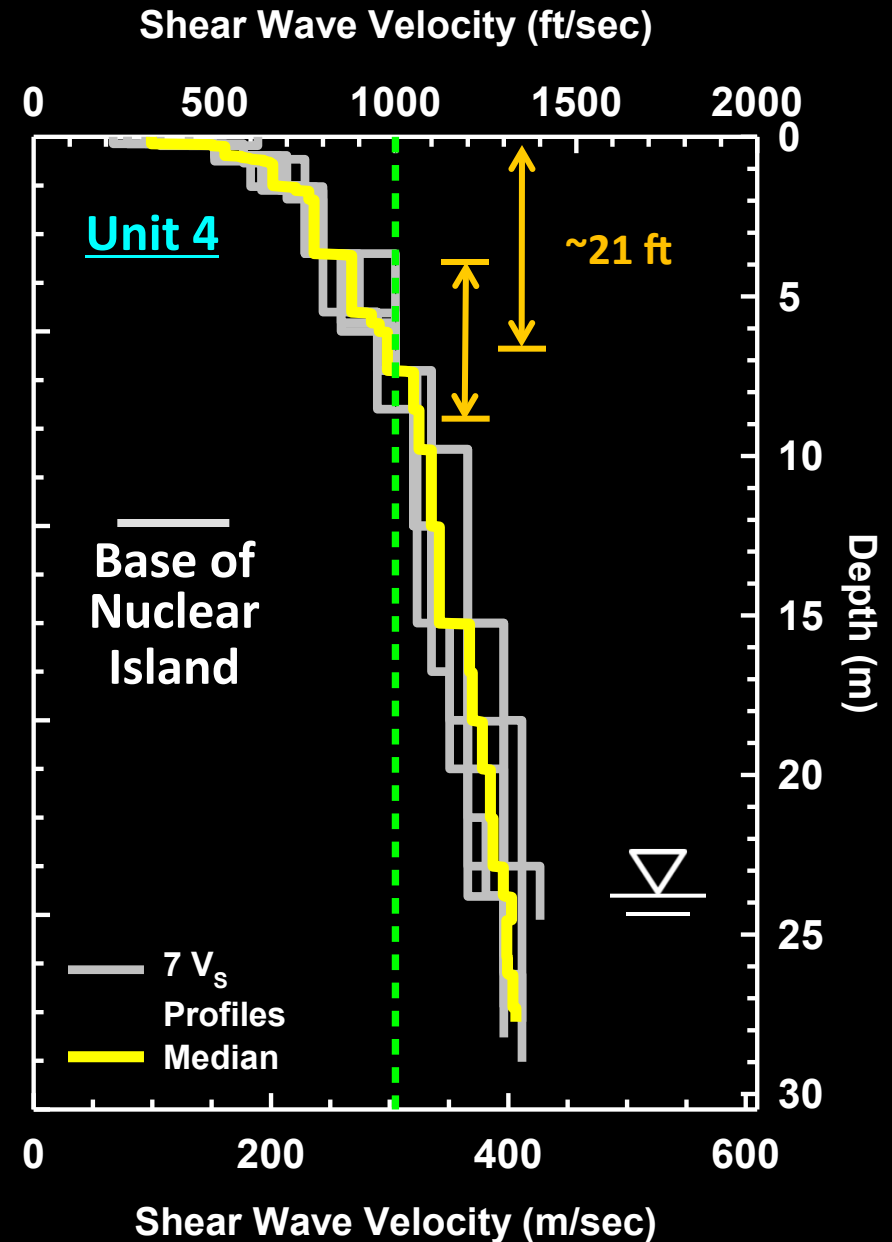
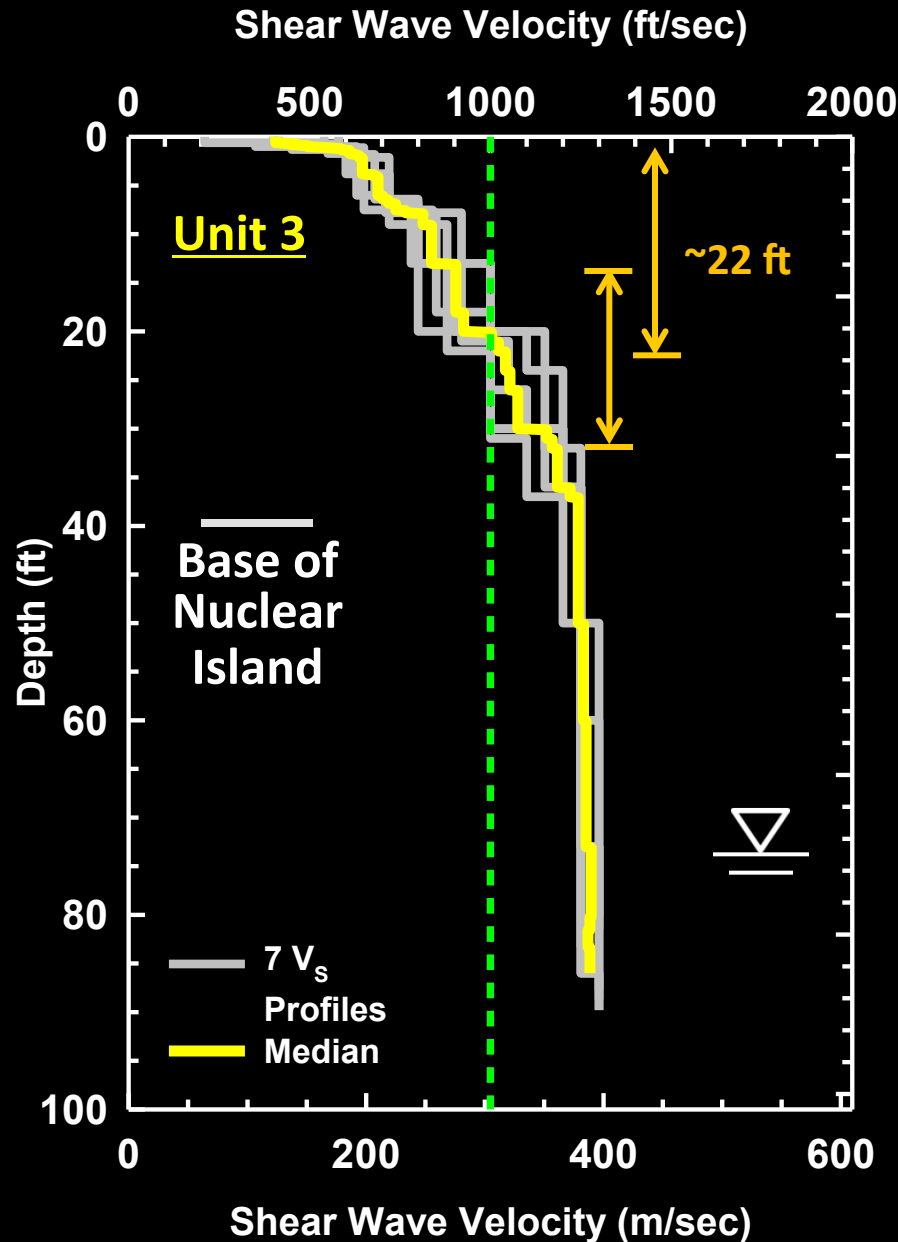
# Are the Two Backfills Alike?



# Do the Field and Lab $V_s$ Values Agree? (Could $V_s$ Profile be Predicted from Lab?)



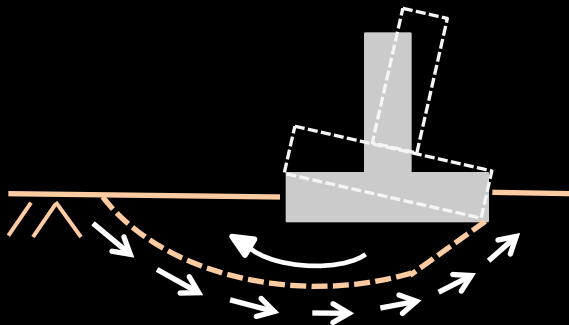
# Depth to $V_s > 1000$ fps (300 m/s)



## 2.3a Predicting Movements Under Static Loads: Shallow Foundations on Granular Soil

### Main Design Criteria

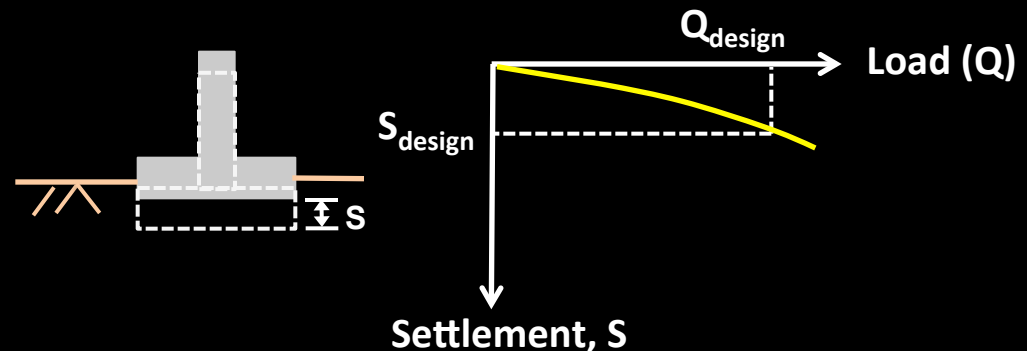
1. Bearing Capacity:  $Q_{\text{design}} = Q_{\text{ult}} / \text{F.S.}$



#### Approach

- Limit equilibrium analysis
- Requires strength parameters ( $\phi'$  and  $c'$ )

2. Permissible Settlement:  $S \leq S_{\text{design}}$



#### Traditional Approach

- Based on SPT and CPT correlations
- Soil sampling is hard and/or expensive in granular soil so rarely performed
- Stresses and strains are undefined

#### New Framework

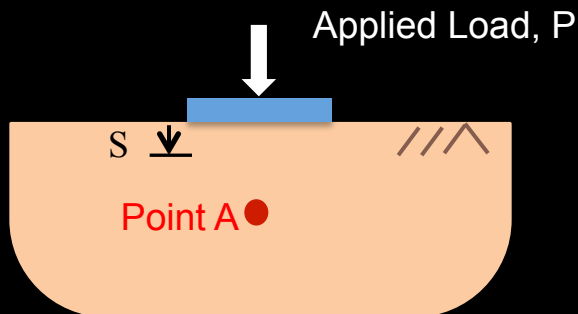
- Deformation-based analysis
- Stresses and strains are calculated

# New Framework for Predicting Settlements

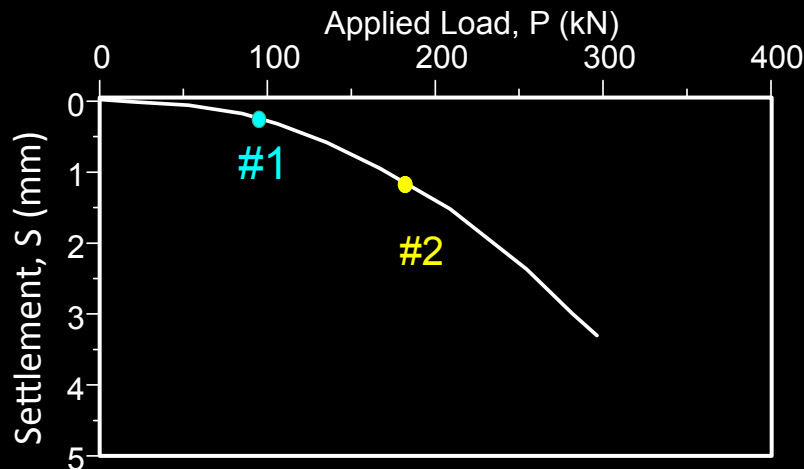
## Framework:

- Requires Stiffness Parameters
- $G$  Changing with  $\gamma$  and  $\sigma$
- $\nu$  Changing with  $\gamma$  (but presently assumed  $\nu = \text{constant}$ )

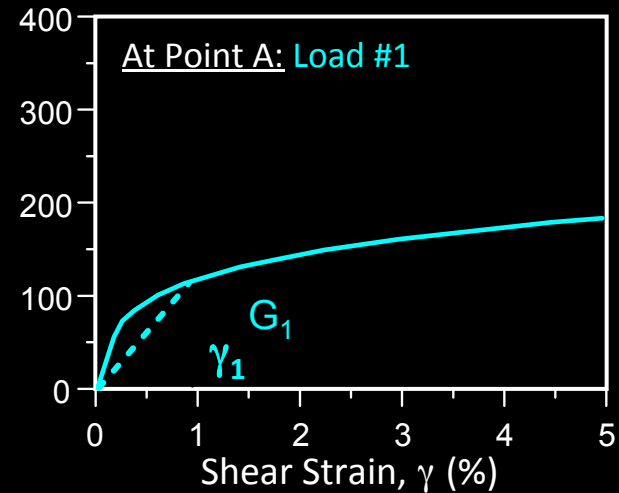
### 1. Loading Applied



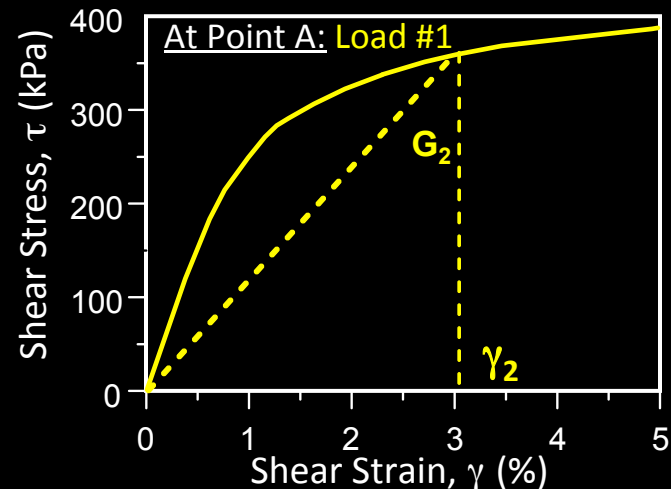
### 2. Load - Settlement Curve



### 3. Stress - and Strain - Dependent Moduli, Load #1:



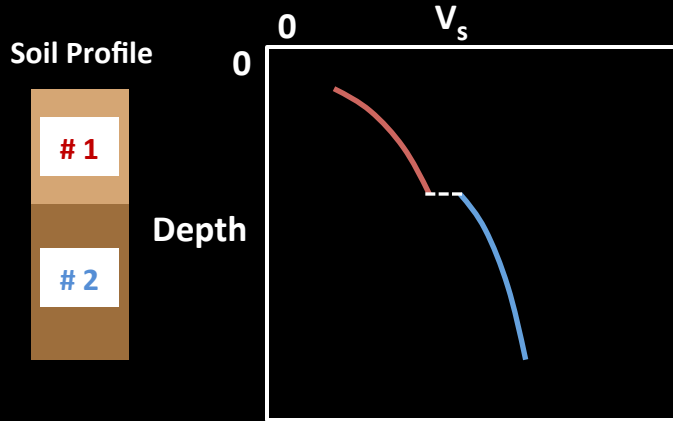
### 4. Stress - and Strain - Dependent Moduli, Load #2:



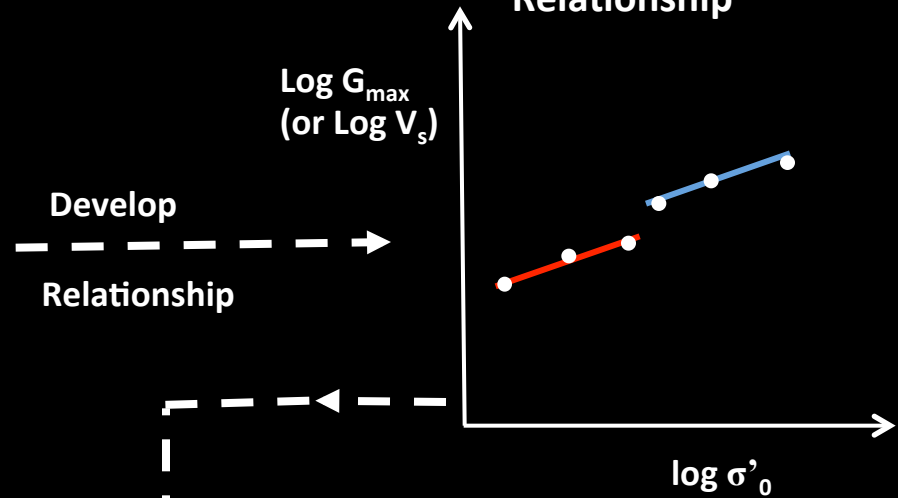


# Modeling with Dynamically Measured Soil Properties\*

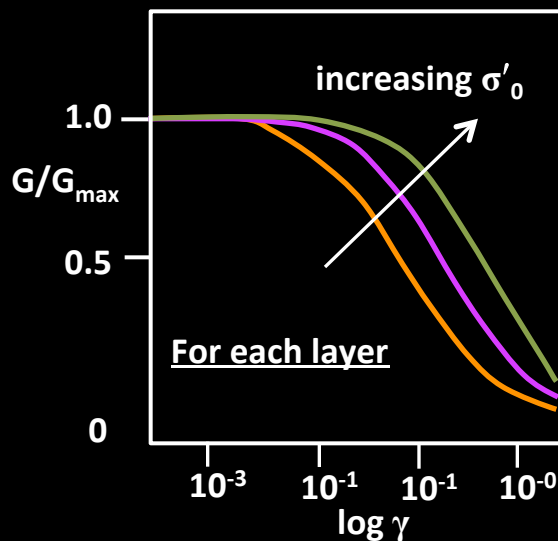
## Step # 1 - Field Seismic Testing for $V_s$ - Depth Profile



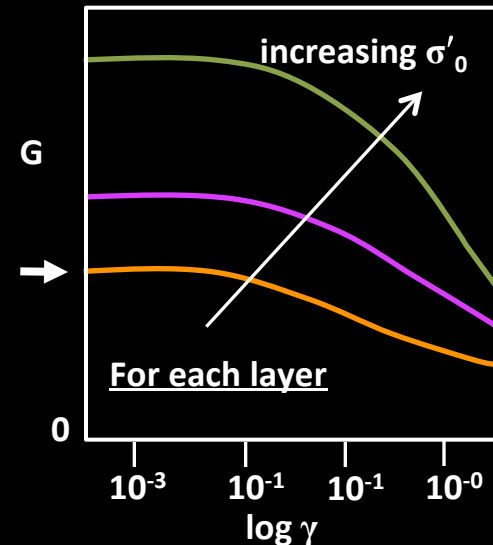
## Step # 2 - Field $\log G_{\max} - \log \gamma$ Relationship



## Step # 3 - Dynamic Laboratory Tests for $G/G_{\max} - \log \gamma$ Relationships

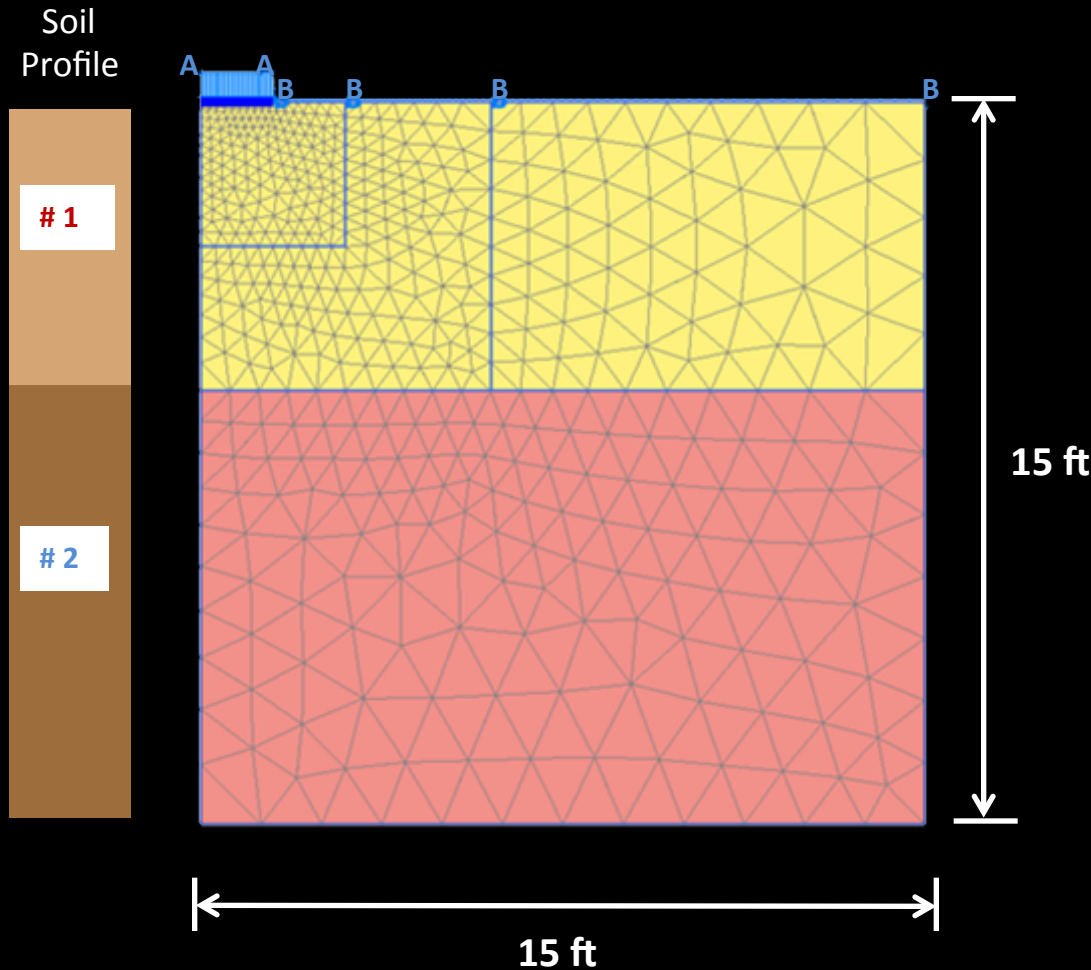


## Step # 4 - Combine Field Seismic and Dynamic Laboratory Tests for $G - \log \gamma$ Relationships



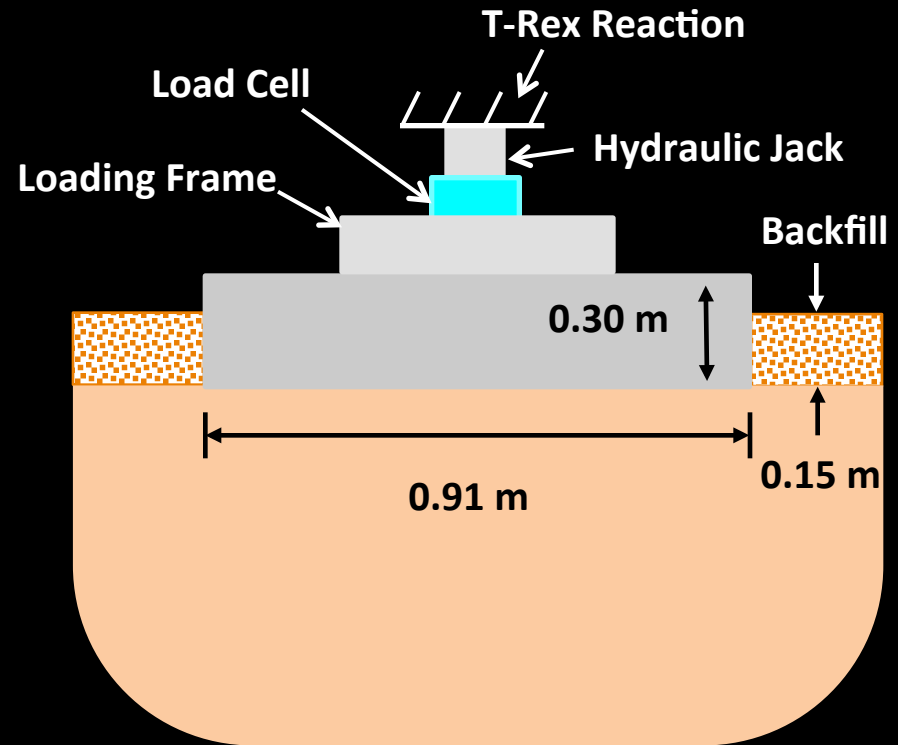
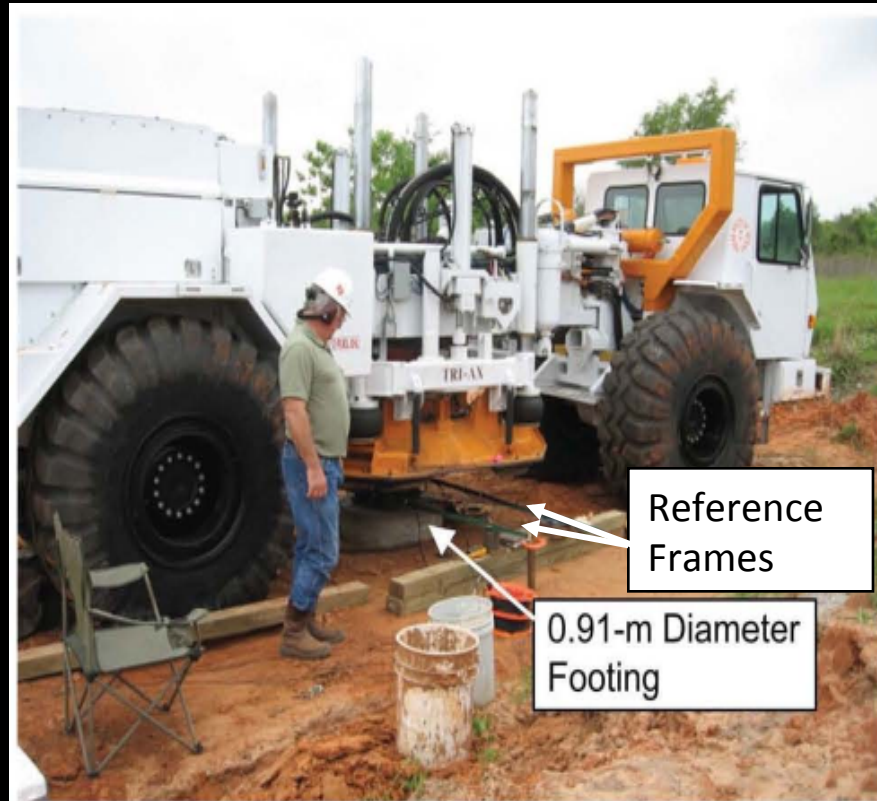
\* MoDaMP

# PLAXIS Finite Element Model with MoDaMP



- 946, 15-node triangular elements
- 15 ft x 15 ft dimensions
- Footings are modeled as flexible
- Axisymmetric model
- The lower boundary is fixed in both direction
- The vertical boundaries are fixed only in horizontal direction

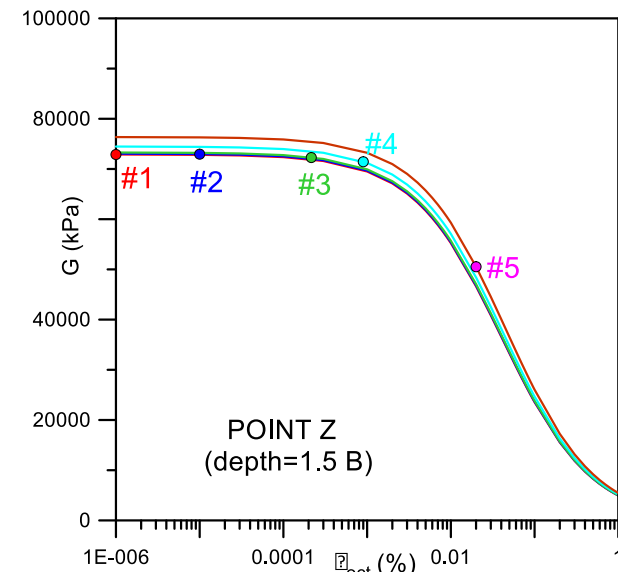
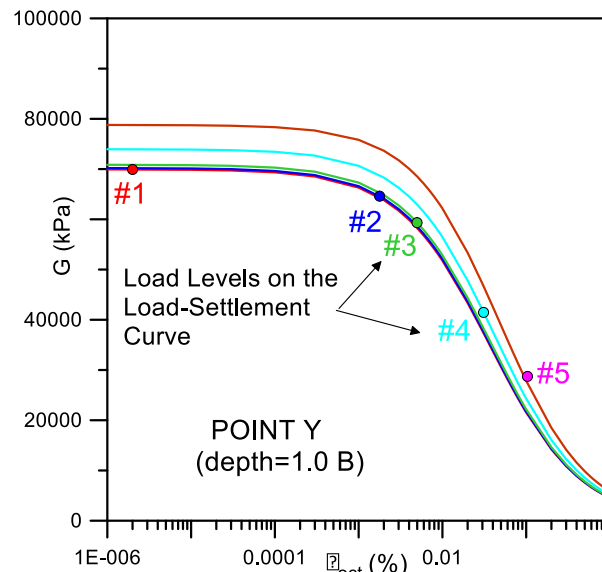
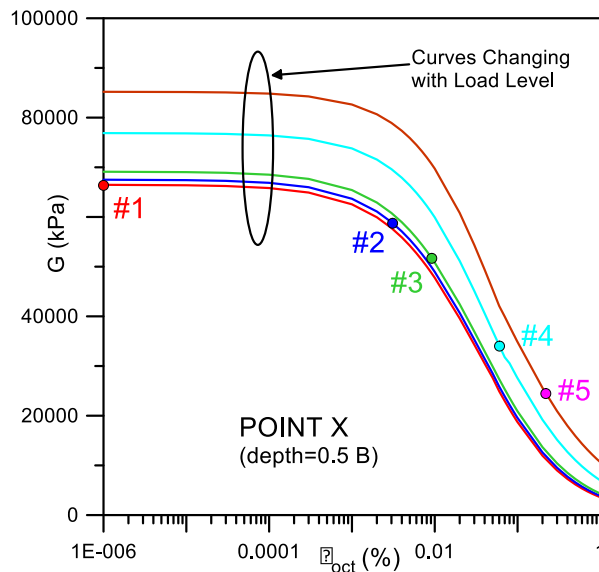
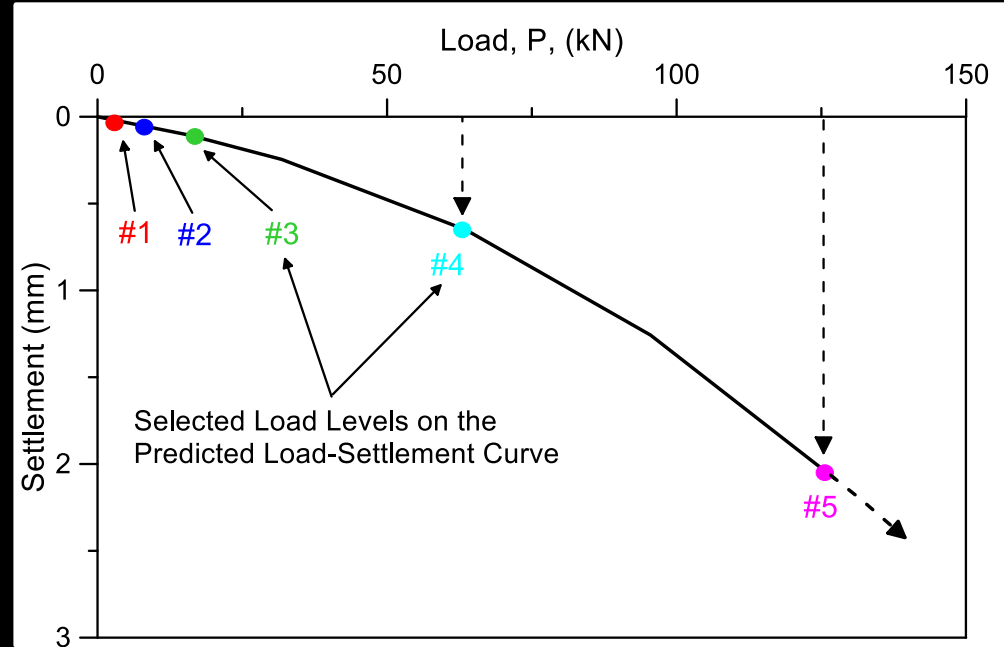
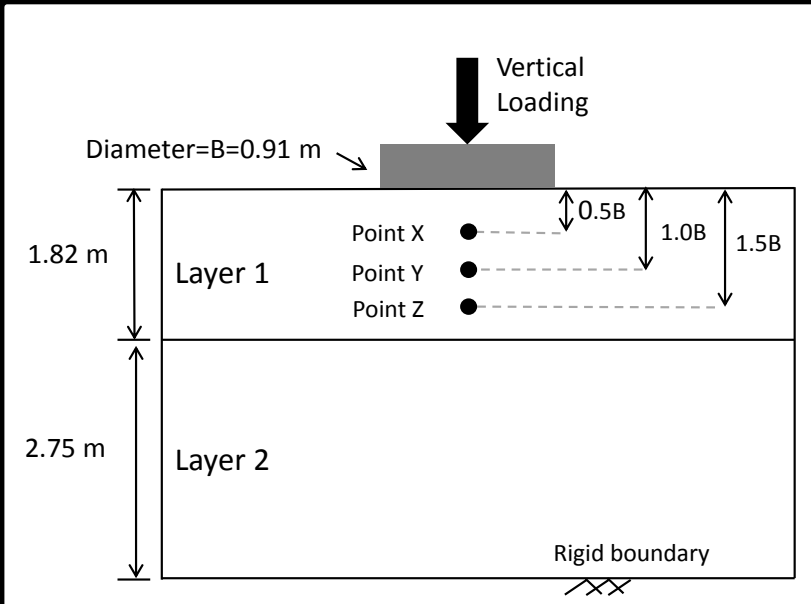
# Load-Settlement Tests at the NGES Test Site



- Two, circular, reinforced concrete footings with diameters of 0.91 m (3.0 ft) and 0.46 m (1.5 ft).
- Loading with T-Rex as a reaction; Settlements measured with linear potentiometers

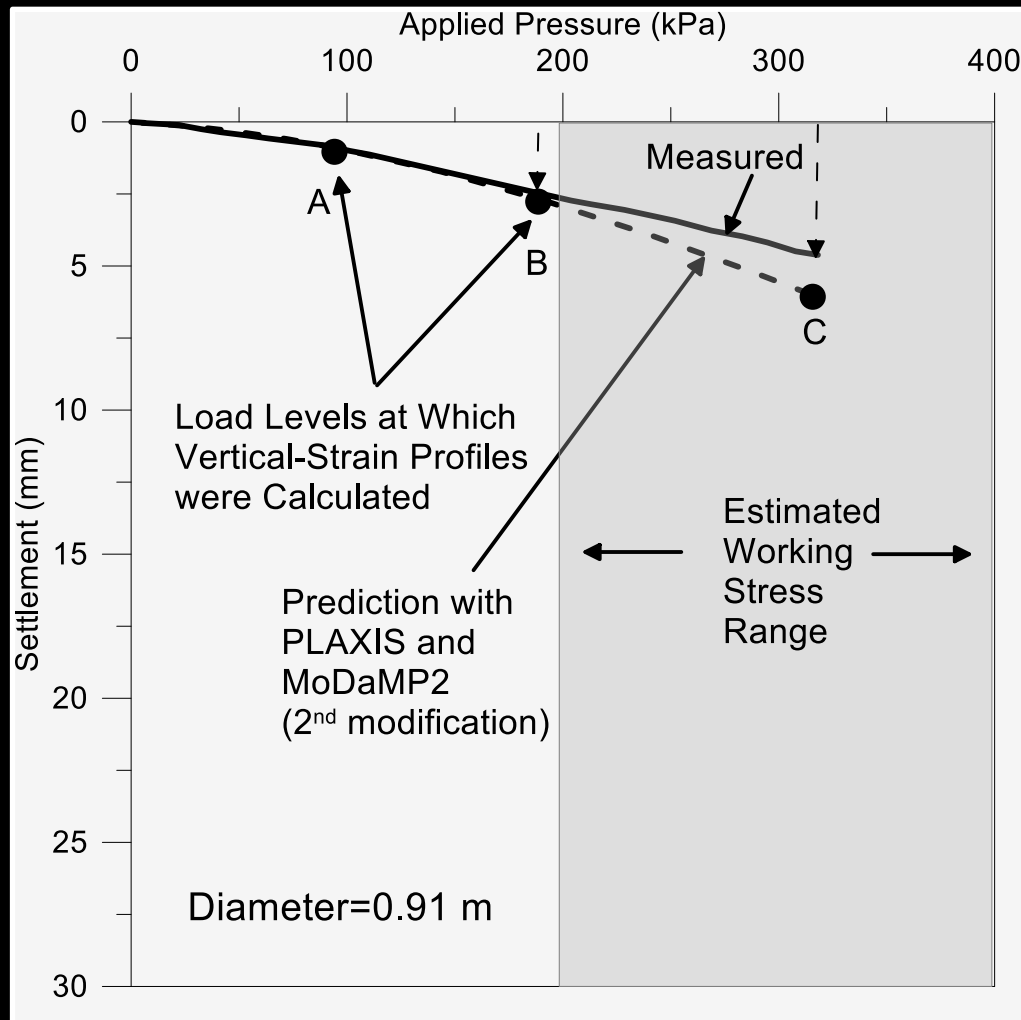
(Thank you Prof. Briaud!)

# Example of How MoDaMP Works



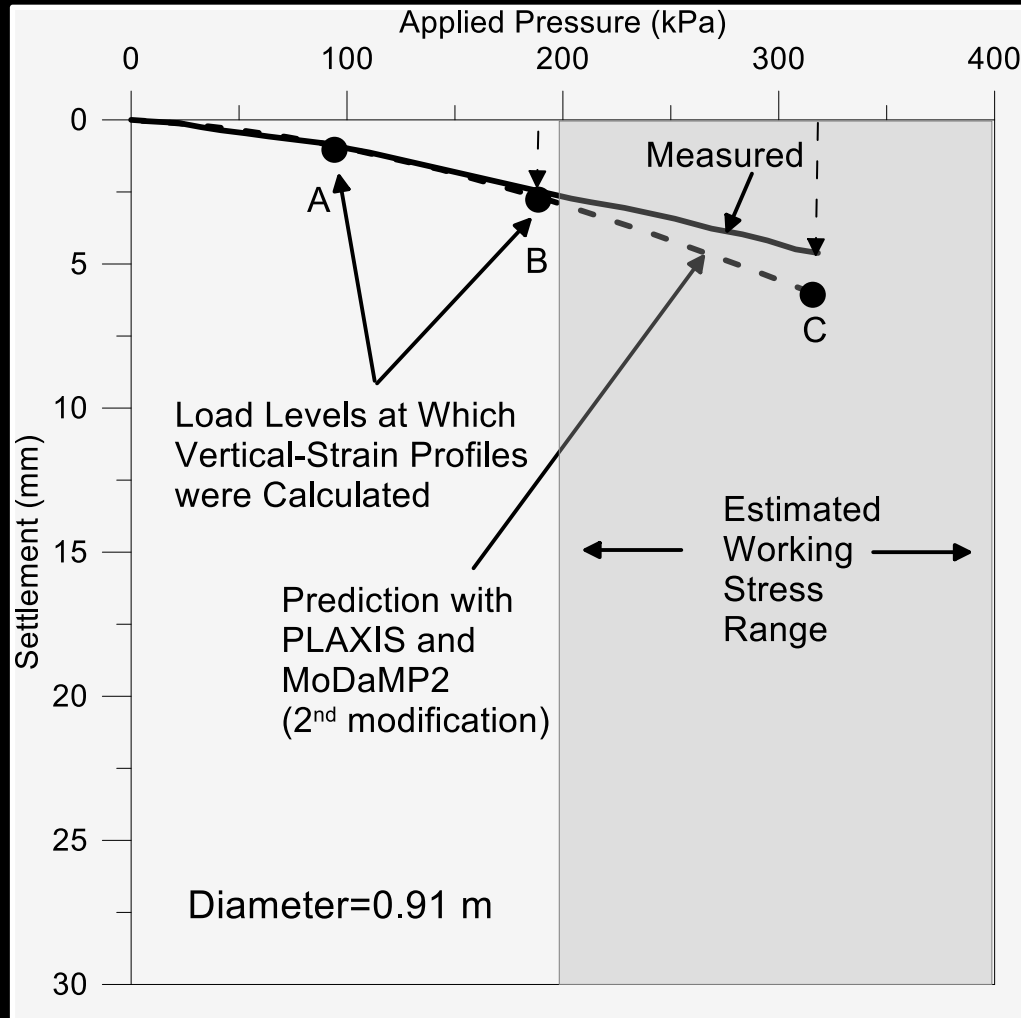
# Load-Settlement Predictions with MoDaMP

## Comparison of Predicted and Measured Settlements

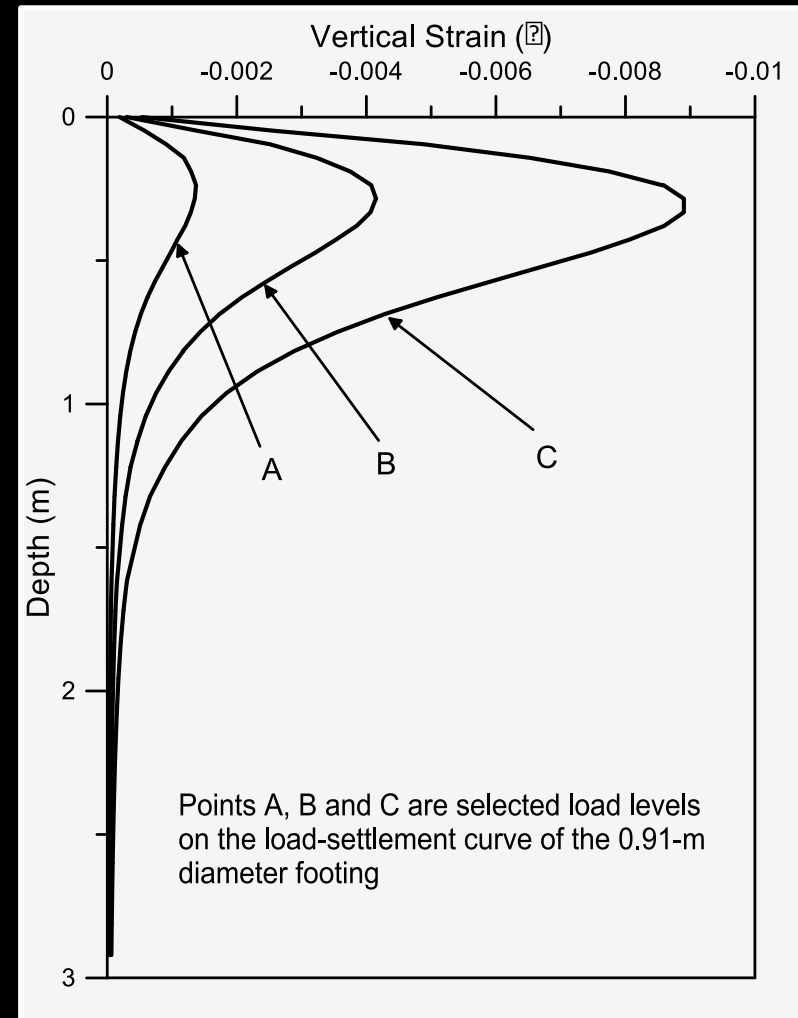


# Load-Settlement Predictions with MoDaMP

## Comparison of Predicted and Measured Settlements



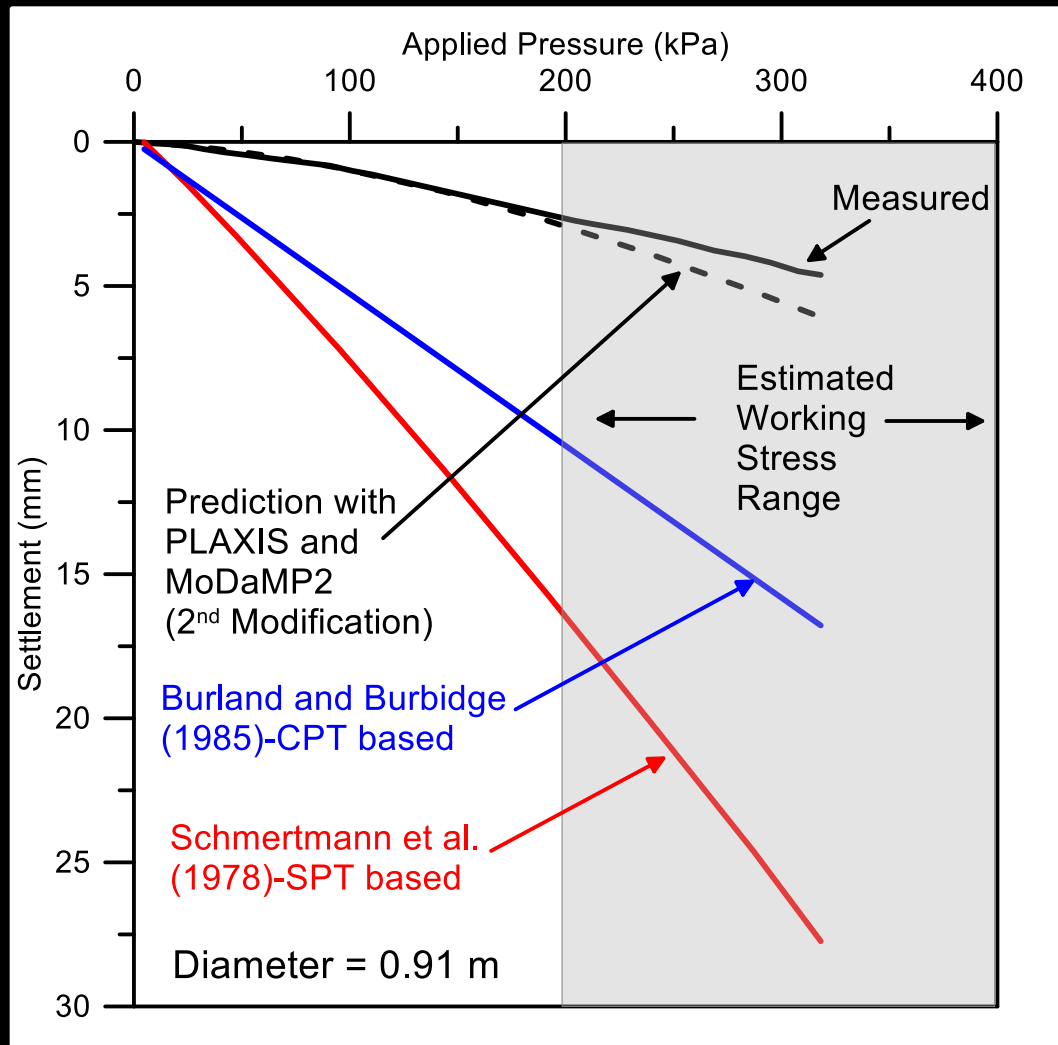
## Predicted Vertical Strains Beneath the Centerline of Footing





# Load-Settlement Predictions with MoDaMP

## Comparison of Predicted Settlements with CPT- and SPT-based Methods



## 2. Examples: Applications and Case Histories

- static loading conditions
- dynamic loading conditions

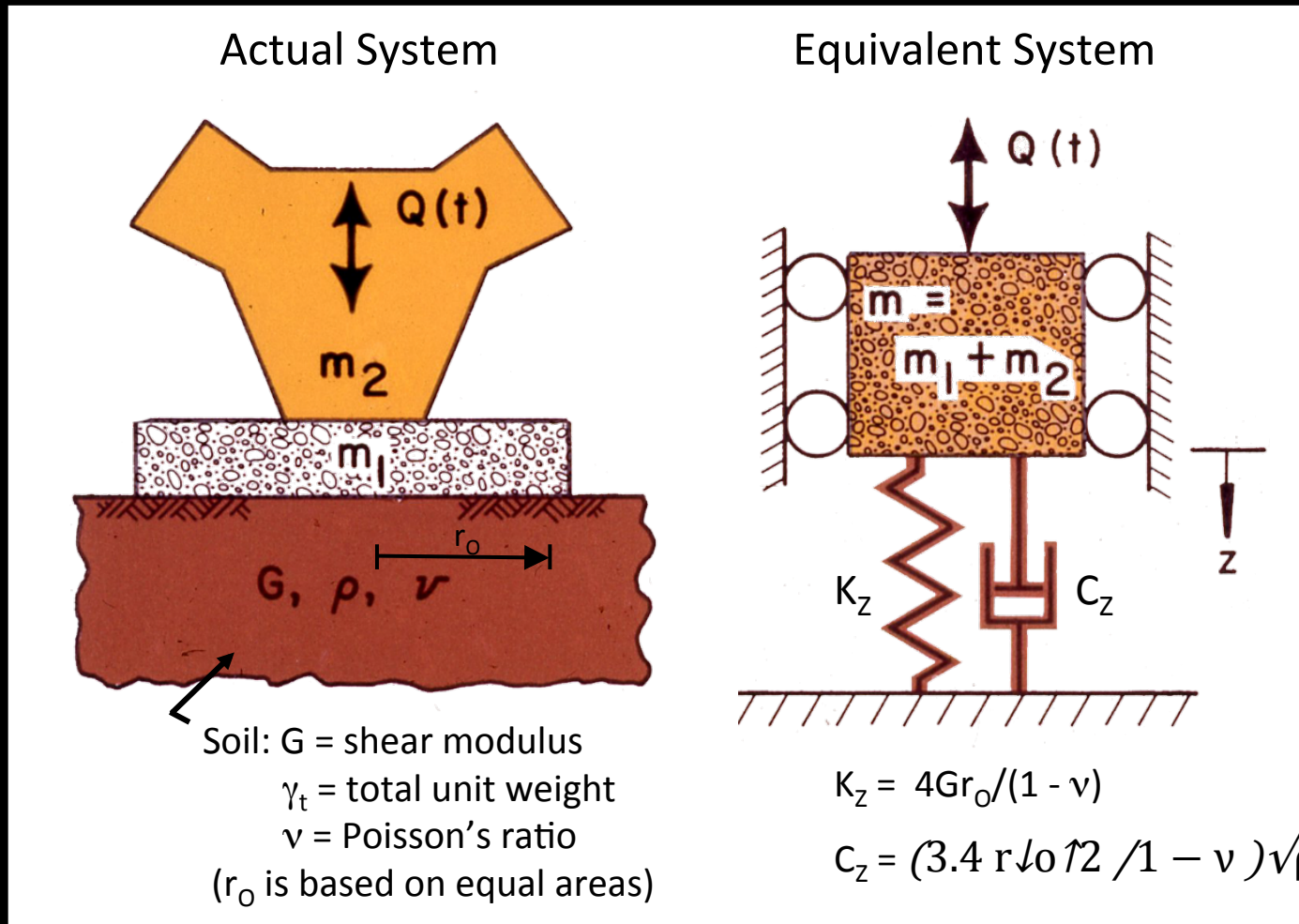
## **2. Examples (Cont'd): Dynamic Loading Conditions**

**→ 2.4 Machine-Foundation Design**

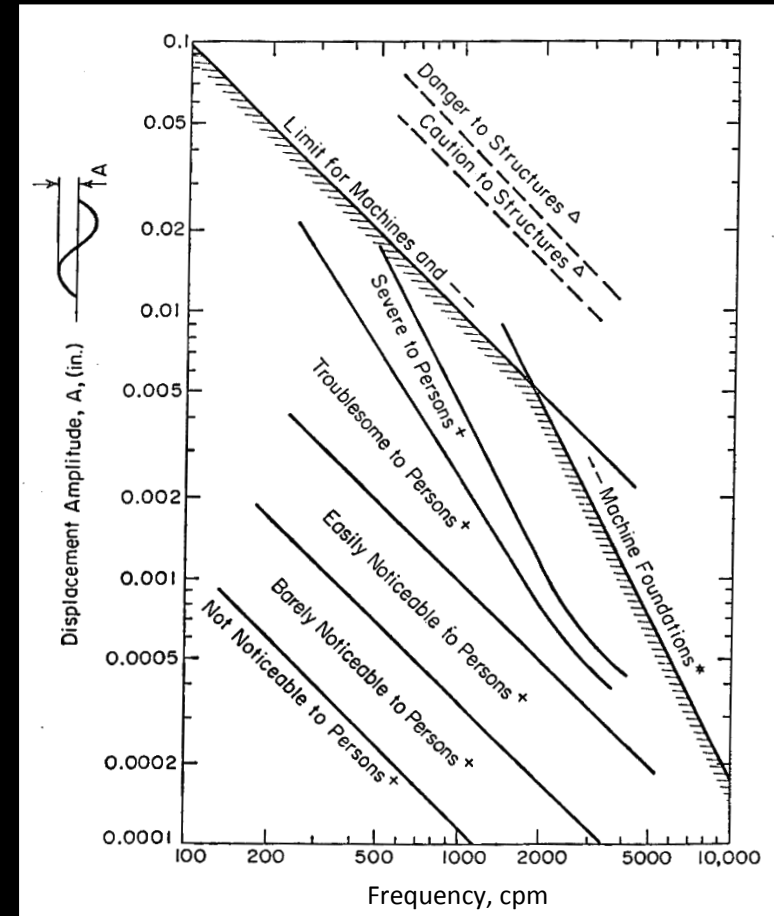
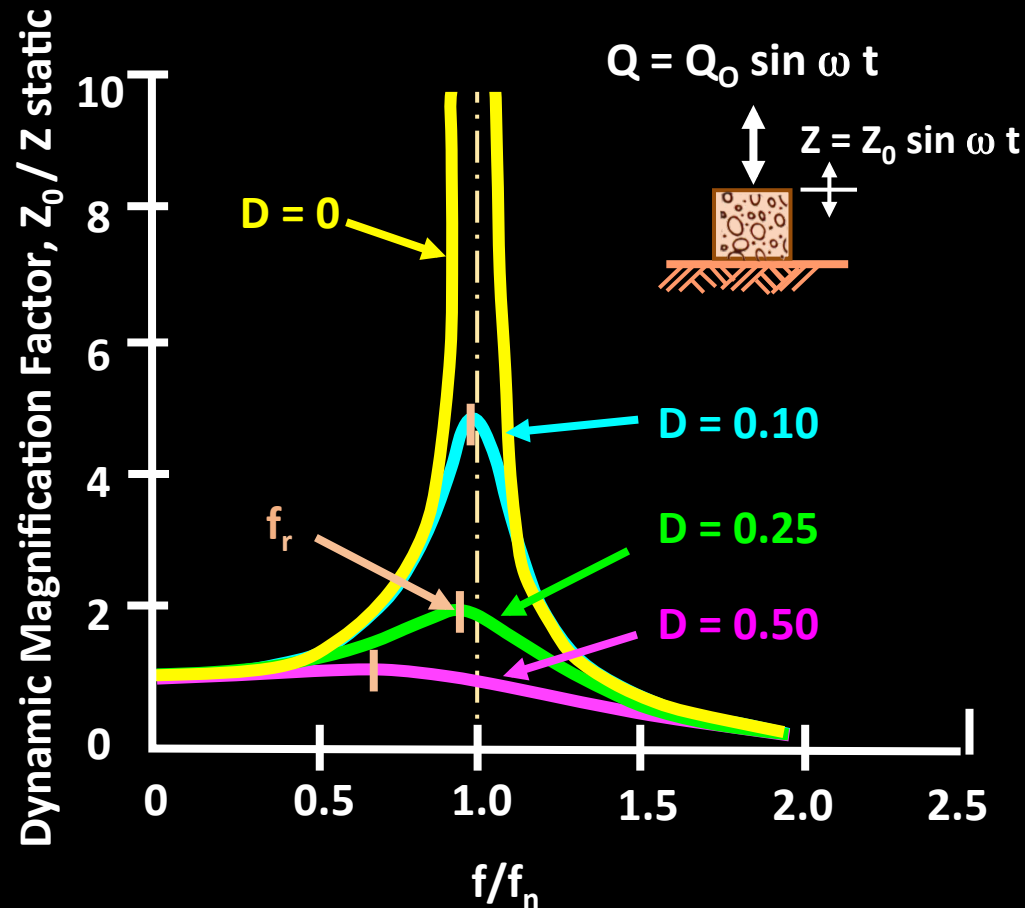
**2.5 Vibration-Isolation Barriers**

**2.6 Earthquake Engineering  
site response, soil-structure  
interaction, liquefaction, etc.**

## 2.4 Dynamically Loaded Machine Foundations



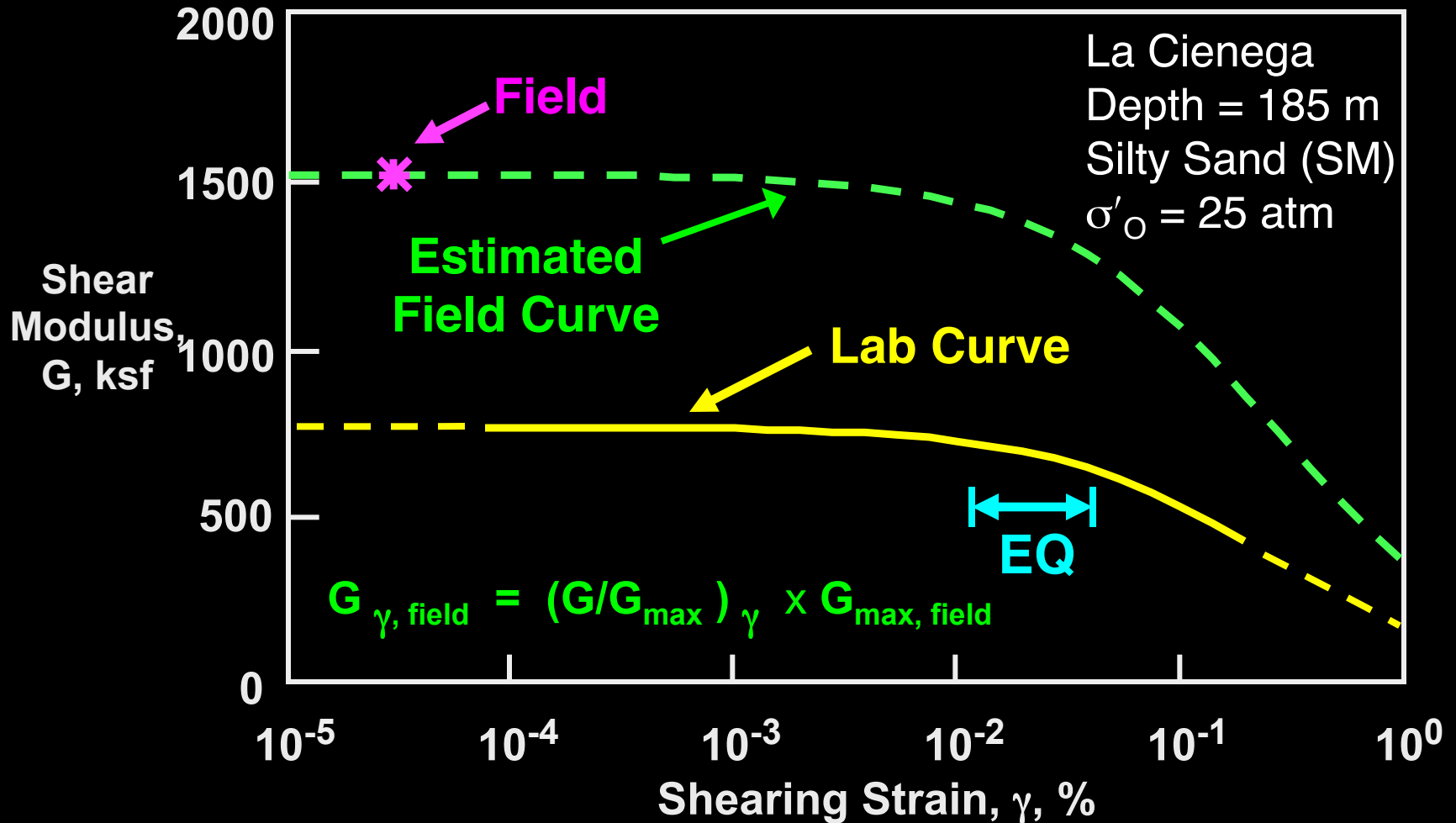
# Evaluating the Dynamic Response of the Machine Foundation System



From Richart, Hall and Woods, 1970

### 3. Link Between Field and Lab:

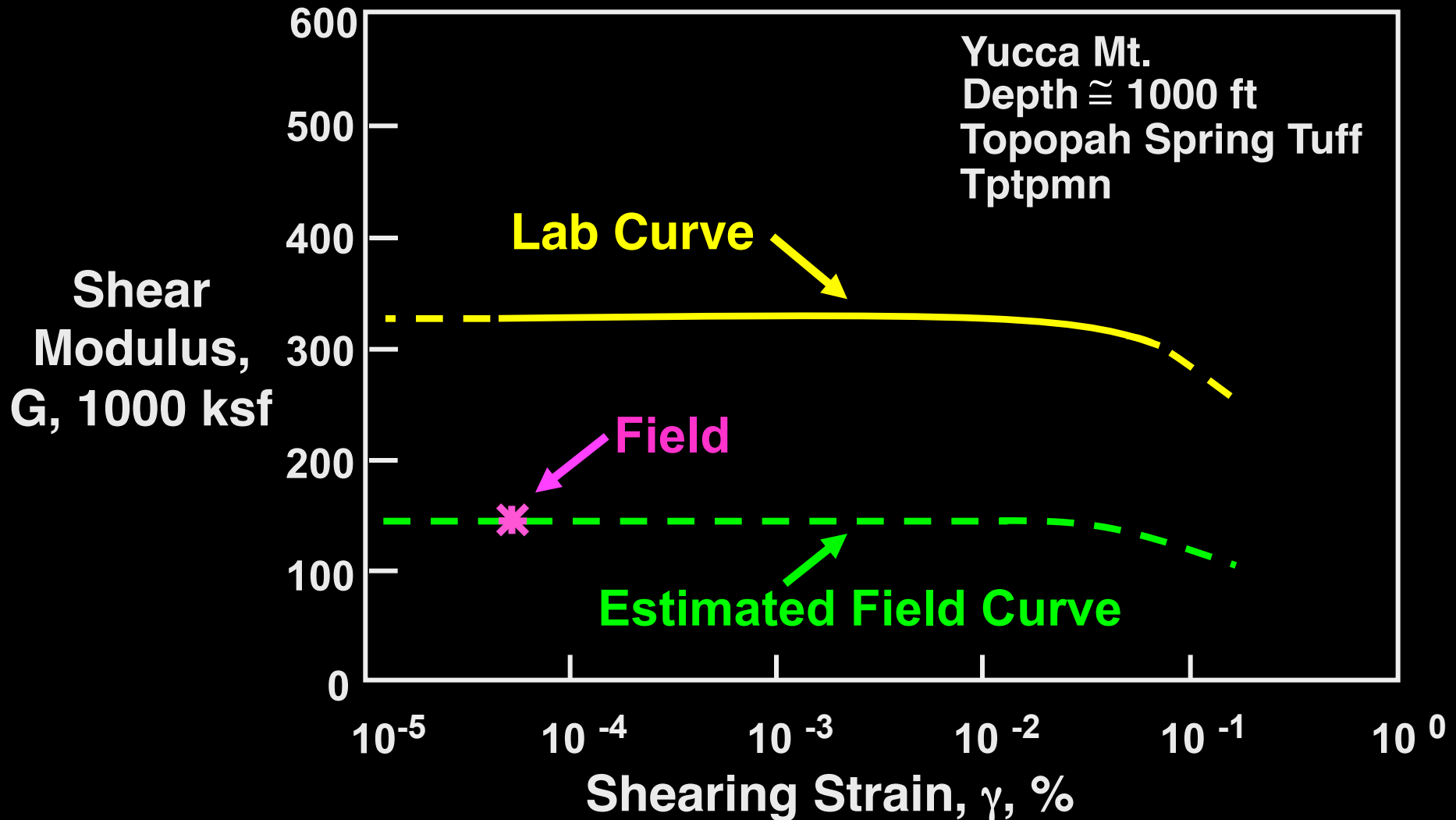
#### Estimating the Field $G - \log \gamma$ Relationship (Soil)





# Link Between Field and Lab:

## Estimating the Field $G - \log \gamma$ Relationship (Rock)



# Concluding Remarks

1. **Small-strain mechanical properties, expressed by  $V_s$  or  $G_{max}$ , play an important role in Geotechnical Engineering.**
2. **Small-strain mechanical properties are critical in dynamic and static deformational analyses under working loads.**
3. **Field measurements of  $V_s$  form the way to map nonlinear laboratory measurements to field behavior.**
4. **The importance of  $V_s$  or  $G_{max}$  ( and also  $V_p$  and  $M_{max}$  ) will continue to grow in solving dynamic and static problems.**

**Thank you**